

**ALLEGATO ALLA RELAZIONE TECNICA  
GENERALE E DI CALCOLO**

**N° 3**

**CORPO POMPE**



## INDICE

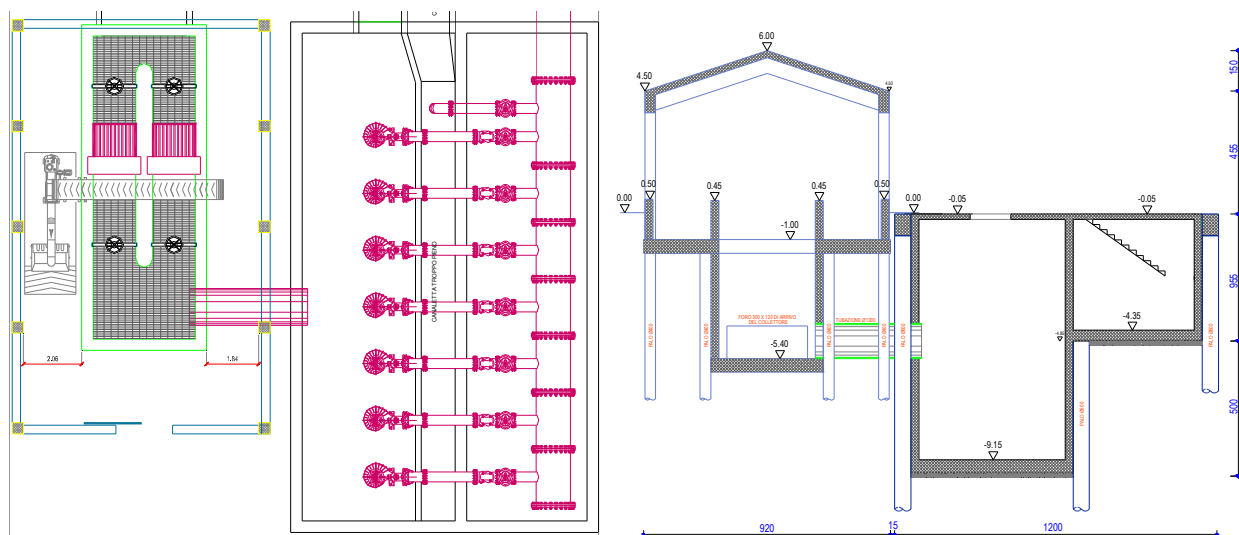
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# 1 - DESCRIZIONE GENERALE DELL'OPERA

L'opera oggetto della presente relazione consiste in una stazione di sollevamento di liquami; l'impianto presenta tre corpi giuntati di cui uno adibito ad uffici, uno con funzione di grigliatura ed uno destinato all'alloggiamento delle pompe di sollevamento.

Il locale griglia ed il locale pompe sono ravvicinati e presentano un giunto sismico di circa 15 cm.



Il locale adibito alle pompe è di forma rettangolare ed è interamente interrato, una paratia di pali disposta lungo il perimetro protegge lo scavo da spostamenti del terreno laterale, un locale di comando è posto lateralmente alla vasca con pompe e presenta una quota di fondo superiore. L'impalcato del locale pompe è realizzato con una soletta da 20 cm di spessore poggiante sulle pareti da 30 cm di spessore a loro volta sostenuti dalle platee di fondazione.

Le azioni previste sulla struttura sono legate alla destinazione d'uso e sono rappresentate da:

- Ambienti suscettibili di grande affollamento: musei, sale da ballo, palestre, tribune, sale da concerto, palasport, ecc.  
(Cat. C3 – Tab. 3.1.II - DM 14.01.2008) pari a 5,0 kN/m<sup>2</sup>;
- carichi accidentali per *Balconi, ballatoi e scale comuni*  
(Cat. C2 – Tab. 3.1.II - DM 14.01.2008) pari a 4,0 kN/m<sup>2</sup>;
- azione della neve;
- azione del vento;
- sisma.



## **2 - NORMATIVA DI RIFERIMENTO**

Le fasi di analisi e verifica della struttura sono state condotte in accordo alle seguenti disposizioni normative, per quanto applicabili in relazione al criterio di calcolo adottato dal progettista, evidenziato nel prosieguo della presente relazione:

**Legge 5 novembre 1971 n. 1086** (G. U. 21 dicembre 1971 n. 321)

"Norme per la disciplina delle opere di conglomerato cementizio armato, normale e precompresso ed a struttura metallica"

**Legge 2 febbraio 1974 n. 64** (G. U. 21 marzo 1974 n. 76)

"Provvedimenti per le costruzioni con particolari prescrizioni per le zone sismiche"

Indicazioni progettive per le nuove costruzioni in zone sismiche a cura del Ministero per la Ricerca scientifica - Roma 1981.

**D. M. Infrastrutture Trasporti 14 gennaio 2008** (G.U. 4 febbraio 2008 n. 29 - Suppl. Ord.)

"Norme tecniche per le Costruzioni"

Inoltre, in mancanza di specifiche indicazioni, ad integrazione della norma precedente e per quanto con esse non in contrasto, sono state utilizzate le indicazioni contenute nella:

**Circolare 2 febbraio 2009 n. 617 del Ministero delle Infrastrutture e dei Trasporti**  
(G.U. 26 febbraio 2009 n. 27 – Suppl. Ord.)

"Istruzioni per l'applicazione delle 'Norme Tecniche delle Costruzioni' di cui al D.M. 14 gennaio 2008".

**C.N.R. – UNI 10011**

"Istruzioni per il calcolo l'esecuzione e il montaggio"

**UNI ENV 1993-1-1**

"Eurocodice 3: Progettazione delle strutture di acciaio Parte 1-1 regole generali e regole per gli edifici"

**UNI 11104:2004**

**UNI EN 206-1:2006**

**UNI EN 197**

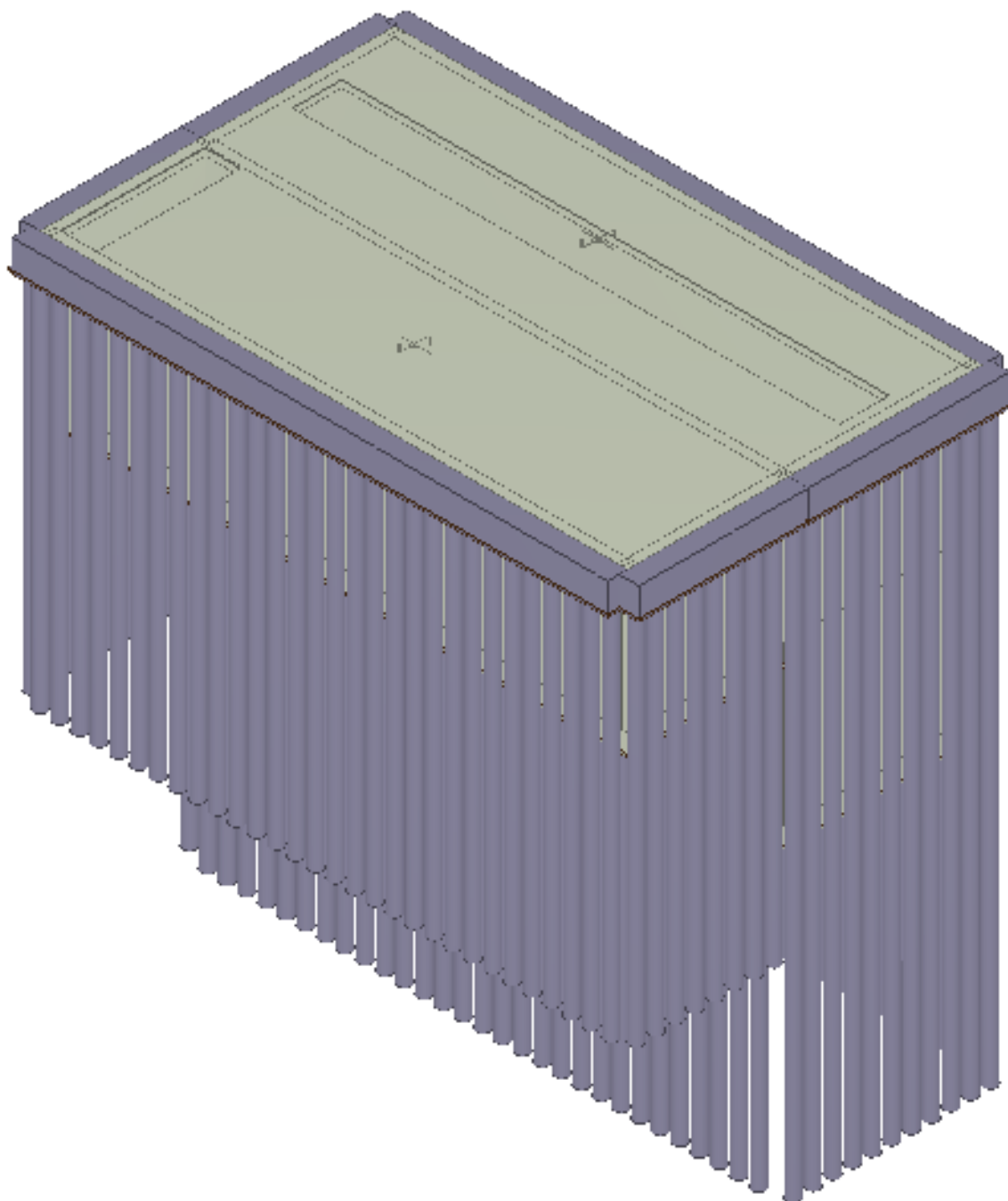


### 3 – TABULATO DI CALCOLO – FONDAZIONE CORPO POMPE

Vengono riportate di seguito due viste assonometriche contrapposte, allo scopo di consentire una migliore comprensione della struttura oggetto della presente relazione:

#### **Vista Anteriore**

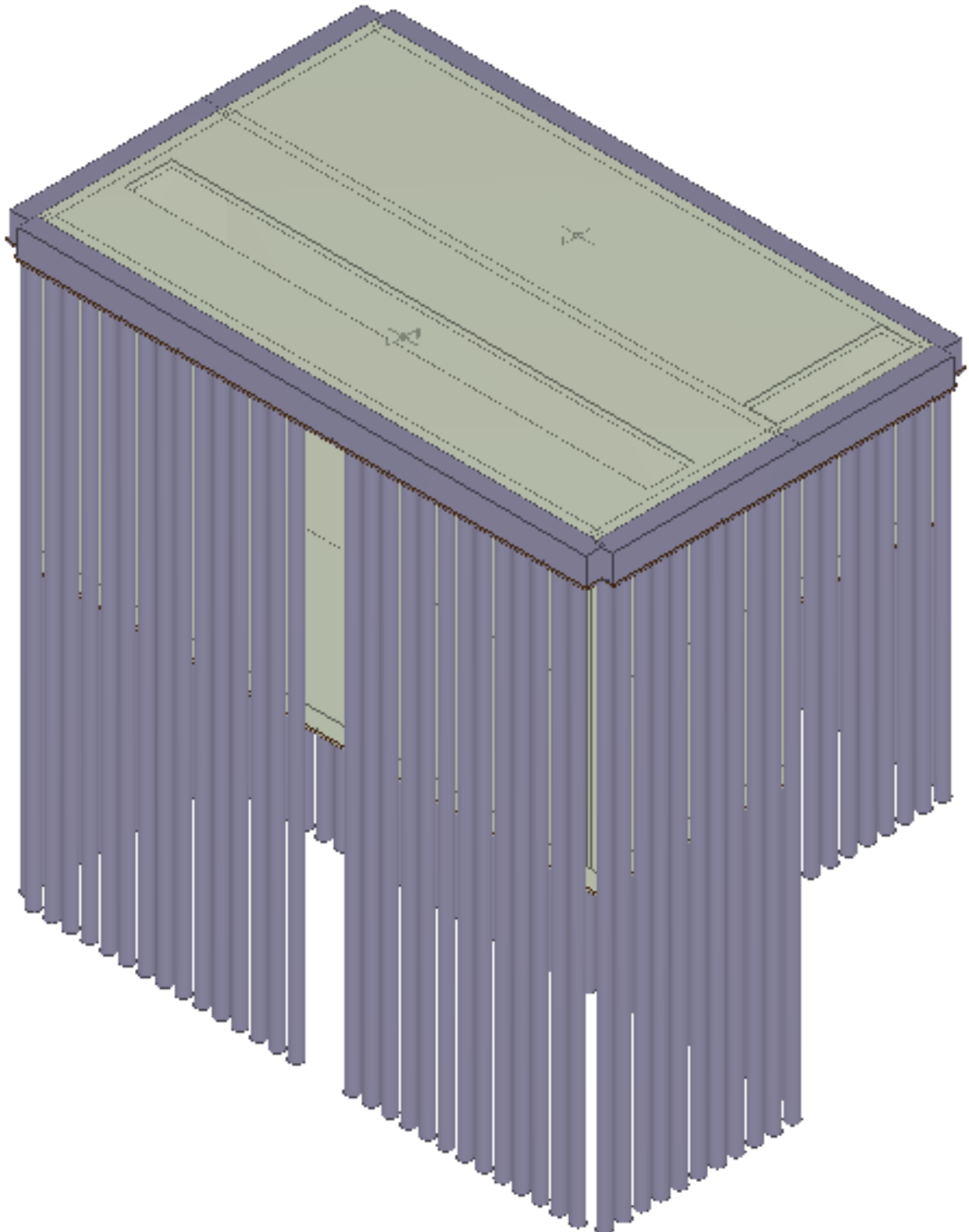
*La direzione di visualizzazione (bisettrice del cono ottico), relativamente al sistema di riferimento globale  $0, X, Y, Z$ , ha versore  $(1;1;-1)$*





### **Vista Posteriore**

*La direzione di visualizzazione (bisettrice del cono ottico), relativamente al sistema di riferimento globale  $0, X, Y, Z$ , ha versore  $(-1;-1;-1)$*



### **Verifiche di regolarità**

Sia per la scelta del metodo di calcolo, sia per la valutazione del fattore di struttura adottato, deve essere effettuato il controllo della regolarità della struttura.



La tabella seguente riepiloga, per la struttura in esame, le condizioni di regolarità in pianta ed in altezza soddisfatte.

REGOLARITÀ DELLA STRUTTURA IN PIANTA	
La configurazione in pianta è compatta e approssimativamente simmetrica rispetto a due direzioni ortogonali, in relazione alla distribuzione di masse e rigidezze	SI
Il rapporto tra i lati di un rettangolo in cui la costruzione risulta inscritta è inferiore a 4	SI
Nessuna dimensione di eventuali rientri o sporgenze supera il 25 % della dimensione totale della costruzione nella corrispondente direzione	SI
Gli orizzontamenti possono essere considerati infinitamente rigidi nel loro piano rispetto agli elementi verticali e sufficientemente resistenti	SI

REGOLARITÀ DELLA STRUTTURA IN ALTEZZA	
Tutti i sistemi resistenti verticali (quali telai e pareti) si estendono per tutta l'altezza della costruzione	NO
Massa e rigidezza rimangono costanti o variano gradualmente, senza bruschi cambiamenti, dalla base alla sommità della costruzione (le variazioni di massa da un orizzontamento all'altro non superano il 25 %, la rigidezza non si riduce da un orizzontamento a quello sovrastante più del 30% e non aumenta più del 10%); ai fini della rigidezza si possono considerare regolari in altezza strutture dotate di pareti o nuclei in c.a. o pareti e nuclei in muratura di sezione costante sull'altezza o di telai controventati in acciaio, ai quali sia affidato almeno il 50% dell'azione sismica alla base	NO
Nelle strutture intelaiate progettate in CD "B" il rapporto tra resistenza effettiva e resistenza richiesta dal calcolo non è significativamente diverso per orizzontamenti diversi (il rapporto fra la resistenza effettiva e quella richiesta, calcolata ad un generico orizzontamento, non deve differire più del 20% dall'analogo rapporto determinato per un altro orizzontamento); può fare eccezione l'ultimo orizzontamento di strutture intelaiate di almeno tre orizzontamenti	NO
Eventuali restringimenti della sezione orizzontale della costruzione avvengono in modo graduale da un orizzontamento al successivo, rispettando i seguenti limiti: ad ogni orizzontamento il rientro non supera il 30% della dimensione corrispondente al primo orizzontamento, né il 20% della dimensione corrispondente all'orizzontamento immediatamente sottostante. Fa eccezione l'ultimo orizzontamento di costruzioni di almeno quattro piani per il quale non sono previste limitazioni di restringimento	NO

La rigidezza è calcolata come rapporto fra il taglio complessivamente agente al piano e  $\delta$ , spostamento relativo di piano (il taglio di piano è la sommatoria delle azioni orizzontali agenti al di sopra del piano considerato).

Tutti i valori calcolati ed utilizzati per le verifiche sono riportati nei tabulati di calcolo nella relativa sezione.

La struttura è pertanto:

- REGOLARE in pianta
- NON REGOLARE in altezza

## Spettri di Progetto per S.L.U. e S.L.D.

L'edificio è stato progettato per una Vita Nominale pari a **50** e per Classe d'Uso pari a **3**.

In base alle indagini geognostiche effettuate si è classificato il suolo di fondazione di categoria **C**, cui corrispondono i seguenti valori per i parametri necessari alla costruzione degli spettri di risposta orizzontale e verticale:

Stato Limite	Parametri di pericolosità sismica							
	$a_g$	$F_0$	$T^*_c$	$C_c$	$T_B$	$T_c$	$T_D$	$S_s$
	[g]		[s]		[s]	[s]	[s]	[s]
SLO	0.0577	2.333	0.305	1.55	0.158	0.474	1.831	1.50
SLD	0.0758	2.329	0.321	1.53	0.164	0.491	1.903	1.50
SLV	0.1942	2.422	0.344	1.49	0.171	0.513	2.377	1.42
SLC	0.2419	2.509	0.347	1.49	0.172	0.517	2.568	1.34

Per la definizione degli spettri di risposta, oltre all'accelerazione  $a_g$  al suolo (dipendente dalla classificazione sismica del Comune) occorre determinare il Fattore di Struttura  $q$ .



Il Fattore di struttura  $q$  è un fattore riduttivo delle forze elastiche introdotto per tenere conto delle capacità dissipative della struttura che dipende dal sistema costruttivo adottato, dalla Classe di Duttilità e dalla regolarità in altezza.

Si è inoltre assunto il Coefficiente di Amplificazione Topografica  $S_T$  pari a **1,00**.

Tali succitate caratteristiche sono riportate negli allegati tabulati di calcolo al punto "DATI GENERALI ANALISI SISMICA".

Per la struttura in esame sono stati determinati i seguenti valori:

#### Stato Limite di salvaguardia della Vita

Fattore di Struttura  $q$  per sisma orizzontale in direzione X: **2,64**

Fattore di Struttura  $q$  per sisma orizzontale in direzione Y: **2,64**

Fattore di Struttura  $q$  per sisma verticale: **1,50**

Di seguito si esplicita il calcolo del fattore di struttura utilizzato per il sisma orizzontale:

- tipologia tab. 7.4.I D.M. 14/01/2008: **A pareti, miste equivalenti a pareti**
- tipologia strutturale: **altre strutture a pareti non accoppiate**
- $\alpha_u/\alpha_1, X$ : **1.1**
- $\alpha_u/\alpha_1, Y$ : **1.1**
- fattore di riduzione  $q_0$  (kw): **1.00**
- regolarità in pianta: **REGOLARE**
- regolarità in altezza: **NON REGOLARE**

Il fattore di struttura è calcolato secondo la relazione (7.3.1) del § 7.3.1 del D.M. 14/01/2008:

$$q = q_0 \times K_R$$

dove:

$q_0$  è il valore massimo del fattore di struttura che dipende dal livello di duttilità attesa, dalla tipologia strutturale e dal rapporto  $\alpha_u/\alpha_1$  tra il valore dell'azione sismica per il quale si verifica la formazione di un numero di cerniere plastiche tali da rendere la struttura labile e quello per il quale il primo elemento strutturale raggiunge la plasticizzazione a flessione;

$K_R$  è un fattore riduttivo che dipende dalle caratteristiche di regolarità in altezza della costruzione, con valore pari ad 1 per costruzioni regolari in altezza e pari a 0,8 per costruzioni non regolari in altezza.

**N.B:** Per le costruzioni *regolari in pianta*, qualora non si proceda ad un'analisi non lineare finalizzata alla valutazione del rapporto  $\alpha_u/\alpha_1$ , per esso possono essere adottati i valori indicati nei § 7.4.3.2 del D.M. 14/01/2008 per le diverse tipologie costruttive. Per le costruzioni *non regolari in pianta*, si possono adottare valori di  $\alpha_u/\alpha_1$  pari alla media tra 1,0 ed i valori di volta in volta forniti per le diverse tipologie costruttive.

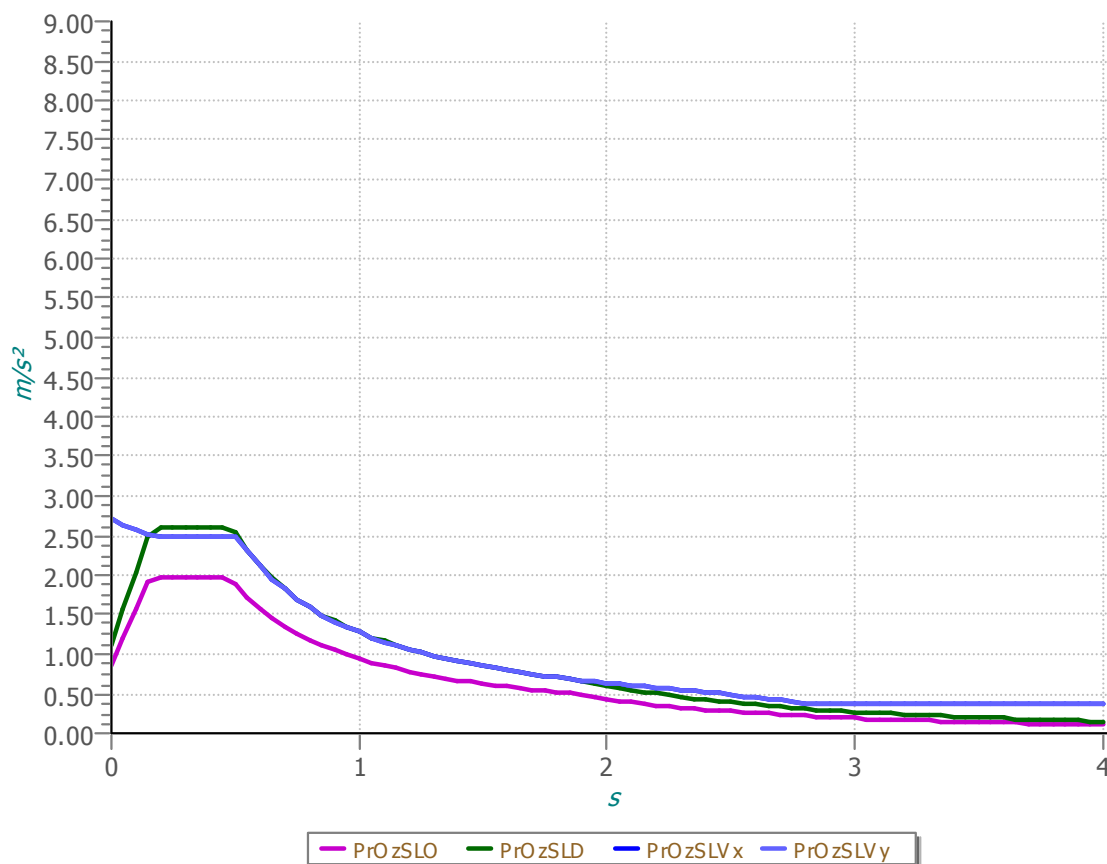
**Tabella 7.4.I – Valori di  $q_0$**

Tipologia	$q_0$	
	CD" B "	CD" A "
Strutture a telaio, a pareti accoppiate, miste	$3,0 \alpha_u/\alpha_1$	$4,5 \alpha_u/\alpha_1$
Strutture a pareti non accoppiate	3,0	$4,0 \alpha_u/\alpha_1$
Strutture deformabili torsionalmente	2,0	3,0
Strutture a pendolo inverso	1,5	2,0

Gli spettri utilizzati sono riportati nella successiva figura.



## SPETTRI di RISPOSTA di ACCELERAZIONE



## Metodo di Analisi

Il calcolo delle azioni sismiche è stato eseguito in analisi dinamica modale, considerando il comportamento della struttura in regime elastico lineare.

Il numero di modi di vibrazione considerato (15) ha consentito, nelle varie condizioni, di mobilitare le seguenti percentuali delle masse della struttura:

Stato Limite	Direzione Sisma	%
salvaguardia della vita	X	93.8
salvaguardia della vita	Y	89.4
salvaguardia della vita	Z	100.0

## Modello di Calcolo

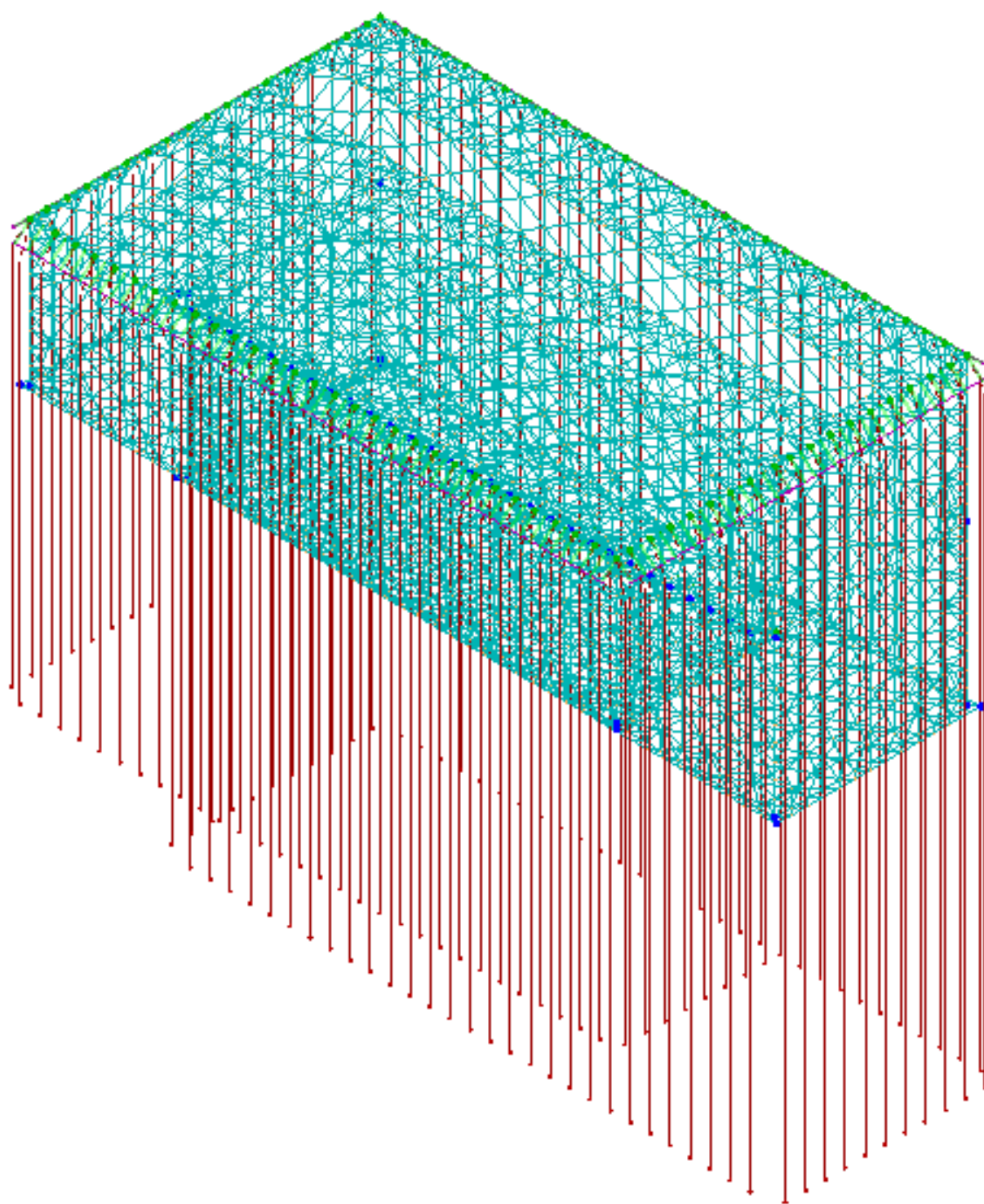
Il modello della struttura viene creato automaticamente dal codice di calcolo, individuando i vari elementi strutturali e fornendo le loro caratteristiche geometriche e meccaniche.

Viene definita un'opportuna numerazione degli elementi (nodi, aste, shell) costituenti il modello, al fine di individuare celermente ed univocamente ciascun elemento nei tabulati di calcolo.

Qui di seguito è fornita una rappresentazione grafica dettagliata della discretizzazione operata con evidenziazione dei nodi e degli elementi.

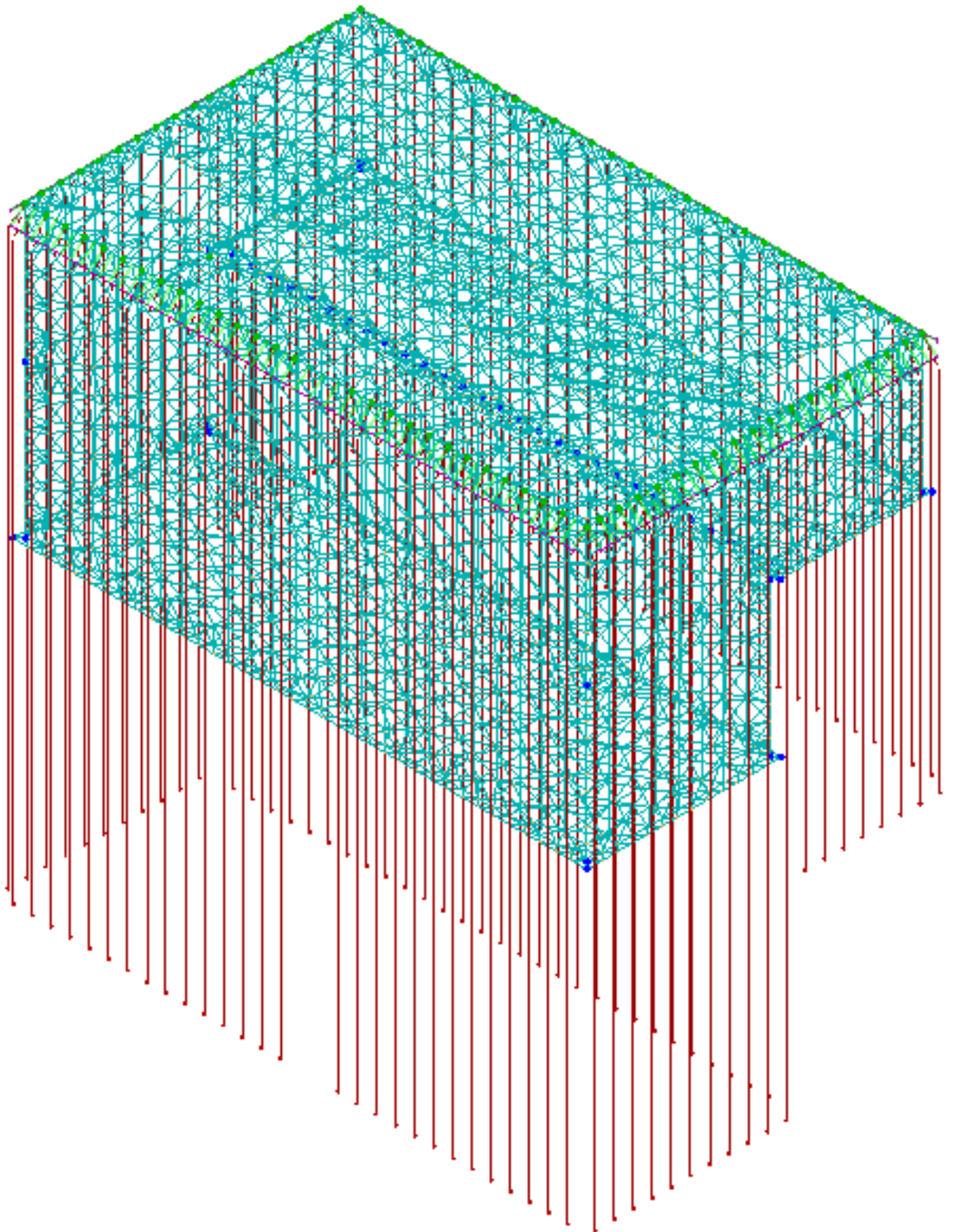


## Vista Anteriore





### Vista Posteriore



Dalle illustrazioni precedenti si evince come le aste, sia travi che pilastri, siano schematizzate con un tratto flessibile centrale e da due tratti (braccetti) rigidi alle estremità. I nodi vengono posizionati sull'asse verticale dei pilastri, in corrispondenza dell'estradosso della trave più alta che in esso si collega. Tramite i braccetti i tratti flessibili sono quindi collegati ad esso.



In questa maniera il nodo risulta perfettamente aderente alla realtà poiché vengono presi in conto tutti gli eventuali disassamenti degli elementi con gli effetti che si possono determinare, quali momenti flettenti/torcenti aggiuntivi.

Le sollecitazioni vengono determinate, com'è corretto, solo per il tratto flessibile. Sui tratti rigidi, infatti, essendo (teoricamente) nulle le deformazioni le sollecitazioni risultano indeterminate.

Questa schematizzazione dei nodi viene automaticamente realizzata dal programma anche quando il nodo sia determinato dall'incontro di più travi senza il pilastro, o all'attacco di travi/pilastri con elementi shell.

## MATERIALI CALCESTRUZZO ARMATO

Caratteristiche Calcestruzzo Armato												
N	$\gamma_k$	CdT	E	G	R <sub>ck</sub>	R <sub>cm</sub>	%R <sub>ck</sub>	$\gamma_c$	f <sub>ctd</sub>	f <sub>cfm</sub>	n	n Ac
	[N/m <sup>3</sup> ]	[1/°C]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]						
Cls C25/30_B450C - (C25/30)												
001	25,000	0.000010	31,447	13,103	30.00	-	85	1.50	1.19	3.07	15	002

### LEGENDA Caratteristiche Calcestruzzo Armato

<b>N</b>	Numero identificativo del materiale.
<b><math>\gamma_k</math></b>	Peso specifico.
<b>CdT</b>	Coefficiente di Dilatazione Termica.
<b>E</b>	Modulo elastico normale.
<b>G</b>	Modulo elastico tangenziale.
<b>R<sub>ck</sub></b>	Resistenza caratteristica cubica.
<b>R<sub>cm</sub></b>	Resistenza media cubica.
<b>%R<sub>ck</sub></b>	Percentuale di riduzione della R <sub>ck</sub>
<b><math>\gamma_c</math></b>	Coefficiente di sicurezza allo SLV del materiale.
<b>f<sub>ctd</sub></b>	Resistenza di calcolo a trazione.
<b>f<sub>cfm</sub></b>	Resistenza media a trazione per flessione.
<b>n</b>	Coefficiente di omogeneizzazione.
<b>n Ac</b>	Identificativo, nella relativa tabella materiali, dell'acciaio utilizzato: [-] = parametro NON significativo per il materiale.

## MATERIALI ACCIAIO

Caratteristiche Acciaio													
N	$\gamma_k$	CdT	E	G	$f_{yk,1}$	$f_{yk,2}$	$\gamma_s$	$\gamma_{M1}$	$\gamma_{M2}$	$f_{tk}$	$\gamma_{M3,SLV}$	$\gamma_{M3,SLE}$	$\gamma_{M7}$
	[N/m³]	[1/°C]	[N/mm²]	[N/mm²]	[N/mm²]	[N/mm²]				[N/mm²]			
Acciaio B450C - (B450C)													
002	78.500	0.000010	210.000	80.769	450.00	-	1.15	-	-	-	-	-	-

### LEGENDA Caratteristiche Acciaio

<b>N</b>	Numero identificativo del materiale.
<b><math>\gamma_k</math></b>	Peso specifico.
<b>CdT</b>	Coefficiente di Dilatazione Termica.
<b>E</b>	Modulo elastico normale.
<b>G</b>	Modulo elastico tangenziale.
<b>f<sub>yk,1</sub></b>	Resistenza caratteristica allo snervamento (per profili con t ≤ 40 mm).
<b>f<sub>yk,2</sub></b>	Resistenza caratteristica allo snervamento (per profili con 40 mm < t ≤ 80 mm).
<b><math>\gamma_s</math></b>	Coefficiente di sicurezza allo SLV del materiale.
<b><math>\gamma_{M1}</math></b>	Coefficiente di sicurezza per instabilità.
<b><math>\gamma_{M2}</math></b>	Coefficiente di sicurezza per sezioni tese indebolite.
<b>f<sub>tk</sub></b>	Resistenza a Rottura
<b><math>\gamma_{M3,SLV}</math></b>	Coefficiente di sicurezza a scorrimento alla SLV (Bulloni)
<b><math>\gamma_{M3,SLE}</math></b>	Coefficiente di sicurezza a scorrimento alla SLE (Bulloni).
<b><math>\gamma_{M7}</math></b>	Coefficiente di sicurezza precarico bulloni ad alta resistenza (Bulloni): [-] = parametro NON significativo per il materiale.

## SEZIONI ASTE

Sezioni aste																					
N	Tp	Label	Dimensioni										V	Area	A per Taglio		Inerzia			Δθ Assi Pr.	
			B	H	S.An	L.An	S.AI0	L.AI0	S.AI1	L.AI1	L.AI2	L.AI3			X	Y	X	Torsionale	Y		XY
001	!	60x80	[cm]	[cm]	[cm]	[cm]	[cm]	[cm]	[cm]	[cm]	[cm]	[cm]		[cm²]	[cm²]	[cm²]	[cm⁴]	[cm⁴]	[cm⁴]	[°ssdc]	
			60	80	-	-	-	-	-	-	-	-	4	4,800.00							
002	8	Ø40	40	-	-	-	-	-	-	-	-	-	-	1,256.64	1,130.97	1,130.97	125.664	251.327	125.664	0	0.00

### LEGENDA Sezioni aste

<b>N</b>	Numero identificativo della sezione.
<b>Tp</b>	Identificativo del tipo di sezione.
<b>Label</b>	Identificativo della sezione come indicato nelle carpenterie.
<b>B</b>	Base/Diametro/Raggio.
<b>H</b>	Altezza/Lato/Altezza di colmo.
<b>S.An</b>	Spessore Anima.
<b>L.An</b>	Lunghezza Anima.
<b>S.AI0</b>	Spessore Ala 0.
<b>L.AI0</b>	Lunghezza Ala 0.
<b>S.AI1</b>	Spessore Ala 1.
<b>L.AI1</b>	Lunghezza Ala 1.



Sezioni aste																					
N	Tp	Label	Dimensioni										V	Area	A per Taglio		Inerzia				ΔΘ Assi Pr.
			B	H	S.An	L.An	S.AIO	L.AIO	S.AI1	L.AI1	L.AI2	L.AI3			X	Y	X	Torsionale	Y	XY	
			[cm]	[cm]	[cm]	[cm]	[cm]	[cm]	[cm]	[cm]	[cm]	[cm]		[cm²]	[cm²]	[cm²]	[cm⁴]	[cm⁴]	[cm⁴]	[cm⁴]	[°ssdc]
L.AI2			Lunghezza Ala 2.																		
L.AI3			Lunghezza Ala 3.																		
V			Nel caso di sezioni poligonali, indica il numero dei vertici della sezione.																		
Area			Area della sezione.																		
X, Y			Coppia di assi baricentrici di tipo ortolevogyro con x in direzione orizzontale.																		
Area per Taglio X, Y			Aree della sezione deformabili a Taglio lungo gli assi x e y.																		
Inerzia: X, Torsionale, Y, XY			Inerzie della sezione rispetto agli assi.																		
ΔΘ Assi Pr.			Rotazione degli assi principali d'inerzia rispetto agli assi x, y, espresse in gradi sessadecimali.																		

ANALISI CARICHI

										Analisi carichi
N	Tipo Car.	Descrizione del Carico	Condizione di Carico	Peso proprio Descrizione	PP	Permanente NON Strutturale Descrizione	PNS	Sovraccarico Accidentale Descrizione	SA	Carico neve [N/m <sup>2</sup> ]
001	S	Soletta copertura	Carico Verticale/Coperture	<i>*vedi le relative tabelle dei carichi</i>	-	Pavimento e sottofondo, incidenza dei tramezzi e intonaco inferiore	2,360	Ambienti suscettibili di grande affollamento: musei, sale da ballo, palestre, tribune, sale da concerto, palasport, ecc. (Cat. C3 – Tab. 3.1.II - DM 14.01.2008)	5,000	600
002	S	Platea locale tecnico	Carico Verticale/Abitazioni	<i>*vedi le relative tabelle dei carichi</i>	-	Sottofondo e pavimento di tipo industriale in calcestruzzo	2,000	Biblioteche, archivi, magazzini, depositi, laboratori manifatturieri (Cat. E1 – Tab. 3.1.II - DM 14.01.2008)	6,000	0
003	S	Platea acqua	Carico Verticale/Magazzini	<i>*vedi le relative tabelle dei carichi</i>	-	Sottofondo e pavimento di tipo industriale in calcestruzzo	2,000	Acqua	60,000	0

LEGENDA Analisi carichi

**N** Numero identificativo dell'analisi di carico.

**Tipo Car.** Identificativo del tipo di carico: [S] = Superficiale - [L] = Lineare - [C] = Concentrato.

**PP, PNS, SA** Valori rispettivamente, del Peso Proprio, del Sovraccarico Permanente NON strutturale, del Sovraccarico Accidentale. Secondo il tipo di carico indicato nella colonna "Tipo Carico" ("S" - "L" - "C"), i valori riportati nelle colonne "PP", "PNS" e "SA", devono intendersi espressi in [N/m<sup>2</sup>] per carichi Superficiali, [N/m] per carichi Lineari, [N] per carichi Concentrati.

CONDIZIONI DI CARICO

Condizioni di carico								
N	Condizioni Carico Utente			Tipologia Carico Accidentale				
	Descrizione	AgS	Alt	Descrizione	Durata	ψ 0	ψ 1	ψ 2
0001	Carico Permanente	SI	NO	Carico Permanente	Permanente	1.0	1.0	1.0
0002	Carico Permanente	SI	NO	Permanenti NON Strutturali	Lunga	1.0	1.0	1.0
0003	Carico Verticale	SI	NO	Coperture	Media	0.0	0.0	0.0
0004	Carico da Neve	SI	NO	Carico da Neve <= 1000 m s.l.m.	Breve	0.5	0.2	0.0
0005	Carico Verticale	SI	NO	Abitazioni	Media	0.7	0.5	0.3
0006	Spinta Terreno (statica)	SI	NO	Spinta Terreno (statica)	Lunga	1.0	1.0	1.0
0007	Spinta Terreno (sisma)	SI	NO	Spinta Terreno (sisma)	Istantanea	0.0	0.0	0.0
0008	Carico Verticale	SI	NO	Magazzini	Lunga	1.0	0.9	0.8

LEGENDA Condizioni di carico

**N** Numero identificativo della condizione di carico.

**AgS** Indica se la condizione di carico considerata è Agente con il Sisma.

**Alt** Indica se la condizione di carico è Alternata (cioè considerata due volte con segno opposto) o meno.

**Durata** Indica la classe di durata del carico.

NOTA: questo dato è significativo solo per elementi in materiale legnoso.

**ψ 0** Coefficiente riduttivo dei carichi allo SLU e SLE (Carichi rari).

**ψ 1** Coefficiente riduttivo dei carichi allo SLE (Carichi frequenti).

**ψ 2** Coefficiente riduttivo dei carichi allo SLE (Carichi frequenti e quasi permanenti).

SLE: COMBINAZIONE DI AZIONI QUASI PERMANENTE - COEFFICIENTI

SLE: Combinazione di azioni Quasi permanente - Coefficienti									
CC 01	CC 02	CC 03	CC 04	CC 05	CC 06	CC 07	CC 08		
Carico	Carico	Carico	Carico da	Carico	Spinta Terreno	Spinta Terreno	Carico		
Permanente	Permanente/Permanenti NON Strutturali	Verticale/Coperture	Neve/Carico da Neve <= 1000 m s.l.m.	Verticale/Abitazioni	(statica)	(sisma)	Verticale/Magazzini		
<b>01</b>	1.00	1.00	0.00	0.00	0.30	1.00	0.00	0.80	

LEGENDA SLE: Combinazione di azioni Quasi permanente - Coefficienti

**COMB.** Numero identificativo della Combinazione di Carico.

**CC** Condizione di carico considerata.

CC 01= Carico Permanente



SLE: Combinazione di azioni Quasi permanente - Coefficienti

COMB.	CC 01 Carico Permanente	CC 02 Carico Permanente/Pe rmanenti NON Strutturali	CC 03 Carico Verticale/Coper ture	CC 04 Carico da Neve/Carico da Neve <= 1000 m s.l.m.	CC 05 Carico Verticale/Abitaz ioni	CC 06 Spinta Terreno (statica)	CC 07 Spinta Terreno (sisma)	CC 08 Carico Verticale/Magaz zini
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CC 02= Carico Permanente/Permanenti NON Strutturali  
 CC 03= Carico Verticale/Coperture  
 CC 04= Carico da Neve/Carico da Neve <= 1000 m s.l.m.  
 CC 05= Carico Verticale/Abitazioni  
 CC 06= Spinta Terreno (statica)  
 CC 07= Spinta Terreno (sisma)  
 CC 08= Carico Verticale/Magazzini

## SLE: COMBINAZIONE DI AZIONI FREQUENTE - COEFFICIENTI

SLE: Combinazione di azioni Frequente - Coefficienti

COMB.	CC 01 Carico Permanente	CC 02 Carico Permanente/Pe rmanenti NON Strutturali	CC 03 Carico Verticale/Coper ture	CC 04 Carico da Neve/Carico da Neve <= 1000 m s.l.m.	CC 05 Carico Verticale/Abitaz ioni	CC 06 Spinta Terreno (statica)	CC 07 Spinta Terreno (sisma)	CC 08 Carico Verticale/Magaz zini
01	1.00	1.00	0.00	0.00	0.30	1.00	0.00	0.80
02	1.00	1.00	0.00	0.20	0.30	1.00	0.00	0.80
03	1.00	1.00	0.00	0.00	0.50	1.00	0.00	0.80
04	1.00	1.00	0.00	0.00	0.30	1.00	0.00	0.90

### LEGENDA SLE: Combinazione di azioni Frequente - Coefficienti

**COMB.** Numero identificativo della Combinazione di Carico.  
**CC** Condizione di carico considerata.  
 CC 01= Carico Permanente  
 CC 02= Carico Permanente/Permanenti NON Strutturali  
 CC 03= Carico Verticale/Coperture  
 CC 04= Carico da Neve/Carico da Neve <= 1000 m s.l.m.  
 CC 05= Carico Verticale/Abitazioni  
 CC 06= Spinta Terreno (statica)  
 CC 07= Spinta Terreno (sisma)  
 CC 08= Carico Verticale/Magazzini

## SLE: COMBINAZIONE DI AZIONI RARA - COEFFICIENTI

SLE: Combinazione di azioni Rara - Coefficienti

COMB.	CC 01 Carico Permanente	CC 02 Carico Permanente/Pe rmanenti NON Strutturali	CC 03 Carico Verticale/Coper ture	CC 04 Carico da Neve/Carico da Neve <= 1000 m s.l.m.	CC 05 Carico Verticale/Abitaz ioni	CC 06 Spinta Terreno (statica)	CC 07 Spinta Terreno (sisma)	CC 08 Carico Verticale/Magaz zini
01	1.00	1.00	1.00	0.50	0.70	1.00	0.00	1.00
02	1.00	1.00	0.00	1.00	0.70	1.00	0.00	1.00
03	1.00	1.00	0.00	0.50	1.00	1.00	0.00	1.00
04	1.00	1.00	0.00	0.50	0.70	1.00	0.00	1.00

### LEGENDA SLE: Combinazione di azioni Rara - Coefficienti

**COMB.** Numero identificativo della Combinazione di Carico.  
**CC** Condizione di carico considerata.  
 CC 01= Carico Permanente  
 CC 02= Carico Permanente/Permanenti NON Strutturali  
 CC 03= Carico Verticale/Coperture  
 CC 04= Carico da Neve/Carico da Neve <= 1000 m s.l.m.  
 CC 05= Carico Verticale/Abitazioni  
 CC 06= Spinta Terreno (statica)  
 CC 07= Spinta Terreno (sisma)  
 CC 08= Carico Verticale/Magazzini

## SLU: COMBINAZIONI DI CARICO IN ASSENZA DI SISMA - COEFFICIENTI

SLU: Combinazioni di carico in assenza di sisma - Coefficienti

COMB.	CC 01 Carico Permanente	CC 02 Carico Permanente/Pe rmanenti NON Strutturali	CC 03 Carico Verticale/Coper ture	CC 04 Carico da Neve/Carico da Neve <= 1000 m s.l.m.	CC 05 Carico Verticale/Abitaz ioni	CC 06 Spinta Terreno (statica)	CC 07 Spinta Terreno (sisma)	CC 08 Carico Verticale/Magaz zini
01	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00
02	1.00	1.00	0.00	0.00	0.00	0.00	0.00	1.50
03	1.00	1.00	0.00	0.00	0.00	1.50	0.00	0.00
04	1.00	1.00	0.00	0.00	0.00	1.50	0.00	1.50
05	1.00	1.00	0.00	0.00	1.05	0.00	0.00	0.00
06	1.00	1.00	0.00	0.00	1.05	0.00	0.00	1.50
07	1.00	1.00	0.00	0.00	1.05	1.50	0.00	0.00
08	1.00	1.00	0.00	0.00	1.05	1.50	0.00	1.50



COMB.	CC 01 Carico Permanente	CC 02 Carico Permanente/Pe rmanenti NON Strutturali	CC 03 Carico Verticale/Coper ture	CC 04 Carico da Neve/Carico da Neve <= 1000 m s.l.m.	CC 05 Carico Verticale/Abitaz ioni	CC 06 Spinta Terreno (statica)	CC 07 Spinta Terreno (sisma)	CC 08 Carico Verticale/Magaz zini
09	1.00	1.00	0.00	0.75	0.00	0.00	0.00	0.00
10	1.00	1.00	0.00	0.75	0.00	0.00	0.00	1.50
11	1.00	1.00	0.00	0.75	0.00	1.50	0.00	0.00
12	1.00	1.00	0.00	0.75	0.00	1.50	0.00	1.50
13	1.00	1.00	0.00	0.75	1.05	0.00	0.00	0.00
14	1.00	1.00	0.00	0.75	1.05	0.00	0.00	1.50
15	1.00	1.00	0.00	0.75	1.05	1.50	0.00	0.00
16	1.00	1.00	0.00	0.75	1.05	1.50	0.00	1.50
17	1.00	1.00	1.50	0.00	0.00	0.00	0.00	0.00
18	1.00	1.00	1.50	0.00	0.00	0.00	0.00	1.50
19	1.00	1.00	1.50	0.00	0.00	1.50	0.00	0.00
20	1.00	1.00	1.50	0.00	0.00	1.50	0.00	1.50
21	1.00	1.00	1.50	0.00	1.05	0.00	0.00	0.00
22	1.00	1.00	1.50	0.00	1.05	0.00	0.00	1.50
23	1.00	1.00	1.50	0.00	1.05	1.50	0.00	0.00
24	1.00	1.00	1.50	0.00	1.05	1.50	0.00	1.50
25	1.00	1.00	1.50	0.75	0.00	0.00	0.00	0.00
26	1.00	1.00	1.50	0.75	0.00	0.00	0.00	1.50
27	1.00	1.00	1.50	0.75	0.00	1.50	0.00	0.00
28	1.00	1.00	1.50	0.75	0.00	1.50	0.00	1.50
29	1.00	1.00	1.50	0.75	1.05	0.00	0.00	0.00
30	1.00	1.00	1.50	0.75	1.05	0.00	0.00	1.50
31	1.00	1.00	1.50	0.75	1.05	1.50	0.00	0.00
32	1.00	1.00	1.50	0.75	1.05	1.50	0.00	1.50
33	1.00	1.00	0.00	1.50	0.00	0.00	0.00	0.00
34	1.00	1.00	0.00	1.50	0.00	0.00	0.00	1.50
35	1.00	1.00	0.00	1.50	0.00	1.50	0.00	0.00
36	1.00	1.00	0.00	1.50	0.00	1.50	0.00	1.50
37	1.00	1.00	0.00	1.50	1.05	0.00	0.00	0.00
38	1.00	1.00	0.00	1.50	1.05	0.00	0.00	1.50
39	1.00	1.00	0.00	1.50	1.05	1.50	0.00	0.00
40	1.00	1.00	0.00	1.50	1.05	1.50	0.00	1.50
41	1.00	1.00	0.00	0.00	1.50	0.00	0.00	0.00
42	1.00	1.00	0.00	0.00	1.50	0.00	0.00	1.50
43	1.00	1.00	0.00	0.00	1.50	1.50	0.00	0.00
44	1.00	1.00	0.00	0.00	1.50	1.50	0.00	1.50
45	1.00	1.00	0.00	0.75	1.50	0.00	0.00	0.00
46	1.00	1.00	0.00	0.75	1.50	0.00	0.00	1.50
47	1.00	1.00	0.00	0.75	1.50	1.50	0.00	0.00
48	1.00	1.00	0.00	0.75	1.50	1.50	0.00	1.50
49	1.30	1.30	0.00	0.00	0.00	0.00	0.00	0.00
50	1.30	1.30	0.00	0.00	0.00	0.00	0.00	1.50
51	1.30	1.30	0.00	0.00	0.00	1.50	0.00	0.00
52	1.30	1.30	0.00	0.00	0.00	1.50	0.00	1.50
53	1.30	1.30	0.00	0.00	1.05	0.00	0.00	0.00
54	1.30	1.30	0.00	0.00	1.05	0.00	0.00	1.50
55	1.30	1.30	0.00	0.00	1.05	1.50	0.00	0.00
56	1.30	1.30	0.00	0.00	1.05	1.50	0.00	1.50
57	1.30	1.30	0.00	0.75	0.00	0.00	0.00	0.00
58	1.30	1.30	0.00	0.75	0.00	0.00	0.00	1.50
59	1.30	1.30	0.00	0.75	0.00	1.50	0.00	0.00
60	1.30	1.30	0.00	0.75	0.00	1.50	0.00	1.50
61	1.30	1.30	0.00	0.75	1.05	0.00	0.00	0.00
62	1.30	1.30	0.00	0.75	1.05	0.00	0.00	1.50
63	1.30	1.30	0.00	0.75	1.05	1.50	0.00	0.00
64	1.30	1.30	0.00	0.75	1.05	1.50	0.00	1.50
65	1.30	1.30	1.50	0.00	0.00	0.00	0.00	0.00
66	1.30	1.30	1.50	0.00	0.00	0.00	0.00	1.50
67	1.30	1.30	1.50	0.00	0.00	1.50	0.00	0.00
68	1.30	1.30	1.50	0.00	0.00	1.50	0.00	1.50
69	1.30	1.30	1.50	0.00	1.05	0.00	0.00	0.00
70	1.30	1.30	1.50	0.00	1.05	0.00	0.00	1.50
71	1.30	1.30	1.50	0.00	1.05	1.50	0.00	0.00
72	1.30	1.30	1.50	0.00	1.05	1.50	0.00	1.50
73	1.30	1.30	1.50	0.75	0.00	0.00	0.00	0.00
74	1.30	1.30	1.50	0.75	0.00	0.00	0.00	1.50
75	1.30	1.30	1.50	0.75	0.00	1.50	0.00	0.00
76	1.30	1.30	1.50	0.75	0.00	1.50	0.00	1.50



COMB.	CC 01 Carico Permanente	CC 02 Carico Permanente/Pe rmanenti NON Strutturali	CC 03 Carico Verticale/Coper ture	CC 04 Carico da Neve/Carico da Neve <= 1000 m s.l.m.	CC 05 Carico Verticale/Abitaz ioni	CC 06 Spinta Terreno (statica)	CC 07 Spinta Terreno (sisma)	CC 08 Carico Verticale/Magaz zini
77	1.30	1.30	1.50	0.75	1.05	0.00	0.00	0.00
78	1.30	1.30	1.50	0.75	1.05	0.00	0.00	1.50
79	1.30	1.30	1.50	0.75	1.05	1.50	0.00	0.00
80	1.30	1.30	1.50	0.75	1.05	1.50	0.00	1.50
81	1.30	1.30	0.00	1.50	0.00	0.00	0.00	0.00
82	1.30	1.30	0.00	1.50	0.00	0.00	0.00	1.50
83	1.30	1.30	0.00	1.50	0.00	1.50	0.00	0.00
84	1.30	1.30	0.00	1.50	0.00	1.50	0.00	1.50
85	1.30	1.30	0.00	1.50	1.05	0.00	0.00	0.00
86	1.30	1.30	0.00	1.50	1.05	0.00	0.00	1.50
87	1.30	1.30	0.00	1.50	1.05	1.50	0.00	0.00
88	1.30	1.30	0.00	1.50	1.05	1.50	0.00	1.50
89	1.30	1.30	0.00	0.00	1.50	0.00	0.00	0.00
90	1.30	1.30	0.00	0.00	1.50	0.00	0.00	1.50
91	1.30	1.30	0.00	0.00	1.50	1.50	0.00	0.00
92	1.30	1.30	0.00	0.00	1.50	1.50	0.00	1.50
93	1.30	1.30	0.00	0.75	1.50	0.00	0.00	0.00
94	1.30	1.30	0.00	0.75	1.50	0.00	0.00	1.50
95	1.30	1.30	0.00	0.75	1.50	1.50	0.00	0.00
96	1.30	1.30	0.00	0.75	1.50	1.50	0.00	1.50

## LEGENDA SLU: Combinazioni di carico in assenza di sisma - Coefficienti

**COMB.** Numero identificativo della Combinazione di Carico.  
**CC** Condizione di carico considerata.  
 CC 01= Carico Permanente  
 CC 02= Carico Permanente/Permanenti NON Strutturali  
 CC 03= Carico Verticale/Coperture  
 CC 04= Carico da Neve/Carico da Neve <= 1000 m s.l.m.  
 CC 05= Carico Verticale/Abitazioni  
 CC 06= Spinta Terreno (statica)  
 CC 07= Spinta Terreno (sisma)  
 CC 08= Carico Verticale/Magazzini

## SLU: COMBINAZIONI DI CARICO IN PRESENZA DI SISMA - COEFFICIENTI

COMB.	CC 01 Carico Permanente	CC 02 Carico Permanente/Pe rmanenti NON Strutturali	CC 03 Carico Verticale/Coper ture	CC 04 Carico da Neve/Carico da Neve <= 1000 m s.l.m.	CC 05 Carico Verticale/Abitaz ioni	CC 06 Spinta Terreno (statica)	CC 07 Spinta Terreno (sisma)	CC 08 Carico Verticale/Magaz zini
01	1.00	1.00	0.00	0.00	0.30	1.00	1.00	0.80

## LEGENDA SLU: Combinazioni di carico in presenza di sisma - Coefficienti

**COMB.** Numero identificativo della Combinazione di Carico.  
**CC** Condizione di carico considerata.  
 CC 01= Carico Permanente  
 CC 02= Carico Permanente/Permanenti NON Strutturali  
 CC 03= Carico Verticale/Coperture  
 CC 04= Carico da Neve/Carico da Neve <= 1000 m s.l.m.  
 CC 05= Carico Verticale/Abitazioni  
 CC 06= Spinta Terreno (statica)  
 CC 07= Spinta Terreno (sisma)  
 CC 08= Carico Verticale/Magazzini

## D.M. 14-01-2008

Alle combinazioni riportate nella precedente tabella è stato aggiunto l'effetto del sisma secondo la formula (3.2.16) riportata al punto 3.2.4 del D.M. 14-01-2008. L'azione sismica è stata considerata come caratterizzata da tre componenti traslazionali lungo i tre assi globali X, Y e Z; la risposta della struttura è stata calcolata separatamente per i tre effetti e quindi combinata secondo la seguente espressione simbolica:

$$\alpha = \alpha_i + 0.3 * \alpha_{ii} + 0.3 * \alpha_{iii}$$

con  $\alpha$  effetto totale dell'azione sismica,  $\alpha_i$ ,  $\alpha_{ii}$  e  $\alpha_{iii}$  azioni sismiche nelle tre direzioni. E' stata effettuata una rotazione degli indici e dei segni, per cui le combinazioni totali generate sono le :

(con  $\alpha'_p$  sollecitazione dovuta alla combinazione delle condizioni statiche e  $\alpha$  sollecitazione dovuta al sisma; in particolare  $\alpha_x, \alpha_y, \alpha_z, \alpha_{ex}, \alpha_{ey}$  sono rispettivamente le sollecitazioni dovute al sisma agente in direzione x, in direzione y, in direzione z, per eccentricità accidentale positiva in direzione x e per eccentricità accidentale positiva in direzione y)

**1)**  $\alpha'_p + (\alpha_x + \alpha_{ex}) + 0.3 * (\alpha_y + \alpha_{ey}) + 0.3 * (\alpha_z)$ ; **2)**  $\alpha'_p + (\alpha_x + \alpha_{ex}) - 0.3 * (\alpha_y + \alpha_{ey}) + 0.3 * (\alpha_z)$ ; **3)**  $\alpha'_p + (\alpha_x + \alpha_{ex}) + 0.3 * (\alpha_y + \alpha_{ey}) - 0.3 * (\alpha_z)$ ; **4)**  $\alpha'_p + (\alpha_x + \alpha_{ex}) - 0.3 * (\alpha_y + \alpha_{ey}) - 0.3 * (\alpha_z)$ ; **5)**  $\alpha'_p + (\alpha_x + \alpha_{ex}) + 0.3 * (\alpha_y - \alpha_{ey}) + 0.3 * (\alpha_z)$ ; **6)**  $\alpha'_p + (\alpha_x + \alpha_{ex}) - 0.3 * (\alpha_y - \alpha_{ey}) + 0.3 * (\alpha_z)$ ; **7)**  $\alpha'_p + (\alpha_x + \alpha_{ex}) + 0.3 * (\alpha_y - \alpha_{ey}) - 0.3 * (\alpha_z)$ ; **8)**  $\alpha'_p + (\alpha_x + \alpha_{ex}) - 0.3 * (\alpha_y - \alpha_{ey}) - 0.3 * (\alpha_z)$ ; **9)**  $\alpha'_p + (\alpha_x + \alpha_{ex}) + 0.3 * (-\alpha_y + \alpha_{ey}) + 0.3 * (\alpha_z)$ ; **10)**  $\alpha'_p + (\alpha_x + \alpha_{ex}) - 0.3 * (-\alpha_y + \alpha_{ey}) + 0.3 * (\alpha_z)$ ; **11)**  $\alpha'_p + (\alpha_x - \alpha_{ex}) + 0.3 * (-\alpha_y + \alpha_{ey}) - 0.3 * (\alpha_z)$ ; **12)**  $\alpha'_p + (\alpha_x - \alpha_{ex}) - 0.3 * (-\alpha_y + \alpha_{ey}) - 0.3 * (\alpha_z)$ ; **13)**  $\alpha'_p + (\alpha_x - \alpha_{ex}) + 0.3 * (\alpha_y - \alpha_{ey}) + 0.3 * (\alpha_z)$ ; **14)**  $\alpha'_p + (\alpha_x - \alpha_{ex}) - 0.3 * (\alpha_y - \alpha_{ey}) + 0.3 * (\alpha_z)$ ; **15)**  $\alpha'_p + (\alpha_x - \alpha_{ex}) + 0.3 * (\alpha_y - \alpha_{ey}) - 0.3 * (\alpha_z)$ ; **16)**  $\alpha'_p + (\alpha_x - \alpha_{ex}) - 0.3 * (\alpha_y - \alpha_{ey}) - 0.3 * (\alpha_z)$ ; **17)**



$\alpha'_p + (\alpha_y + \alpha_{ey}) + 0.3 * (\alpha_x + \alpha_{ex}) + 0.3 * (\alpha_z);$ <b>18)</b> $\alpha'_p + (\alpha_y + \alpha_{ey}) - 0.3 * (\alpha_x + \alpha_{ex}) + 0.3 * (\alpha_z);$ <b>19)</b> $\alpha'_p + (\alpha_y + \alpha_{ey}) + 0.3 * (\alpha_x + \alpha_{ex}) - 0.3 * (\alpha_z);$ <b>20)</b> $\alpha'_p + (\alpha_y + \alpha_{ey}) - 0.3 * (\alpha_x + \alpha_{ex}) - 0.3 * (\alpha_z);$ <b>21)</b> $\alpha'_p + (\alpha_y + \alpha_{ey}) + 0.3 * (\alpha_x - \alpha_{ex}) + 0.3 * (\alpha_z);$ <b>22)</b> $\alpha'_p + (\alpha_y + \alpha_{ey}) - 0.3 * (\alpha_x - \alpha_{ex}) + 0.3 * (\alpha_z);$ <b>23)</b> $\alpha'_p + (\alpha_y + \alpha_{ey}) + 0.3 * (\alpha_x - \alpha_{ex}) - 0.3 * (\alpha_z);$ <b>24)</b> $\alpha'_p + (\alpha_y + \alpha_{ey}) - 0.3 * (\alpha_x - \alpha_{ex}) - 0.3 * (\alpha_z);$ <b>25)</b> $\alpha'_p + (\alpha_y - \alpha_{ey}) + 0.3 * (\alpha_x + \alpha_{ex}) + 0.3 * (\alpha_z);$ <b>26)</b> $\alpha'_p + (\alpha_y - \alpha_{ey}) - 0.3 * (\alpha_x + \alpha_{ex}) + 0.3 * (\alpha_z);$ <b>27)</b> $\alpha'_p + (\alpha_y - \alpha_{ey}) + 0.3 * (\alpha_x - \alpha_{ex}) + 0.3 * (\alpha_z);$ <b>28)</b> $\alpha'_p + (\alpha_y - \alpha_{ey}) - 0.3 * (\alpha_x - \alpha_{ex}) + 0.3 * (\alpha_z);$ <b>29)</b> $\alpha'_p + (\alpha_y - \alpha_{ey}) + 0.3 * (\alpha_x - \alpha_{ex}) - 0.3 * (\alpha_z);$ <b>30)</b> $\alpha'_p + (\alpha_y - \alpha_{ey}) - 0.3 * (\alpha_x - \alpha_{ex}) - 0.3 * (\alpha_z);$ <b>31)</b> $\alpha'_p + (\alpha_y + \alpha_{ey}) + 0.3 * (\alpha_x - \alpha_{ex}) - 0.3 * (\alpha_z);$ <b>32)</b> $\alpha'_p + (\alpha_y - \alpha_{ey}) - 0.3 * (\alpha_x - \alpha_{ex}) - 0.3 * (\alpha_z);$ <b>33)</b> $\alpha'_p + \alpha_z + 0.3 * (\alpha_x + \alpha_{ex}) + 0.3 * (\alpha_y + \alpha_{ey});$ <b>34)</b> $\alpha'_p + \alpha_z - 0.3 * (\alpha_x + \alpha_{ex}) + 0.3 * (\alpha_y + \alpha_{ey});$ <b>35)</b> $\alpha'_p + \alpha_z + 0.3 * (\alpha_x + \alpha_{ex}) - 0.3 * (\alpha_y + \alpha_{ey});$ <b>36)</b> $\alpha'_p + \alpha_z - 0.3 * (\alpha_x + \alpha_{ex}) - 0.3 * (\alpha_y + \alpha_{ey});$ <b>37)</b> $\alpha'_p + \alpha_z + 0.3 * (\alpha_x - \alpha_{ex}) + 0.3 * (\alpha_y - \alpha_{ey});$ <b>38)</b> $\alpha'_p + \alpha_z - 0.3 * (\alpha_x - \alpha_{ex}) + 0.3 * (\alpha_y - \alpha_{ey});$ <b>39)</b> $\alpha'_p + \alpha_z + 0.3 * (\alpha_x + \alpha_{ex}) - 0.3 * (\alpha_y - \alpha_{ey});$ <b>40)</b> $\alpha'_p + \alpha_z - 0.3 * (\alpha_x + \alpha_{ex}) - 0.3 * (\alpha_y - \alpha_{ey});$ <b>41)</b> $\alpha'_p + \alpha_z + 0.3 * (\alpha_x - \alpha_{ex}) + 0.3 * (\alpha_y + \alpha_{ey});$ <b>42)</b> $\alpha'_p + \alpha_z - 0.3 * (\alpha_x - \alpha_{ex}) + 0.3 * (\alpha_y + \alpha_{ey});$ <b>43)</b> $\alpha'_p + \alpha_z + 0.3 * (\alpha_x - \alpha_{ex}) - 0.3 * (\alpha_y + \alpha_{ey});$ <b>44)</b> $\alpha'_p + \alpha_z - 0.3 * (\alpha_x - \alpha_{ex}) - 0.3 * (\alpha_y + \alpha_{ey});$ <b>45)</b> $\alpha'_p + \alpha_z + 0.3 * (\alpha_x - \alpha_{ex}) + 0.3 * (\alpha_y - \alpha_{ey});$ <b>46)</b> $\alpha'_p + \alpha_z - 0.3 * (\alpha_x - \alpha_{ex}) + 0.3 * (\alpha_y - \alpha_{ey});$ <b>47)</b> $\alpha'_p + \alpha_z + 0.3 * (\alpha_x - \alpha_{ex}) - 0.3 * (\alpha_y - \alpha_{ey});$ <b>48)</b> $\alpha'_p + \alpha_z - 0.3 * (\alpha_x - \alpha_{ex}) - 0.3 * (\alpha_y - \alpha_{ey}).$
<p>Nel caso di verifiche effettuate con sollecitazioni composte, per tenere conto del fatto che le sollecitazioni sismiche sono state ricavate come CQC delle sollecitazioni derivanti dai modi di vibrazione, dette N, Mx, My, Tx e Ty le sollecitazioni dovute al sisma, per ognuna delle combinazioni precedenti, sono state ricavate 32 combinazioni di carico permutando nel seguente modo i segni delle sollecitazioni derivanti dal sisma:</p> <p><b>1)</b> N, Mx, My, Tx e Ty; <b>2)</b> N, Mx, -My, Tx e Ty; <b>3)</b> N, -Mx, My, Tx e Ty; <b>4)</b> N, -Mx, -My, Tx e Ty; <b>5)</b> -N, Mx, My, Tx e Ty; <b>6)</b> -N, Mx, -My, Tx e Ty; <b>7)</b> -N, -Mx, My, Tx e Ty; <b>8)</b> -N, -Mx, -My, Tx e Ty; <b>9)</b> N, Mx, My, Tx e -Ty; <b>10)</b> N, Mx, -My, Tx e -Ty; <b>11)</b> N, -Mx, My, Tx e -Ty; <b>12)</b> N, -Mx, -My, Tx e -Ty; <b>13)</b> -N, Mx, My, Tx e -Ty; <b>14)</b> -N, Mx, -My, Tx e -Ty; <b>15)</b> -N, -Mx, My, Tx e -Ty; <b>16)</b> -N, -Mx, -My, Tx e -Ty; <b>17)</b> N, Mx, My, -Tx e Ty; <b>18)</b> N, Mx, -My, -Tx e Ty; <b>19)</b> N, -Mx, My, -Tx e Ty; <b>20)</b> N, -Mx, -My, -Tx e Ty; <b>21)</b> -N, Mx, My, -Tx e Ty; <b>22)</b> -N, Mx, -My, -Tx e Ty; <b>23)</b> -N, -Mx, My, -Tx e Ty; <b>24)</b> -N, -Mx, -My, -Tx e Ty; <b>25)</b> N, Mx, My, -Tx e -Ty; <b>26)</b> N, Mx, -My, -Tx e -Ty; <b>27)</b> N, -Mx, My, -Tx e -Ty; <b>28)</b> N, -Mx, -My, -Tx e -Ty; <b>29)</b> -N, Mx, My, -Tx e -Ty; <b>30)</b> -N, Mx, -My, -Tx e -Ty; <b>31)</b> -N, -Mx, My, -Tx e -Ty; <b>32)</b> -N, -Mx, -My, -Tx e -Ty.</p>

## DATI GENERALI ANALISI SISMICA

Dati generali analisi sismica												
Ang	NV	CD	MP	S	Mcm	PAc	EcA	IrT	TP	RP	RH	CVE
[ssdc]												
0	45	B	ca	P	N	A	N	N	C	SI	NO	5

### Fattori di struttura

Dir. X			Dir. Y			Dir. Z	
q	$\alpha_u/\alpha_1$	Kw	q	$\alpha_u/\alpha_1$	Kw	q	
2.64	1.10	1.00	2.64	1.10	1.00	1.50	

Stato Limite	Tr	Ag/g	Amplif. Stratigrafica		F0	T <sup>c</sup>	Tb	Tc	Td
			Ss	Cc					
	[anni]	[adim]	[adim]	[adim]	[adim]	[s]	[s]	[s]	[s]
SLO	45	0.0577	1.500	1.554	2.333	0.305	0.158	0.474	1.831
SLD	75	0.0758	1.500	1.527	2.329	0.321	0.164	0.491	1.903
SLV	712	0.1942	1.418	1.494	2.422	0.344	0.171	0.513	2.377
SLC	1462	0.2419	1.336	1.489	2.509	0.347	0.172	0.517	2.568

Classe Edificio	Vita Nominale	Periodo di Riferimento	Latitudine	Longitudine	Altitudine	Ampl. Topog.	
						Categoria	Coefficiente
	[anni]	[anni]	[°ssdc]	[°ssdc]	[m]		
3	50	75	40.8775	14.3419	25	T1	1.00

## LEGENDA Dati generali analisi sismica

<b>Ang</b>	Direzione di una componente dell'azione sismica rispetto all'asse X (sistema di riferimento globale); la seconda componente dell'azione sismica e' assunta con direzione ruotata di 90 gradi rispetto alla prima.
<b>NV</b>	Nel caso di analisi dinamica, indica il numero di modi di vibrazione considerati.
<b>CD</b>	Classe di duttilita': [A] = Alta - [B] = Bassa - [ND] = Non Dissipativa - [-] = Nessuna.
<b>MP</b>	Tipo di materiale prevalente nella struttura: [ca] = calcestruzzo armato - [muOld] = muratura esistente - [muNew] = muratura nuova - [muArm] = muratura armata - [ac] = acciaio.
<b>S</b>	Tipologia della struttura: Cemento armato: [T] = Telaio - [P] = Pareti - [2P] = Due pareti per direzione non accoppiate - [DT] = Deformabili torsionalmente - [PI] = Pendolo inverso; Muratura: [P] = un solo piano - [PP] = più di un piano; Acciaio: [T] = Telaio - [CT] = controventi concentrici diagonale tesa - [CV] = controventi concentrici a V - [M] = mensola o pendolo invertito - [TT] = telaio con tamponature.
<b>Mcm</b>	Struttura con telai multicampata: [N]=Nessuna direzione - [X]=Solo in direzione X - [Y]=Solo in direzione Y - [XY]=Sia in direzione X che Y.
<b>PAc</b>	Presenza nella struttura di pareti accoppiate: [P] = presenti - [A] = Assenti
<b>EcA</b>	Eccentricita' accidentale: [S] = considerata come condizione di carico statica aggiuntiva - [N] = Considerata come incremento delle sollecitazioni.
<b>IrT</b>	Irregolarita' tamponature in pianta: [S] = Tamponature irregolari in pianta - [N] = Tamponature regolari in pianta.
<b>TP</b>	Tipo terreno prevalente, categoria di suolo di fondazione come definito al punto 3.2.2 del DM 14 gennaio 2008 'Nuove Norme tecniche per le costruzioni: [A] = Ammassi rocciosi affioranti o terreni molto rigidi - [B] = Rocce tenere e depositi di terreni a grana grossa molto addensati o terreni a grana fina molto consistenti - [C] = Depositati di terreni a grana grossa mediamente addensati o terreni a grana fina mediamente consistenti - [D] = Depositati di terreni a grana grossa scarsamente addensati o di terreni a grana fina scarsamente consistenti - [E] = Terreni dei sottosuoli di tipo C o D per spessore non superiore a 20 m.
<b>RP</b>	Regolarita' in pianta: [S]= Struttura regolare - [N]=Struttura non regolare.
<b>RH</b>	Regolarita' in altezza: [S]= Struttura regolare - [N]=Struttura non regolare.
<b>CVE</b>	Coefficiente viscoso equivalente.
<b>Classe</b>	Classe dell'edificio.



Classe Edificio	Vita Nominale	Periodo di Riferimento	Latitudine	Longitudine	Altitudine	Ampl. Topog.	
						Categoria	Coefficiente
	[anni]	[anni]	[°ssdc]	[°ssdc]	[m]		

#### Edificio

#### Categ

Categoria topografica. (Vedi NOTE)

#### Topog

#### Coef Ampl

Coefficiente di amplificazione topografica.

#### Topog

#### Tr

Periodo di ritorno dell'azione sismica.

#### Ag/g

Coefficiente di accelerazione al suolo.

#### Ss

Coefficienti di Amplificazione Stratigrafica allo SLO / SLD / SLV / SLC.

#### Cc

Coefficienti di Amplificazione di Tc allo SLO / SLD / SLV / SLC.

#### F0

Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale.

#### T\*c

Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale.

#### Tb

Periodo di inizio del tratto accelerazione costante dello spettro di progetto.

#### Tc

Periodo di inizio del tratto a velocità costante dello spettro di progetto.

#### Td

Periodo di inizio del tratto a spostamento costante dello spettro di progetto.

#### Latitudine

Latitudine geografica del sito (in datum ED50).

#### Longitudi

Longitudine geografica del sito (in datum ED50).

#### ne

#### Altitudine

Altitudine geografica del sito.

#### q

Fattore di riduzione dello spettro di risposta sismico allo SLU (Fattore di struttura).

#### α/α1

Rapporto di sovrarresistenza.

#### Kw

Fattore di riduzione di q0.

#### NOTE

[-] = Parametro non significativo per il tipo di calcolo effettuato

Categoria topografica

T1: Superficie pianeggiante, pendii e rilievi isolati con inclinazione media  $i = 15^\circ$

T2: Pendii con inclinazione media  $i > 15^\circ$

T3: Rilievi con larghezza in cresta molto minore che alla base e inclinazione media  $15^\circ = i = 30^\circ$

T4: Rilievi con larghezza in cresta molto minore che alla base e inclinazione media  $i > 30^\circ$

## PRINCIPALI ELEMENTI ANALISI SISMICA

Dir sisma	M.S	M.SLU	M.Ecc.SLU	M.SLD	M.Ecc.SLD	P.T.M.Ecc	R.SLU
	[N-s²/m]	[N-s²/m]	[N-s²/m]	[N-s²/m]	[N-s²/m]	[%]	[N]
X	1,699,244	730,507	684,907	730,507	684,907	93.8	1,923,308
Y	1,699,244	730,507	653,301	730,507	653,301	89.4	1,929,121
Z	1,699,244	0	0	0	0	100.0	0

### LEGENDA Principali elementi analisi sismica

#### Dir sisma

Direzione del sisma: [X] = Sisma in direzione X - [Y] = Sisma in direzione Y - [Z] = Sisma in direzione Z.

#### M.S

Massa complessiva della struttura.

#### M.SLU

Massa eccitabile della struttura allo S.L. Ultimo, nelle direzioni X, Y, Z.

#### M.Ecc.SLU

Massa Eccitata dal sisma allo S.L. Ultimo.

#### M.SLD

Massa eccitabile della struttura allo S.L. di Danno, nelle direzioni X, Y, Z.

#### M.Ecc.SLD

Massa Eccitata dal sisma allo S.L. di Danno.

#### P.T.M.Ecc

Percentuale Totale di Masse Eccitate dal sisma.

#### R.SLU

Reazioni Totali (S.L. Ultimo).

## RIEPILOGO MODI DI VIBRAZIONE Modi di vibrazione considerati: n.45

Spettro	Periodo	As.O	As.V	C.Part	C.Mod	P.M.M	M.Ec
	[s]	[m/s²]	[m/s²]			[%]	[N-s²/m]
<b>Modo Vibrazione n. 1</b>							
SLU-X	0.046	2.641	0.000	-5.3806	-0.0003	0.0	29
SLU-Y	0.046	2.641	0.000	633.7044	0.0338	55.0	401,581
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.046	1.531	0.000	-5.3806	-0.0003	0.0	29
SLD-Y	0.046	1.531	0.000	633.7044	0.0338	55.0	401,581
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.730	0.000	-	-	-	-
Elast-Y	-	3.730	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 2</b>							
SLU-X	0.052	2.633	0.000	-583.2102	-0.0399	46.6	340,134
SLU-Y	0.052	2.633	0.000	-4.2666	-0.0003	0.0	18
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.052	1.586	0.000	-583.2102	-0.0399	46.6	340,134
SLD-Y	0.052	1.586	0.000	-4.2666	-0.0003	0.0	18
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.867	0.000	-	-	-	-
Elast-Y	-	3.867	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 3</b>							
SLU-X	0.079	2.598	0.000	-316.6325	-0.0498	13.7	100,256
SLU-Y	0.079	2.598	0.000	0.5402	0.0001	0.0	0
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.079	1.830	0.000	-316.6325	-0.0498	13.7	100,256
SLD-Y	0.079	1.830	0.000	0.5402	0.0001	0.0	0
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0



Spettro	Periodo	As.O	As.V	C.Part	C.Mod	P.M.M	M.Ec
	[s]	[m/s <sup>2</sup> ]	[m/s <sup>2</sup> ]			[%]	[N·s <sup>2</sup> /m]
Elast-X	-	4.469	0.000	-	-	-	-
Elast-Y	-	4.469	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 4</b>							
SLU-X	0.096	2.576	0.000	288.9347	0.0673	11.4	83,483
SLU-Y	0.096	2.576	0.000	0.6809	0.0002	0.0	0
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.096	1.985	0.000	288.9347	0.0673	11.4	83,483
SLD-Y	0.096	1.985	0.000	0.6809	0.0002	0.0	0
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	4.852	0.000	-	-	-	-
Elast-Y	-	4.852	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 5</b>							
SLU-X	0.040	2.648	0.000	-4.3837	-0.0002	0.0	19
SLU-Y	0.040	2.648	0.000	265.9115	0.0109	9.7	70,709
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.040	1.481	0.000	-4.3837	-0.0002	0.0	19
SLD-Y	0.040	1.481	0.000	265.9115	0.0109	9.7	70,709
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.605	0.000	-	-	-	-
Elast-Y	-	3.605	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 6</b>							
SLU-X	0.058	2.625	0.000	259.2357	0.0222	9.2	67,203
SLU-Y	0.058	2.625	0.000	3.6360	0.0003	0.0	13
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.058	1.643	0.000	259.2357	0.0222	9.2	67,203
SLD-Y	0.058	1.643	0.000	3.6360	0.0003	0.0	13
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	4.006	0.000	-	-	-	-
Elast-Y	-	4.006	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 7</b>							
SLU-X	0.024	2.669	0.000	22.3812	0.0003	0.1	501
SLU-Y	0.024	2.669	0.000	-153.2470	-0.0023	3.2	23,485
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.024	1.337	0.000	22.3812	0.0003	0.1	501
SLD-Y	0.024	1.337	0.000	-153.2470	-0.0023	3.2	23,485
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.249	0.000	-	-	-	-
Elast-Y	-	3.249	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 8</b>							
SLU-X	0.027	2.665	0.000	-10.1140	-0.0002	0.0	102
SLU-Y	0.027	2.665	0.000	-145.7956	-0.0027	2.9	21,256
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.027	1.360	0.000	-10.1140	-0.0002	0.0	102
SLD-Y	0.027	1.360	0.000	-145.7956	-0.0027	2.9	21,256
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.306	0.000	-	-	-	-
Elast-Y	-	3.306	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 9</b>							
SLU-X	0.049	2.637	0.000	-1.7286	-0.0001	0.0	3
SLU-Y	0.049	2.637	0.000	143.8192	0.0086	2.8	20,684
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.049	1.555	0.000	-1.7286	-0.0001	0.0	3
SLD-Y	0.049	1.555	0.000	143.8192	0.0086	2.8	20,684
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.790	0.000	-	-	-	-
Elast-Y	-	3.790	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 10</b>							
SLU-X	0.050	2.635	0.000	-136.1968	-0.0086	2.5	18,550
SLU-Y	0.050	2.635	0.000	1.6457	0.0001	0.0	3
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.050	1.568	0.000	-136.1968	-0.0086	2.5	18,550
SLD-Y	0.050	1.568	0.000	1.6457	0.0001	0.0	3
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.822	0.000	-	-	-	-
Elast-Y	-	3.822	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 11</b>							
SLU-X	0.029	2.663	0.000	-134.4132	-0.0029	2.5	18,067
SLU-Y	0.029	2.663	0.000	7.1482	0.0002	0.0	51
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.029	1.380	0.000	-134.4132	-0.0029	2.5	18,067
SLD-Y	0.029	1.380	0.000	7.1482	0.0002	0.0	51
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.355	0.000	-	-	-	-
Elast-Y	-	3.355	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-



Spettro	Periodo	As.O	As.V	C.Part	C.Mod	P.M.M	M.Ec
	[s]	[m/s <sup>2</sup> ]	[m/s <sup>2</sup> ]			[%]	[N·s <sup>2</sup> /m]
<b>Modo Vibrazione n. 12</b>							
SLU-X	0.026	2.667	0.000	130.2928	0.0022	2.3	16,976
SLU-Y	0.026	2.667	0.000	1.9535	0.0000	0.0	4
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.026	1.347	0.000	130.2928	0.0022	2.3	16,976
SLD-Y	0.026	1.347	0.000	1.9535	0.0000	0.0	4
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.275	0.000	-	-	-	-
Elast-Y	-	3.275	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 13</b>							
SLU-X	0.036	2.654	0.000	-17.3550	-0.0006	0.0	301
SLU-Y	0.036	2.654	0.000	127.4276	0.0041	2.2	16,238
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.036	1.437	0.000	-17.3550	-0.0006	0.0	301
SLD-Y	0.036	1.437	0.000	127.4276	0.0041	2.2	16,238
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.498	0.000	-	-	-	-
Elast-Y	-	3.498	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 14</b>							
SLU-X	0.035	2.655	0.000	-116.4614	-0.0036	1.9	13,563
SLU-Y	0.035	2.655	0.000	-7.4849	-0.0002	0.0	56
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.035	1.431	0.000	-116.4614	-0.0036	1.9	13,563
SLD-Y	0.035	1.431	0.000	-7.4849	-0.0002	0.0	56
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.482	0.000	-	-	-	-
Elast-Y	-	3.482	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 15</b>							
SLU-X	0.016	2.679	0.000	1.9402	0.0000	0.0	4
SLU-Y	0.016	2.679	0.000	115.9296	0.0008	1.8	13,440
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.016	1.263	0.000	1.9402	0.0000	0.0	4
SLD-Y	0.016	1.263	0.000	115.9296	0.0008	1.8	13,440
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.067	0.000	-	-	-	-
Elast-Y	-	3.067	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 16</b>							
SLU-X	0.024	2.669	0.000	-19.4016	-0.0003	0.1	376
SLU-Y	0.024	2.669	0.000	-115.4845	-0.0017	1.8	13,337
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.024	1.335	0.000	-19.4016	-0.0003	0.1	376
SLD-Y	0.024	1.335	0.000	-115.4845	-0.0017	1.8	13,337
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.245	0.000	-	-	-	-
Elast-Y	-	3.245	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 17</b>							
SLU-X	0.039	2.650	0.000	31.4169	0.0012	0.1	987
SLU-Y	0.039	2.650	0.000	108.4235	0.0041	1.6	11,756
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.039	1.466	0.000	31.4169	0.0012	0.1	987
SLD-Y	0.039	1.466	0.000	108.4235	0.0041	1.6	11,756
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.569	0.000	-	-	-	-
Elast-Y	-	3.569	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 18</b>							
SLU-X	0.020	2.674	0.000	-2.7122	0.0000	0.0	7
SLU-Y	0.020	2.674	0.000	102.9845	0.0011	1.5	10,606
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.020	1.297	0.000	-2.7122	0.0000	0.0	7
SLD-Y	0.020	1.297	0.000	102.9845	0.0011	1.5	10,606
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.151	0.000	-	-	-	-
Elast-Y	-	3.151	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 19</b>							
SLU-X	0.016	2.680	0.000	4.5402	0.0000	0.0	21
SLU-Y	0.016	2.680	0.000	-78.2243	-0.0005	0.8	6,119
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.016	1.256	0.000	4.5402	0.0000	0.0	21
SLD-Y	0.016	1.256	0.000	-78.2243	-0.0005	0.8	6,119
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.049	0.000	-	-	-	-
Elast-Y	-	3.049	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 20</b>							
SLU-X	0.015	2.681	0.000	1.8020	0.0000	0.0	3
SLU-Y	0.015	2.681	0.000	76.5886	0.0004	0.8	5,866



Spettro	Periodo	As.O	As.V	C.Part	C.Mod	P.M.M	M.Ec
	[s]	[m/s <sup>2</sup> ]	[m/s <sup>2</sup> ]			[%]	[N·s <sup>2</sup> /m]
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.015	1.252	0.000	1.8020	0.0000	0.0	3
SLD-Y	0.015	1.252	0.000	76.5886	0.0004	0.8	5,866
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.039	0.000	-	-	-	-
Elast-Y	-	3.039	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 21</b>							
SLU-X	0.016	2.680	0.000	7.9406	0.0001	0.0	63
SLU-Y	0.016	2.680	0.000	-69.4932	-0.0004	0.7	4,829
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.016	1.258	0.000	7.9406	0.0001	0.0	63
SLD-Y	0.016	1.258	0.000	-69.4932	-0.0004	0.7	4,829
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.055	0.000	-	-	-	-
Elast-Y	-	3.055	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 22</b>							
SLU-X	0.038	2.651	0.000	-28.0908	-0.0010	0.1	789
SLU-Y	0.038	2.651	0.000	67.4063	0.0025	0.6	4,544
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.038	1.459	0.000	-28.0908	-0.0010	0.1	789
SLD-Y	0.038	1.459	0.000	67.4063	0.0025	0.6	4,544
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.551	0.000	-	-	-	-
Elast-Y	-	3.551	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 23</b>							
SLU-X	0.028	2.664	0.000	12.0366	0.0002	0.0	145
SLU-Y	0.028	2.664	0.000	66.3760	0.0013	0.6	4,406
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.028	1.370	0.000	12.0366	0.0002	0.0	145
SLD-Y	0.028	1.370	0.000	66.3760	0.0013	0.6	4,406
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.331	0.000	-	-	-	-
Elast-Y	-	3.331	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 24</b>							
SLU-X	0.030	2.662	0.000	64.9967	0.0014	0.6	4,225
SLU-Y	0.030	2.662	0.000	2.2845	0.0001	0.0	5
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.030	1.383	0.000	64.9967	0.0014	0.6	4,225
SLD-Y	0.030	1.383	0.000	2.2845	0.0001	0.0	5
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.363	0.000	-	-	-	-
Elast-Y	-	3.363	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 25</b>							
SLU-X	0.021	2.673	0.000	62.2600	0.0007	0.5	3,876
SLU-Y	0.021	2.673	0.000	-7.0254	-0.0001	0.0	49
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.021	1.308	0.000	62.2600	0.0007	0.5	3,876
SLD-Y	0.021	1.308	0.000	-7.0254	-0.0001	0.0	49
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.178	0.000	-	-	-	-
Elast-Y	-	3.178	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 26</b>							
SLU-X	0.013	2.683	0.000	0.5298	0.0000	0.0	0
SLU-Y	0.013	2.683	0.000	55.2741	0.0002	0.4	3,055
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.013	1.234	0.000	0.5298	0.0000	0.0	0
SLD-Y	0.013	1.234	0.000	55.2741	0.0002	0.4	3,055
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	2.994	0.000	-	-	-	-
Elast-Y	-	2.994	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 27</b>							
SLU-X	0.020	2.675	0.000	0.6915	0.0000	0.0	0
SLU-Y	0.020	2.675	0.000	-55.1165	-0.0005	0.4	3,038
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.020	1.293	0.000	0.6915	0.0000	0.0	0
SLD-Y	0.020	1.293	0.000	-55.1165	-0.0005	0.4	3,038
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.140	0.000	-	-	-	-
Elast-Y	-	3.140	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 28</b>							
SLU-X	0.014	2.683	0.000	-0.5516	0.0000	0.0	0
SLU-Y	0.014	2.683	0.000	-54.6618	-0.0003	0.4	2,988
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.014	1.239	0.000	-0.5516	0.0000	0.0	0
SLD-Y	0.014	1.239	0.000	-54.6618	-0.0003	0.4	2,988



Spettro	Periodo	As.O	As.V	C.Part	C.Mod	P.M.M	M.Ec
	[s]	[m/s <sup>2</sup> ]	[m/s <sup>2</sup> ]			[%]	[N·s <sup>2</sup> /m]
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.006	0.000	-	-	-	-
Elast-Y	-	3.006	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 29</b>							
SLU-X	0.035	2.655	0.000	20.3275	0.0006	0.1	413
SLU-Y	0.035	2.655	0.000	50.0461	0.0016	0.3	2,505
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.035	1.433	0.000	20.3275	0.0006	0.1	413
SLD-Y	0.035	1.433	0.000	50.0461	0.0016	0.3	2,505
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.488	0.000	-	-	-	-
Elast-Y	-	3.488	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 30</b>							
SLU-X	0.043	2.645	0.000	49.7813	0.0023	0.3	2,478
SLU-Y	0.043	2.645	0.000	-20.6781	-0.0009	0.1	428
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.043	1.501	0.000	49.7813	0.0023	0.3	2,478
SLD-Y	0.043	1.501	0.000	-20.6781	-0.0009	0.1	428
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.654	0.000	-	-	-	-
Elast-Y	-	3.654	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 31</b>							
SLU-X	0.034	2.656	0.000	-48.9644	-0.0015	0.3	2,398
SLU-Y	0.034	2.656	0.000	5.7034	0.0002	0.0	33
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.034	1.425	0.000	-48.9644	-0.0015	0.3	2,398
SLD-Y	0.034	1.425	0.000	5.7034	0.0002	0.0	33
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.468	0.000	-	-	-	-
Elast-Y	-	3.468	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 32</b>							
SLU-X	0.018	2.677	0.000	-45.9863	-0.0004	0.3	2,115
SLU-Y	0.018	2.677	0.000	1.3454	0.0000	0.0	2
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.018	1.277	0.000	-45.9863	-0.0004	0.3	2,115
SLD-Y	0.018	1.277	0.000	1.3454	0.0000	0.0	2
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.101	0.000	-	-	-	-
Elast-Y	-	3.101	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 33</b>							
SLU-X	0.025	2.667	0.000	-45.0808	-0.0007	0.3	2,032
SLU-Y	0.025	2.667	0.000	-24.1797	-0.0004	0.1	585
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.025	1.346	0.000	-45.0808	-0.0007	0.3	2,032
SLD-Y	0.025	1.346	0.000	-24.1797	-0.0004	0.1	585
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.272	0.000	-	-	-	-
Elast-Y	-	3.272	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 34</b>							
SLU-X	0.045	2.642	0.000	27.5897	0.0014	0.1	761
SLU-Y	0.045	2.642	0.000	44.9205	0.0023	0.3	2,018
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.045	1.519	0.000	27.5897	0.0014	0.1	761
SLD-Y	0.045	1.519	0.000	44.9205	0.0023	0.3	2,018
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.701	0.000	-	-	-	-
Elast-Y	-	3.701	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 35</b>							
SLU-X	0.019	2.676	0.000	0.9048	0.0000	0.0	1
SLU-Y	0.019	2.676	0.000	42.6576	0.0004	0.2	1,820
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.019	1.283	0.000	0.9048	0.0000	0.0	1
SLD-Y	0.019	1.283	0.000	42.6576	0.0004	0.2	1,820
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.116	0.000	-	-	-	-
Elast-Y	-	3.116	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 36</b>							
SLU-X	0.015	2.681	0.000	-4.9532	0.0000	0.0	25
SLU-Y	0.015	2.681	0.000	42.1593	0.0002	0.2	1,777
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.015	1.251	0.000	-4.9532	0.0000	0.0	25
SLD-Y	0.015	1.251	0.000	42.1593	0.0002	0.2	1,777
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.037	0.000	-	-	-	-
Elast-Y	-	3.037	0.000	-	-	-	-



Spettro	Periodo	As.O	As.V	C.Part	C.Mod	P.M.M	M.Ec
	[s]	[m/s <sup>2</sup> ]	[m/s <sup>2</sup> ]			[%]	[N·s <sup>2</sup> /m]
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 37</b>							
SLU-X	0.017	2.678	0.000	-4.2990	0.0000	0.0	18
SLU-Y	0.017	2.678	0.000	-35.2566	-0.0003	0.2	1,243
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.017	1.272	0.000	-4.2990	0.0000	0.0	18
SLD-Y	0.017	1.272	0.000	-35.2566	-0.0003	0.2	1,243
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.087	0.000	-	-	-	-
Elast-Y	-	3.087	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 38</b>							
SLU-X	0.015	2.682	0.000	-34.0157	-0.0002	0.2	1,157
SLU-Y	0.015	2.682	0.000	3.6469	0.0000	0.0	13
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.015	1.247	0.000	-34.0157	-0.0002	0.2	1,157
SLD-Y	0.015	1.247	0.000	3.6469	0.0000	0.0	13
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.027	0.000	-	-	-	-
Elast-Y	-	3.027	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 39</b>							
SLU-X	0.017	2.679	0.000	-33.9127	-0.0002	0.2	1,150
SLU-Y	0.017	2.679	0.000	3.2032	0.0000	0.0	10
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.017	1.266	0.000	-33.9127	-0.0002	0.2	1,150
SLD-Y	0.017	1.266	0.000	3.2032	0.0000	0.0	10
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.073	0.000	-	-	-	-
Elast-Y	-	3.073	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 40</b>							
SLU-X	0.015	2.681	0.000	25.9537	0.0001	0.1	674
SLU-Y	0.015	2.681	0.000	-33.0976	-0.0002	0.1	1,095
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.015	1.248	0.000	25.9537	0.0001	0.1	674
SLD-Y	0.015	1.248	0.000	-33.0976	-0.0002	0.1	1,095
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.030	0.000	-	-	-	-
Elast-Y	-	3.030	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 41</b>							
SLU-X	0.015	2.681	0.000	-5.4900	0.0000	0.0	30
SLU-Y	0.015	2.681	0.000	-32.3472	-0.0002	0.1	1,046
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.015	1.251	0.000	-5.4900	0.0000	0.0	30
SLD-Y	0.015	1.251	0.000	-32.3472	-0.0002	0.1	1,046
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.036	0.000	-	-	-	-
Elast-Y	-	3.036	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 42</b>							
SLU-X	0.042	2.646	0.000	31.1857	0.0014	0.1	973
SLU-Y	0.042	2.646	0.000	-26.4258	-0.0012	0.1	698
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.042	1.492	0.000	31.1857	0.0014	0.1	973
SLD-Y	0.042	1.492	0.000	-26.4258	-0.0012	0.1	698
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.634	0.000	-	-	-	-
Elast-Y	-	3.634	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 43</b>							
SLU-X	0.014	2.682	0.000	31.0351	0.0002	0.1	963
SLU-Y	0.014	2.682	0.000	4.4364	0.0000	0.0	20
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.014	1.245	0.000	31.0351	0.0002	0.1	963
SLD-Y	0.014	1.245	0.000	4.4364	0.0000	0.0	20
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.022	0.000	-	-	-	-
Elast-Y	-	3.022	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 44</b>							
SLU-X	0.014	2.682	0.000	-1.3150	0.0000	0.0	2
SLU-Y	0.014	2.682	0.000	-30.7882	-0.0002	0.1	948
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.014	1.244	0.000	-1.3150	0.0000	0.0	2
SLD-Y	0.014	1.244	0.000	-30.7882	-0.0002	0.1	948
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.020	0.000	-	-	-	-
Elast-Y	-	3.020	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-
<b>Modo Vibrazione n. 45</b>							
SLU-X	0.014	2.683	0.000	5.8114	0.0000	0.0	34



Spettro	Periodo	As.O	As.V	C.Part	C.Mod	P.M.M	M.Ec
	[s]	[m/s <sup>2</sup> ]	[m/s <sup>2</sup> ]			[%]	[N·s <sup>2</sup> /m]
SLU-Y	0.014	2.683	0.000	-30.3973	-0.0001	0.1	924
SLU-Z	0.000	0.000	1.133	0.0000	0.0000	0.0	0
SLD-X	0.014	1.238	0.000	5.8114	0.0000	0.0	34
SLD-Y	0.014	1.238	0.000	-30.3973	-0.0001	0.1	924
SLD-Z	0.000	0.000	0.276	0.0000	0.0000	0.0	0
Elast-X	-	3.005	0.000	-	-	-	-
Elast-Y	-	3.005	0.000	-	-	-	-
Elast-Z	-	0.000	1.133	-	-	-	-

## LEGENDA Modi di vibrazione

<b>Spettro</b>	Spettro di risposta considerato.
<b>Periodo</b>	Periodo del Modo di vibrazione.
<b>As.O</b>	Valore dell'Accelerazione Spettrale Orizzontale, riferita al corrispondente periodo.
<b>As.V</b>	Valore dell'Accelerazione Spettrale Verticale, riferita al corrispondente periodo.
<b>C.Part</b>	Coefficiente di partecipazione del Modo di Vibrazione.
<b>C.Mod</b>	Coefficiente modale del modo di vibrazione.
<b>P.M.M</b>	Percentuale di mobilitazione delle masse nel modo di vibrazione.
<b>M.Ec</b>	Massa Eccitata nel modo di vibrazione.
<b>SLU-X</b>	Spettro di progetto allo S.L. Ultimo per sisma in direzione X.
<b>SLU-Y</b>	Spettro di progetto allo S.L. Ultimo per sisma in direzione Y.
<b>SLU-Z</b>	Spettro di progetto allo S.L. Ultimo per sisma in direzione Z.
<b>SLD-X</b>	Spettro di progetto allo S.L. di Danno per sisma in direzione X.
<b>SLD-Y</b>	Spettro di progetto allo S.L. di Danno per sisma in direzione Y.
<b>SLD-Z</b>	Spettro di progetto allo S.L. di Danno per sisma in direzione Z.
<b>Elast-X</b>	Spettro Elastico per sisma in direzione X.
<b>Elast-Y</b>	Spettro Elastico per sisma in direzione Y.
<b>Elast-Z</b>	Spettro Elastico per sisma in direzione Z.

## PLATEE

						Platee
Livello	N	Spessore	Superficie	Materiale	Terreno	Calc. Fond.
		[m]	[m <sup>2</sup> ]			
Piano Fondo Vasca	1	0.50	85.10	003	T001	SI
<b>SHELL</b>	[01176-01175-01180]	[01015-01245-01016]	[00254-00777-00253]	[01148-01142-01147]	[00254-00778-00777]	
	[00079-00994-00078]	[00254-00255-00778]	[00079-00993-00994]	[00242-00766-00765]	[00079-00080-00992]	
	[00242-00243-00766]	[00079-00992-00993]	[00252-00775-00251]	[00075-00076-00997]	[00252-00776-00775]	
	[00075-00997-00998]	[00242-00765-00241]	[00078-00994-00995]	[00253-00777-00776]	[01202-01201-01207]	
	[00255-00779-00778]	[01152-01146-00085]	[00258-00259-00783]	[00093-00183-00976]	[00258-00783-00782]	
	[01019-00065-00182]	[00241-00764-00240]	[01131-00089-00088]	[00241-00765-00764]	[01184-00079-00078]	
	[00256-00781-00780]	[01019-00182-00136]	[00252-00253-00776]	[00092-00976-00977]	[00256-00780-00779]	
	[00244-00767-00243]	[00244-00768-00767]	[00247-00248-00771]	[00245-00769-00768]	[00768-00769-01226]	
	[00244-00245-00768]	[01227-01221-00069]	[00771-00772-01215]	[00248-00772-00771]	[00251-00775-00774]	
	[00083-00987-00988]	[00247-00771-00770]	[00246-00770-00769]	[00246-00769-00245]	[01152-00084-01157]	
	[00250-00774-00773]	[00250-00773-00249]	[00255-00256-00779]	[01028-00093-01114]	[00246-00247-00770]	
	[00270-00795-00794]	[00268-00793-00792]	[00080-00081-00991]	[00266-00791-00790]	[00081-00990-00991]	
	[00266-00267-00791]	[00080-00991-00992]	[00266-00790-00265]	[00232-01017-00231]	[00267-00792-00791]	
	[00082-00989-00990]	[00083-00989-00082]	[00791-00792-01140]	[00282-00133-01028]	[01125-00979-00090]	
	[00092-00977-00978]	[01243-00066-01009]	[00092-00978-00091]	[00090-00979-00980]	[01019-01243-00065]	
	[00083-00988-00989]	[00087-00983-00984]	[00084-00986-00987]	[00086-00984-00985]	[00086-00087-00984]	
	[00257-00258-00782]	[01125-00091-00979]	[01114-00093-00976]	[00087-00982-00983]	[00085-00986-00084]	
	[00085-00985-00986]	[00088-00089-00981]	[00088-00981-00982]	[00088-00982-00087]	[00089-00980-00981]	
	[00066-00067-01008]	[00066-01008-01009]	[00091-00978-00979]	[01184-00077-01189]	[01114-00976-00092]	
	[00067-01007-01008]	[00090-00980-00089]	[00076-00996-00997]	[01243-01009-00065]	[00078-00995-00077]	
	[00273-00134-00138]	[01232-01007-00067]	[00077-00995-00996]	[00069-01005-01006]	[00281-00282-01027]	
	[01027-00282-01028]	[00074-00999-01000]	[00068-00069-01006]	[00071-00072-01002]	[00071-01002-01003]	
	[01152-00085-00084]	[00068-01006-01007]	[00065-01009-01010]	[00070-00071-01003]	[00072-00073-01001]	
	[01232-00068-01007]	[00273-00138-00797]	[00073-01000-01001]	[00073-00074-01000]	[00072-01001-01002]	
	[00070-01003-01004]	[01221-00070-01004]	[01221-01004-01005]	[00234-01015-00233]	[01200-00075-00998]	
	[01200-00999-00074]	[00065-01010-00182]	[00135-00139-00238]	[01200-00998-00999]	[01206-01200-00074]	
	[01120-00091-01125]	[01159-01158-01164]	[01120-00092-00091]	[01227-00068-01232]	[01184-00078-00077]	
	[01206-00074-00073]	[01189-00996-00076]	[01189-00077-00996]	[01146-00985-00085]	[01146-00086-00985]	
	[01221-01005-00069]	[01206-00073-00072]	[01227-00069-00068]	[01014-01015-00234]	[01120-01114-00092]	
	[01168-00990-00081]	[01168-00082-00990]	[01202-01196-01201]	[00275-00276-01021]	[01157-00084-00987]	
	[01157-00987-00083]	[01015-01016-00233]	[00230-01019-00136]	[01016-01017-00232]	[01028-00133-00183]	
	[01028-00183-00093]	[01238-01232-00067]	[01132-01131-01136]	[01238-00067-00066]	[01141-00088-00087]	
	[01141-00086-01146]	[01195-00075-01200]	[01165-01164-01170]	[01201-01200-01206]	[01195-01189-00076]	
	[01195-00076-00075]	[01163-01157-00083]	[01163-00083-00082]	[01216-00072-00071]	[01244-01243-01018]	
	[01201-01195-01200]	[01018-01243-01019]	[01131-00090-00089]	[01131-01125-00090]	[01141-00087-00086]	
	[01238-00066-01243]	[01174-00080-00079]	[01174-01168-00081]	[00239-00763-00139]	[01163-00082-01168]	
	[01216-00071-00070]	[01216-00070-01221]	[00279-00280-01025]	[01211-00072-01216]	[01174-00081-00080]	
	[01018-01019-00230]	[00231-01018-00230]	[00280-00281-01026]	[01027-01028-01114]	[00239-00139-00135]	
	[01222-01221-01227]	[01222-01216-01221]	[01179-01174-00079]	[01211-01206-00072]	[01244-01238-01243]	
	[01169-01168-01174]	[01169-01163-01168]	[01158-01152-01157]	[01158-01157-01163]	[01233-01232-01238]	
	[01233-01227-01232]	[01126-01120-01125]	[01126-01125-01131]	[00272-00797-00796]	[01190-01184-01189]	
	[01207-01201-01206]	[01185-01179-01184]	[01185-01189-01195]	[01115-01114-01120]	[01115-01027-01114]	
	[01017-01244-01018]	[01179-00079-01184]	[01132-01126-01131]	[01147-01146-01152]	[01147-01141-01146]	
	[01136-01131-00088]	[01136-00088-01141]	[01023-00278-01024]	[01121-01115-01120]	[01017-01018-00231]	
	[01026-00281-01027]	[01026-01027-01115]	[00796-00797-01119]	[01121-01120-01126]	[01185-01184-01190]	
	[01207-01206-01211]	[01153-01147-01152]	[01153-01152-01158]	[01116-01115-01121]	[01142-01136-01141]	
	[00268-00792-00267]	[01228-01227-01233]	[01239-01238-01244]	[01175-01174-01179]	[01239-01233-01238]	



							Platee
Livello	N	Spessore	Superficie	Materiale	Terreno	Calc. Fond.	
		[m]	[m²]				
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	[01261-01260-01268]	[01261-01253-01260]	[00299-00885-00886]	[01307-01306-01314]	[01344-01336-01343]	
	[01314-01313-01321]	[01389-01388-01396]	[01389-01381-01388]	[01277-01269-01276]	[01329-01321-01328]	
	[01329-01328-01336]	[01254-01253-01261]	[01254-00840-01253]	[01299-01298-01306]	[01299-01291-01298]	
	[01427-01426-01434]	[01419-01418-01426]	[01419-01411-01418]	[01307-01299-01306]	[00333-00334-00841]	
	[01427-01419-01426]	[00299-00886-00298]	[01277-01276-01284]	[01284-01276-01283]	[01284-01283-01291]	
	[01420-01412-01419]	[00852-00851-00291]	[01382-01374-01381]	[01269-01268-01276]	[01269-01261-01268]	
	[01374-01373-01381]	[01374-01366-01373]	[01262-01261-01269]	[00887-01428-00888]	[00852-01434-00851]	
	[01397-01389-01396]	[01382-01381-01389]	[00292-00852-00291]	[00298-00887-00297]	[00884-01413-00885]	
	[01352-01351-01359]	[01352-01344-01351]	[01300-01292-01299]	[01255-00841-01254]	[01337-01329-01336]	
	[01337-01336-01344]	[01412-01411-01419]	[01412-01404-01411]	[01262-01254-01261]	[00854-01435-00853]	



						Platee
Livello	N	Spessore	Superficie	Materiale	Terreno	Calc. Fond.
		[m]	[m <sup>2</sup> ]			
[00887-00886-01421]		[01322-01314-01321]	[01322-01321-01329]	[01270-01262-01269]	[01292-01291-01299]	
[01292-01284-01291]		[01405-01397-01404]	[00298-00886-00887]	[01367-01359-01366]	[01367-01366-01374]	
[00331-00332-00843]		[01436-01435-00854]	[01285-01284-01292]	[00889-00888-01436]	[01397-01396-01404]	
[01436-01428-01435]		[01405-01404-01412]	[00853-01435-00852]	[00296-00888-00889]	[01420-01419-01427]	
[01360-01352-01359]		[01360-01359-01367]	[01285-01277-01284]	[01308-01307-01315]	[01270-01269-01277]	
[00853-00852-00292]		[01390-01389-01397]	[01390-01382-01389]	[01330-01329-01337]	[01330-01322-01329]	
[01375-01367-01374]		[01435-01434-00852]	[01435-01427-01434]	[00876-01368-00877]	[01315-01307-01314]	
[01375-01374-01382]		[00295-00889-00049]	[01315-01314-01322]	[01428-01420-01427]	[01428-01427-01435]	
[01345-01344-01352]		[01345-01337-01344]	[01421-01413-01420]	[00856-01263-00857]	[00842-00841-01255]	
[00842-00333-00841]		[00870-01338-00871]	[00050-00331-00843]	[00323-00862-00322]	[01323-01315-01322]	
[01338-01330-01337]		[01338-01337-01345]	[01308-01300-01307]	[01368-01360-01367]	[01368-01367-01375]	
[00857-01263-01271]		[01263-01262-01270]	[01293-01285-01292]	[01293-01292-01300]	[01278-01270-01277]	
[01278-01277-01285]		[00878-01383-00879]	[01263-01255-01262]	[00889-01436-00049]	[01256-00843-01255]	
[01398-01397-01405]		[01398-01390-01397]	[01323-01322-01330]	[01413-01405-01412]	[01413-01412-01420]	
[00867-01323-00868]		[00326-00859-00325]	[01383-01375-01382]	[01383-01382-01390]	[01353-01352-01360]	
[01353-01345-01352]		[00856-01256-01263]	[00861-01293-00862]	[00303-00882-00302]	[00843-00842-01255]	
[00843-00332-00842]		[01361-01353-01360]	[01256-01255-01263]	[01316-01315-01323]	[01361-01360-01368]	
[01301-01293-01300]		[01301-01300-01308]	[00873-01353-00874]	[00881-01398-00882]	[01286-01285-01293]	
[01286-01278-01285]		[00864-01308-00865]	[01271-01270-01278]	[01271-01263-01270]	[00878-01376-01383]	
[01376-01375-01383]		[01376-01368-01375]	[01391-01390-01398]	[01391-01383-01390]	[01316-01308-01315]	
[00858-01271-00859]		[01331-01330-01338]	[01331-01323-01330]	[00870-01331-01338]	[01346-01338-01345]	
[01346-01345-01353]		[01406-01398-01405]	[01406-01405-01413]	[00049-01436-00854]	[01421-01420-01428]	
[00859-01278-00860]		[00049-00854-00294]	[00859-01271-01278]	[00050-01256-00855]	[00860-01278-01286]	
[00888-01428-01436]		[00887-01421-01428]	[00050-00843-01256]	[00317-00867-00868]	[00885-01421-00886]	
[00885-01413-01421]		[00131-00049-00294]	[00884-01406-01413]	[00295-00049-00131]	[00296-00889-00295]	
[00883-01398-01406]		[00297-00888-00296]	[00882-01398-00883]	[00881-01391-01398]	[00297-00887-00888]	
[00861-01286-01293]		[00880-01383-01391]	[00316-00869-00315]	[00879-01383-00880]	[00300-00885-00299]	
[00862-01293-00863]		[00306-00879-00305]	[00877-01368-01376]	[00876-01361-01368]	[00863-01293-01301]	
[00875-01361-00876]		[00304-00881-00303]	[00309-00876-00308]	[00874-01353-01361]	[00873-01346-01353]	
[00305-00880-00304]		[00311-00874-00310]	[00315-00870-00314]	[00871-01338-01346]	[00320-00865-00319]	
[00308-00877-00307]		[00309-00875-00876]	[00314-00871-00313]	[00868-01331-00869]	[00868-01323-01331]	
[00864-01301-01308]		[00867-01316-01323]	[00317-00868-00316]	[00873-00872-01346]	[00866-01308-01316]	
[00865-01308-00866]						

## LEGENDA Platee

<b>Livello</b>	Identificativo del livello, nella relativa tabella.
<b>N</b>	Numero identificativo della platea.
<b>Materiale</b>	Identificativo del tipo di materiale, nella relativa tabella.
<b>Terreno</b>	Identificativo del terreno di sottofondo, nella relativa tabella.
<b>Shell</b>	Ciascuna platea è stata suddivisa in shell di forma triangolare o rettangolare, individuate mediante i relativi vertici.
<b>Calc. Fond.</b>	Indica se l'elemento strutturale è incluso nel calcolo della "struttura di fondazione" secondo quanto previsto nel § 7.2.5 del DM. 14/01/2008 ("elementi progettati per rimanere in campo elastico"). [Si]=elemento progettato in accordo alle prescrizioni del § 7.2.5; [No]=elemento non progettato secondo le prescrizioni del § 7.2.5.

## PALI

										Pali
Palo	Nodo	Diametro	Sezione	Lunghezza	Materiale	Tipologia	Tecnologia	Coeff. Attrito	Coeff. Coesione	Num. Ind. Str.
		[cm]		[m]						
PALO92	00106	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO65	00115	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO34	00124	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO89	00107	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO62	00116	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO31	00125	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO20	00054	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO86	00108	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO55	00117	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO28	00126	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO83	00109	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO52	00118	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO25	00127	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO80	00110	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO49	00119	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO23	00128	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO104	00051	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO77	00111	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO46	00120	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO101	00103	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO74	00112	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO43	00121	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO98	00104	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO71	00113	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO40	00122	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO96	00105	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO69	00114	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO38	00123	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO107	00051	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO108	00102	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO109	00101	40	8	18	001	Trivellato	in opera	0.80	0.30	3



										Pali
Palo	Nodo	Diametro	Sezione	Lunghezza	Materiale	Tipologia	Tecnologia	Coeff. Attrito	Coeff. Coesione	Num. Ind. Str.
		[cm]		[m]						
PALO110	00100	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO111	00099	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO112	00098	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO113	00097	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO114	00096	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO115	00095	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO116	00094	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO117	00052	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO118	00005	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO119	00006	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO120	00007	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO121	00008	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO122	00009	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO123	00010	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO124	00011	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO125	00053	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO106	00053	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO103	00012	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO100	00013	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO97	00014	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO95	00015	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO91	00016	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO88	00017	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO85	00018	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO82	00019	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO79	00020	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO76	00021	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO73	00022	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO70	00023	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO68	00024	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO64	00025	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO61	00026	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO59	00027	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO58	00028	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO54	00029	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO51	00030	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO48	00031	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO45	00032	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO42	00033	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO39	00034	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO37	00035	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO33	00036	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO30	00037	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO27	00038	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO24	00039	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO22	00055	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO2	00064	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO1	00054	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO3	00063	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO4	00062	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO5	00061	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO6	00060	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO7	00059	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO8	00058	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO9	00057	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO10	00056	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO11	00137	40	8	18	001	Trivellato	in opera	0.80	0.30	3
PALO12	00040	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO13	00041	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO14	00042	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO15	00043	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO16	00044	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO17	00045	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO18	00046	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO19	00055	40	8	12	001	Trivellato	in opera	0.80	0.30	3
PALO105	00093	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO102	00092	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO99	00091	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO94	00090	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO93	00089	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO90	00088	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO87	00087	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO84	00086	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO81	00085	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO78	00084	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO75	00083	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO72	00082	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO67	00081	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO66	00080	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO63	00079	40	8	14	001	Trivellato	in opera	0.80	0.30	3



										Pali
Palo	Nodo	Diametro	Sezione	Lunghezza	Materiale	Tipologia	Tecnologia	Coeff. Attrito	Coeff. Coesione	Num. Ind. Str.
		[cm]		[m]						
PALO60	00078	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO57	00077	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO56	00076	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO53	00075	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO50	00074	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO47	00073	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO44	00072	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO41	00071	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO36	00070	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO35	00069	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO32	00068	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO29	00067	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO26	00066	40	8	14	001	Trivellato	in opera	0.80	0.30	3
PALO21	00065	40	8	14	001	Trivellato	in opera	0.80	0.30	3

## LEGENDA Pali

<b>Palo</b>	Numero identificativo del palo.
<b>Nodo</b>	Numero identificativo del nodo posto in testa al palo.
<b>Diametro</b>	Diametro del palo.
<b>Sezione</b>	Sezione del palo.
<b>Lunghezza</b>	Lunghezza del palo.
<b>Materiale</b>	Identificativo del materiale nella relativa tabella.
<b>Tipologia</b>	Tipologia di palo (Trivellato, Battuto).
<b>Tecnologia</b>	Tecnologia adottata (in opera, Prefabbricato).
<b>Coeff. Attrito</b>	Coefficiente di attrito terreno/palo.
<b>Coeff. Coesione</b>	Coefficiente di riduzione legato alla coesione.
<b>Num. Ind. Str.</b>	Numero di indagini stratigrafiche significative.

## CARICHI SULLE SOLETTE

									Carichi sulle solette
T.Carico	Shell	Carico	CC	SR	φ	Qx	Qy	Qz	
						[N/m²]	[N/m²]	[N/m²]	
<b>Piano Terra</b>		<b>Soletta P1-P2-P5-P4</b>			<b>Peso proprio</b>		<b>-5,000</b>		
S	-	CR001	002	G	-	0	0	-2,360	
S	-	CR002	003	G	-	0	0	-5,000	
S	-	CR003	004	G	-	0	0	-600	
<b>Piano Terra</b>		<b>Soletta P2-P3-P6-P5</b>			<b>Peso proprio</b>		<b>-5,000</b>		
S	-	CR001	002	G	-	0	0	-2,360	
S	-	CR002	003	G	-	0	0	-5,000	
S	-	CR003	004	G	-	0	0	-600	

## LEGENDA Carichi sulle solette

<b>T.Carico</b>	Descrizione del tipo di carico.
<b>Carico</b>	Descrizione del carico: CR001= SOLETTA: Soletta copertura (sovraccarico permanente) CR002= SOLETTA: Soletta copertura (sovraccarico accidentale) CR003= SOLETTA: Soletta copertura (carico neve)
<b>CC</b>	Identificativo della condizione di carico nella relativa tabella.
<b>SR</b>	Identificativo del sistema di riferimento considerato: [G] = Sistema di riferimento Globale X, Y, Z - [L] = Sistema di riferimento Locale 1, 2, 3.
<b>φ</b>	Nel caso di effettuazione dei calcoli secondo l'Ordinanza 3274/03 e s.m.i., è il valore del coefficiente di riduzione delle masse sismiche.
<b>Qx, Qy, Qz</b>	Valore della forza distribuita superficiale uniforme riferita agli assi del sistema di riferimento indicato nella colonna "SR".
<b>ΔT</b>	Gradiente di temperatura fra le facce dell'elemento shell.

## EDIFICIO - VERIFICHE DI RIPARTIZIONE DELLE FORZE SISMICHE

Edificio - Verifiche di ripartizione delle forze sismiche													
Tg <sub>tot</sub> X	Tg <sub>tot</sub> Y	Tg <sub>pil</sub> X	Tg <sub>pil</sub> Y	% <sub>pil</sub> X	% <sub>pil</sub> Y	Tg <sub>setti</sub> X	Tg <sub>setti</sub> Y	% <sub>setti</sub> X	% <sub>setti</sub> Y	Tg <sub>altro</sub> X	Tg <sub>altro</sub> Y	% <sub>altro</sub> X	% <sub>altro</sub> Y
[N]	[N]	[N]	[N]			[N]	[N]			[N]	[N]		
441,458	945,672	0	0	0.0	0.0	0	0	0.0	0.0	441,458	945,672	100.0	100.0

## LEGENDA Edificio - Verifiche di ripartizione delle forze sismiche

<b>Tg<sub>tot</sub></b>	Taglio totale alla quota Zero Sismico (nella direzione X o Y) [N]
<b>Tg<sub>pil</sub></b>	Taglio totale alla quota Zero Sismico assorbito dai pilastri (nella direzione X o Y) [N]
<b>%<sub>pil</sub></b>	Percentuale del Taglio totale alla quota Zero Sismico assorbito dai pilastri (nella direzione X o Y)
<b>Tg<sub>setti</sub></b>	Taglio totale alla quota Zero Sismico assorbito dai setti [N]
<b>%<sub>setti</sub></b>	Percentuale del Taglio totale alla quota Zero Sismico assorbito dai setti (nella direzione X o Y)
<b>Tg<sub>altro</sub></b>	Taglio totale alla quota Zero Sismico NON assorbito dai pilastri e dai setti (nella direzione X o Y)[N]
<b>%<sub>altro</sub></b>	Percentuale del Taglio totale alla quota Zero Sismico NON assorbito dai pilastri e dai setti (nella direzione X o Y)

## Pareti - VERIFICHE PRESSOFLESSIONE RETTA ALLO STATO LIMITE ULTIMO (Elevazione)

Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
Piano Terra			PareteP1-P2-P3									Parete P1-P2				
P	A	00047	101,518	18,915	0.13407	6.63	00048	-86,179	35,366	0.13407	4.23	00054	435,339	15,069	0.13407	5.44
P	P		107,945	5,784	0.13407	21.55		22,438	494	0.13407	NS		-	816	0.13407	NS
S	A		-	62,240	0.13407	2.62		-	138,145	0.13407	1.14		236,492			
			191.010					142.791					-25,653	14,355	0.13407	9.66



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	P		0	0	0.13407	-		4,444	3,490	0.13407	39.56		90,795	1,782	0.13407	69.36
P	A	00056	129,417	23,176	0.13407	5.26	00057	80,151	15,818	0.13407	8.11	00058	5,546	28,560	0.13407	4.83
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A	00059	-44,653	4,396	0.13407	32.85	00060	-61,048	5,535	0.13407	26.47	00061	-72,914	5,212	0.13407	28.41
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	00059	6,580	35,215	0.13407	3.91	00060	9,774	32,263	0.13407	4.26	00061	52,352	27,737	0.13407	4.75
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A	00062	-	8,332	0.13407	18.36	00063	-	8,679	0.13407	18.08	00064	-	10,984	0.13407	14.25
	P		111,213	0	0.13407	-		141,778	0	0.13407	-		138,586	0	0.13407	-
P	A	00062	62,817	15,399	0.13407	8.48	00063	17,859	11,097	0.13407	12.29	00064	-13,270	9,080	0.13407	15.46
	P		0	0	0.13407	-		78,832	4,996	0.13407	25.71		38,580	7,923	0.13407	16.87
S	A	00137	-56,440	5,508	0.13407	26.49	00379	-13,258	1,944	0.13407	72.20	00517	50,024	1,493	0.13407	88.53
	P		0	0	0.13407	-		0	0	0.13407	-		-	1,551	0.13407	98.36
			107,983													
P	A	00137	132,590	36,655	0.13407	3.31	00379	132,065	29,142	0.13407	4.17	00517	3,151	1,499	0.13407	92.22
	P		10,364	2,673	0.13407	51.37		0	0	0.13407	-		118,955	2,240	0.13407	55.01
S	A	00518	-46,028	16,353	0.13407	8.84	00519	-21,925	4,602	0.13407	30.74	00520	-25,264	1,325	0.13407	NS
	P		2,162	9,991	0.13407	13.85		24,285	239	0.13407	NS		-14,194	10,045	0.13407	13.98
P	A	00518	5,443	3,206	0.13407	43.03	00519	-1,185	3,778	0.13407	36.74	00520	11,549	6,720	0.13407	20.41
	P		76,966	1,417	0.13407	90.81		49,304	952	0.13407	NS		51,580	1,703	0.13407	77.49
S	A	00521	-36,281	6,107	0.13407	23.47	00522	-46,365	17,282	0.13407	8.37	00523	-51,993	22,941	0.13407	6.34
	P		-19,468	8,119	0.13407	17.39		-10,924	7,113	0.13407	19.69		3,690	5,561	0.13407	24.85
P	A	00521	3,906	8,372	0.13407	16.50	00522	-19,969	8,186	0.13407	17.25	00523	-98	12,515	0.13407	11.08
	P		37,038	533	0.13407	NS		31,419	1,011	0.13407	NS		39,845	287	0.13407	NS
S	A	00524	-81,804	33,130	0.13407	4.50	00541	-96,222	45,545	0.13407	3.32	00542	-	47,070	0.13407	3.28
	P		-11,794	3,896	0.13407	35.98		8,691	3,813	0.13407	36.07		121,172	2,604	0.13407	52.34
P	A	00524	21,035	11,748	0.13407	11.57	00541	427,354	818	0.13407	NS	00542	42,603	4,374	0.13407	30.44
	P		0	0	0.13407	-		45,775	6,649	0.13407	19.96		184,465	1,081	0.13407	NS
S	A	00543	-	57,791	0.13407	2.67	00544	-	4,673	0.13407	32.70	00545	-31,055	17,155	0.13407	8.32
	P		123,090	958	0.13407	NS		109,847	4,584	0.13407	26.30		45,783	7,432	0.13407	17.86
P	A	00543	84,088	5,777	0.13407	22.86	00544	139,268	13,706	0.13407	9.77	00545	-8,458	15,199	0.13407	9.19
	P		50,625	1,621	0.13407	72.17		36,083	1,895	0.13407	65.84		75,518	1,317	0.13407	97.85
S	A	00546	-36,484	33,750	0.13407	4.25	00547	-33,558	49,223	0.13407	2.90	00548	-73,273	70,170	0.13407	2.11
	P		28,034	8,285	0.13407	16.30		4,734	7,144	0.13407	19.32		14,853	5,756	0.13407	23.75
P	A	00546	-38,186	18,244	0.13407	7.87	00547	-21,341	26,076	0.13407	5.42	00548	-82,080	24,515	0.13407	6.09
	P		72,496	1,206	0.13407	NS		38,326	974	0.13407	NS		29,835	1,058	0.13407	NS
S	A	00587	-81,835	93,082	0.13407	1.60	00588	-96,854	103,649	0.13407	1.46	00589	-	123,116	0.13407	1.26
	P		9,185	5,545	0.13407	24.79		6,967	4,252	0.13407	32.39		124,345	4,194	0.13407	32.94
P	A	00587	53,014	5,742	0.13407	22.95	00588	0	0	0.13407	-	00589	0	0	0.13407	-
	P		0	0	0.13407	-		8,393	892	0.13407	NS		29,397	10,397	0.13407	12.97
S	A	00590	-	22,943	0.13407	6.68	00591	0	0	0.13407	-	00592	55,992	101	0.13407	NS
	P		113,723	367	0.13407	NS		-85,025	2,728	0.13407	54.84		-94,384	23,907	0.13407	6.31
P	A	00590	0	0	0.13407	-	00591	0	0	0.13407	-	00592	0	0	0.13407	-
	P		22,748	15,079	0.13407	9.00		19,483	15,740	0.13407	8.65		15,537	15,920	0.13407	8.58
S	A	00593	48,100	380	0.13407	NS	00594	38,231	571	0.13407	NS	00595	33,621	572	0.13407	NS
	P		-92,700	37,736	0.13407	3.99		-99,132	42,253	0.13407	3.58		-	40,558	0.13407	3.74
			102,224													
P	A	00593	0	0	0.13407	-	00594	0	0	0.13407	-	00595	0	0	0.13407	-
	P		5,591	11,123	0.13407	12.40		-977	9,090	0.13407	15.27		13,700	819	0.13407	NS
S	A	00596	29,511	224	0.13407	NS	00597	0	0	0.13407	-	01043	-	4,933	0.13407	31.46
	P		-	32,686	0.13407	4.68		-	20,749	0.13407	7.42		128,633	934	0.13407	NS
			110,017													
P	A	00596	-32,609	13,606	0.13407	10.50	00597	-48,946	17,741	0.13407	8.17	01043	33,515	29,100	0.13407	4.62
	P		17,845	848	0.13407	NS		19,477	589	0.13407	NS		0	0	0.13407	-
S	A	01044	-	40,228	0.13407	3.88	01047	-	79,389	0.13407	1.97	01048	-68,695	8,698	0.13407	16.96
	P		135,727	1,813	0.13407	75.43		139,215	2,707	0.13407	50.99		0	0	0.13407	-
P	A	01044	14,650	0	0.13407	-	01047	4,662	0	0.13407	-	01048	0	0	0.13407	-
	P		63,352	21,134	0.13407	6.17		1,310	31,942	0.13407	4.34		17,098	33,628	0.13407	4.06
S	A	01051	0	0	0.13407	-	01052	0	0	0.13407	-	01055	0	0	0.13407	-
	P		-	9,455	0.13407	16.06		-87,839	6,272	0.13407	23.91		-	9,607	0.13407	15.82
P	A	01051	102,426	0	0.13407	-	01052	-	0	0.13407	-	01055	103,446	0	0.13407	-
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A	01056	91,135	11,885	0.13407	10.67	02426	-7,837	14,133	0.13407	9.88	02427	78,871	19,405	0.13407	6.62
	P		0	0	0.13407	-		66,776	8,846	0.13407	14.70		0	0	0.13407	-
P	A	02428	-31,027	3,848	0.13407	37.07	02429	-	2,248	0.13407	72.07	02430	-33,196	2,842	0.13407	50.29
	P		0	0	0.13407	-		181,932	608	0.13407	NS		-	0	0	0.13407
			120,806													
P	A	01056	10,968	25,553	0.13407	5.37	02426	74,304	8,168	0.13407	15.80	02427	99,824	17,134	0.13407	7.34
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A	02428	-64,234	4,347	0.13407	33.80	02429	-	38,619	0.13407	4.07	02430	-21,139	1,860	0.13407	76.01
	P		0	0	0.13407	-		143,783	0	0.13407	-		11,563	1,990	0.13407	68.92
P	A	02428	244,588	7,240	0.13407	14.76	02429	-64,025	16,823	0.13407	8.73	02430	-32,741	9,637	0.13407	14.83
	P		-	1,132	0.13407	NS		20,898	820	0.13407	NS		25,095	771	0.13407	NS
			-	-	-	-		-	-	-	-		-	-	-	-



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
			108,671													
S	A		-35,040	3,866	0.13407	37.03		-	99,601	0.13407	1.56		-	53,132	0.13407	2.92
	P		39,143	3,292	0.13407	40.58		130,754 4,077	3,311	0.13407	41.71		126,962 8,495	2,439	0.13407	56.39
P	A	02431	-18,261	8,354	0.13407	16.88	02432	2,176	5,687	0.13407	24.33	02433	23,411	2,224	0.13407	60.98
	P		48,497	660	0.13407	NS		67,648	426	0.13407	NS		24,947	835	0.13407	NS
S	A		-96,274	42,488	0.13407	3.56		-68,468	29,507	0.13407	5.00		-37,519	16,758	0.13407	8.56
	P		10,250	2,766	0.13407	49.65		16,143	2,647	0.13407	51.59		22,657	1,727	0.13407	78.58
P	A	02434	39,168	6,445	0.13407	20.73	02435	-31,204	152	0.13407	NS	02436	-1,320	1,559	0.13407	89.04
	P		35,537	195	0.13407	NS		10,556	1,004	0.13407	NS		14,451	1,253	0.13407	NS
S	A		-29,068	5,654	0.13407	25.19		-	6,236	0.13407	24.47		-82,080	6,044	0.13407	24.69
	P		0	0	0.13407	-		108,259 17,278	757	0.13407	NS		14,059	262	0.13407	NS
P	A	02437	9,819	2,590	0.13407	53.04	02438	34,570	6,541	0.13407	20.51	02439	0	0	0.13407	-
	P		17,838	1,158	0.13407	NS		0	0	0.13407	-		2,560	7,558	0.13407	18.30
S	A		-57,786	5,490	0.13407	26.61		-61,231	4,560	0.13407	32.14		25,469	254	0.13407	NS
	P		0	0	0.13407	-		0	0	0.13407	-		-	23,733	0.13407	6.43
													108,373			
P	A	02440	0	0	0.13407	-	02441	23,122	1,049	0.13407	NS	02442	12,105	5,065	0.13407	27.06
	P		5,855	4,697	0.13407	29.36		6,808	2,084	0.13407	66.11		5,318	414	0.13407	NS
S	A		22,796	918	0.13407	NS		16,491	1,890	0.13407	72.23		-2,984	2,935	0.13407	47.37
	P		-90,164	16,615	0.13407	9.04		-82,223	10,174	0.13407	14.67		-66,233	3,204	0.13407	45.94
P	A	02443	42,349	15,879	0.13407	8.39	02444	0	0	0.13407	-	02445	18,610	451	0.13407	NS
	P		0	0	0.13407	-		12,480	10,252	0.13407	13.37		10,544	5,205	0.13407	26.37
S	A		-99,776	5,644	0.13407	26.84		29,882	1,164	0.13407	NS		19,718	2,049	0.13407	66.42
	P		0	0	0.13407	-		-96,273	32,354	0.13407	4.67		-93,937	23,050	0.13407	6.54
P	A	02446	23,672	2,802	0.13407	48.39	02447	11,740	11,758	0.13407	11.66	02448	0	0	0.13407	-
	P		-1,985	1,692	0.13407	82.09		0	0	0.13407	-		19,454	11,765	0.13407	11.57
S	A		1,151	2,964	0.13407	46.73		-49,751	3,174	0.13407	45.70		40,878	746	0.13407	NS
	P		-73,646	12,353	0.13407	11.99		-60,630	1,688	0.13407	86.77		-97,303	36,273	0.13407	4.17
P	A	02449	0	0	0.13407	-	02450	27,401	1,296	0.13407	NS	02451	4,306	5,680	0.13407	24.31
	P		17,177	7,793	0.13407	17.51		-11,454	3,039	0.13407	46.11		-6,752	388	0.13407	NS
S	A		26,238	1,478	0.13407	91.51		7,085	2,431	0.13407	56.65		-18,180	3,263	0.13407	43.21
	P		-90,680	26,841	0.13407	5.60		-82,061	17,564	0.13407	8.50		-61,574	7,300	0.13407	20.08
P	A	02452	5,820	20,975	0.13407	6.57	02453	0	0	0.13407	-	02454	34,214	100	0.13407	NS
	P		0	0	0.13407	-		24,259	6,983	0.13407	19.41		15,950	3,187	0.13407	42.86
S	A		-58,108	3,099	0.13407	47.16		38,390	349	0.13407	NS		12,844	903	0.13407	NS
	P		0	0	0.13407	-		-98,243	18,457	0.13407	8.20		-91,985	12,706	0.13407	11.84
P	A	02455	42,437	1,792	0.13407	74.30	02456	13,046	9,865	0.13407	13.88	02457	35,735	176	0.13407	NS
	P		149	1,660	0.13407	83.51		0	0	0.13407	-		12,983	663	0.13407	NS
S	A		-8,529	1,971	0.13407	70.90		-33,978	2,363	0.13407	60.53		-	8,248	0.13407	18.40
	P		-67,021	6,670	0.13407	22.08		-46,517	1,293	0.13407	NS		101,782			
P	A	02458	0	0	0.13407	-	02459	11,809	1,030	0.13407	NS	02460	72,518	866	0.13407	NS
	P		14,006	1,286	0.13407	NS		10,853	1,433	0.13407	95.77		21,976	2,548	0.13407	53.30
S	A		-97,454	8,161	0.13407	18.53		-72,843	6,048	0.13407	24.48		4,748	978	0.13407	NS
	P		23,033	1,243	0.13407	NS		-7,974	1,983	0.13407	70.44		-54,087	4,010	0.13407	36.32
P	A	02461	73,655	9,849	0.13407	13.11							-10,731	2,086	0.13407	67.13
	P		0	0	0.13407	-										
S	A		-34,899	3,134	0.13407	45.68										
	P		-1,040	632	0.13407	NS										
Piano Terra			Parete P1-P2-P3								Parete P2-P3					
P	A	00040	51,629	19,571	0.13407	6.74	00041	29,633	11,372	0.13407	11.85	00042	38,408	13,087	0.13407	10.21
	P		15,574	2,287	0.13407	59.74		7,909	544	0.13407	NS		0	0	0.13407	-
S	A		-9,371	2,963	0.13407	47.20		5,733	2,260	0.13407	61.02		7,279	1,858	0.13407	74.11
	P		2,592	1,025	0.13407	NS		-6,738	378	0.13407	NS		5,653	249	0.13407	NS
P	A	00043	25,607	14,393	0.13407	9.40	00044	20,029	12,563	0.13407	10.83	00045	-1,862	10,489	0.13407	13.24
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-5,389	3,717	0.13407	37.49		-33,312	3,295	0.13407	43.38		-	3,619	0.13407	43.06
	P		0	0	0.13407	-		-21,386	1,121	0.13407	NS		133,657			
P	A	00046	8,999	2,252	0.13407	61.05	00047	101,518	18,915	0.13407	6.63	00055	11,684	56	0.13407	NS
	P		16,936	801	0.13407	NS		107,945	5,784	0.13407	21.55		199,129	6,379	0.13407	17.68
S	A		-75,263	51	0.13407	NS		-	62,240	0.13407	2.62		19,806	2,328	0.13407	58.45
	P		-	4,691	0.13407	32.31		191,010					-90,213	14,034	0.13407	10.71
			100,262					0	0	0.13407	-		91,085	1,664	0.13407	76.23
P	A	00137	132,590	36,655	0.13407	3.31	00139	12,935	1,465	0.13407	93.50	00182	-	78,281	0.13407	2.23
	P		10,364	2,673	0.13407	51.37		-27,003	893	0.13407	NS		284,113	0	0.13407	-
S	A		-46,028	16,353	0.13407	8.84		-8,572	87	0.13407	NS		-	125,506	0.13407	1.40
	P		2,162	9,991	0.13407	13.85		3,398	194	0.13407	NS		293,169			
P	A	00416	44,331	5,125	0.13407	25.93	00517	3,151	1,499	0.13407	92.22	00518	582,422	17,498	0.13407	3.59
	P		115,910	2,967	0.13407	41.66		118,955	2,240	0.13407	55.01		5,443	3,206	0.13407	43.03
S	A		-80,334	4,444	0.13407	33.53		-25,264	1,325	0.13407	NS		76,966	1,417	0.13407	90.81
	P		-	1,819	0.13407	85.47		-14,194	10,045	0.13407	13.98		-36,281	6,107	0.13407	23.47
			130,783										-19,468	8,119	0.13407	17.39
P	A	00519	-1,185	3,778	0.13407	36.74	00520	11,549	6,720	0.13407	20.41	00521	3,906	8,372	0.13407	16.50
	P		49,304	952	0.13407	NS		51,580	1,703	0.13407	77.49		37,038	533	0.13407	NS
																NS



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
S	A		-46,365	17,282	0.13407	8.37		-51,993	22,941	0.13407	6.34		-81,804	33,130	0.13407	4.50
	P		-10,924	7,113	0.13407	19.69		3,690	5,561	0.13407	24.85		-11,794	3,896	0.13407	35.98
P	A	00522	-19,969	8,186	0.13407	17.25	00523	-98	12,515	0.13407	11.08	00524	21,035	11,748	0.13407	11.57
	P		31,419	1,011	0.13407	NS		39,845	287	0.13407	NS		0	0	0.13407	-
S	A		-96,222	45,545	0.13407	3.32		-	47,070	0.13407	3.28		-	57,791	0.13407	2.67
	P		8,691	3,813	0.13407	36.07		121,172					123,090			
P	A	00549	196,792	6,292	0.13407	17.97	00550	150,707	2,871	0.13407	41.48	00551	57,987	3,130	0.13407	41.90
	P		40,119	2,320	0.13407	57.52		7,473	483	0.13407	NS		47,694	649	0.13407	NS
S	A		38,002	7,581	0.13407	17.64		-297	11,072	0.13407	12.53		-17,871	10,230	0.13407	13.78
	P		28,157	3,147	0.13407	42.90		30,079	3,091	0.13407	43.59		9,815	3,325	0.13407	41.32
P	A	00552	30,246	4,367	0.13407	30.85	00553	23,790	4,503	0.13407	30.11	00554	3,279	3,985	0.13407	34.68
	P		23,734	920	0.13407	NS		23,664	580	0.13407	NS		666	912	0.13407	NS
S	A		-25,385	16,690	0.13407	8.50		-35,447	20,876	0.13407	6.86		-33,419	14,270	0.13407	10.02
	P		11,508	3,825	0.13407	35.86		9,423	4,233	0.13407	32.47		7,192	3,371	0.13407	40.85
P	A	00555	4,329	3,447	0.13407	40.06	00556	-21,526	1,915	0.13407	73.85	00963	35,985	12,201	0.13407	10.98
	P		14,453	430	0.13407	NS		12,846	307	0.13407	NS		5,021	97	0.13407	NS
S	A		-28,468	16,188	0.13407	8.79		-31,726	6,517	0.13407	21.90		6,827	946	0.13407	NS
	P		10,666	3,792	0.13407	36.20		18,273	2,727	0.13407	49.97		-1,253	669	0.13407	NS
P	A	00965	31,396	15,018	0.13407	8.96	00966	92,216	26,978	0.13407	4.70	00968	51,603	14,397	0.13407	9.17
	P		0	0	0.13407	-		15,102	3,765	0.13407	36.31		8,339	1,457	0.13407	94.42
S	A		9,373	1,810	0.13407	75.93		-7,334	2,962	0.13407	47.13		2,804	1,874	0.13407	73.79
	P		8,055	232	0.13407	NS		11,079	2,311	0.13407	59.37		-2,607	928	0.13407	NS
P	A	00971	21,330	13,970	0.13407	9.73	00973	12,639	12,006	0.13407	11.41	00975	23,263	7,315	0.13407	18.54
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-18,861	2,340	0.13407	60.29		-76,663	2,490	0.13407	59.65		-88,815	2,602	0.13407	57.68
	P		10,789	178	0.13407	NS		11,439	130	0.13407	NS		15,664	148	0.13407	NS
P	A	01011	-26,269	3,849	0.13407	36.90	01012	-45,474	9,174	0.13407	15.75	01013	-64,238	19,194	0.13407	7.66
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-14,481	1,636	0.13407	85.89		-30,805	2,188	0.13407	65.18		-49,086	4,121	0.13407	35.18
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	01014	-49,366	18,384	0.13407	7.89	01015	-62,916	20,263	0.13407	7.24	01016	-41,659	21,242	0.13407	6.78
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-56,744	5,298	0.13407	27.55		-59,746	5,539	0.13407	26.42		-73,640	4,920	0.13407	30.11
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	01017	-51,140	18,277	0.13407	7.95	01018	-66,994	14,908	0.13407	9.88	01019	-	18,141	0.13407	8.53
	P		0	0	0.13407	-		0	0	0.13407	-		125,363			
S	A		-70,270	3,820	0.13407	38.67		-51,656	5,319	0.13407	27.32		-42,236	125	0.13407	NS
	P		0	0	0.13407	-		-3,527	234	0.13407	NS		-25,267	10,970	0.13407	12.94
P	A	02173	-24,069	1,466	0.13407	96.69	02174	99,286	2,889	0.13407	43.54	02175	3,135	1,379	0.13407	NS
	P		0	0	0.13407	-		7,106	214	0.13407	NS		118,579	14,208	0.13407	8.68
S	A		-17,309	1,442	0.13407	97.70		-93,539	3,663	0.13407	41.14		0	0	0.13407	-
	P		-915	397	0.13407	NS		40,262	849	0.13407	NS		-10,726	1,047	0.13407	NS
P	A	02176	-13,040	16,350	0.13407	8.58	02177	-38,545	6,677	0.13407	21.51	02178	797	1,309	0.13407	NS
	P		0	0	0.13407	-		0	0	0.13407	-		3,705	1,126	0.13407	NS
S	A		193,925	8,912	0.13407	12.19		-52,991	10,634	0.13407	13.42		-10,849	1,947	0.13407	71.93
	P		0	0	0.13407	-		0	0	0.13407	-		-52,885	7,059	0.13407	20.61
P	A	02179	7,990	956	0.13407	NS	02180	45,388	823	0.13407	NS	02181	0	0	0.13407	-
	P		2,472	1,965	0.13407	70.39		941	1,450	0.13407	95.53		73,744	7,159	0.13407	18.03
S	A		-54,105	4,229	0.13407	34.44		-6,517	2,427	0.13407	57.47		0	0	0.13407	-
	P		10,720	848	0.13407	NS		-6,393	404	0.13407	NS		-10,627	1,531	0.13407	91.45
P	A	02182	-63,932	3,474	0.13407	42.28	02183	-19,393	891	0.13407	NS	02184	-14,227	182	0.13407	NS
	P		-12,943	2,208	0.13407	63.55		-7,296	5,750	0.13407	24.28		13,984	832	0.13407	NS
S	A		26,248	1,664	0.13407	81.28		21,674	1,409	0.13407	96.41		498	4,343	0.13407	31.91
	P		-68,071	1,633	0.13407	90.28		-56,317	3,207	0.13407	45.50		10,206	1,281	0.13407	NS
P	A	02185	39,887	3,756	0.13407	35.54	02186	-67,046	7,264	0.13407	20.28	02187	-40,224	3,174	0.13407	45.32
	P		0	0	0.13407	-		0	0	0.13407	-		-45,967	1,987	0.13407	72.76
S	A		3,047	1,069	0.13407	NS		-984	1,136	0.13407	NS		-9,931	7,174	0.13407	19.50
	P		-19,460	1,702	0.13407	82.94		-53,187	1,047	0.13407	NS		20,708	1,705	0.13407	79.74
P	A	02188	-15,226	1,054	0.13407	NS	02189	12,286	2,134	0.13407	64.22	02190	-51,087	5,886	0.13407	24.68
	P		-1,526	7,401	0.13407	18.76		3,958	3,089	0.13407	44.72		29,955	7,742	0.13407	17.41
S	A		20,129	1,733	0.13407	78.50		12,652	1,508	0.13407	90.85		0	0	0.13407	-
	P		-41,404	6,595	0.13407	21.83		-28,567	4,138	0.13407	34.40		4,085	839	0.13407	NS
P	A	02191	-56,580	2,765	0.13407	52.78	02192	-30,520	1,184	0.13407	NS	02193	2,796	377	0.13407	NS
	P		-20,065	4,433	0.13407	31.86		-3,877	8,308	0.13407	16.75		-6,244	1,282	0.13407	NS
S	A		6,257	1,098	0.13407	NS		19,845	1,346	0.13407	NS		3,316	5,529	0.13407	25.00
	P		-41,247	4,277	0.13407	33.66		-38,813	7,241	0.13407	19.84		19,868	1,276	0.13407	NS
P	A	02194	16,998	3,114	0.13407	43.82	02195	-54,457	4,168	0.13407	34.95	02196	-30,167	5,915	0.13407	24.10
	P		-1,880	298	0.13407	NS		0	0	0.13407	-		10,206	1,281	0.13407	NS
S	A		6,079	792	0.13407	NS		-5,269	710	0.13407	NS		-40,224	3,174	0.13407	45.32
	P		-23,832	2,140	0.13407	66.23		-30,709	1,205	0.13407	NS		-45,967	1,987	0.13407	72.76
P	A	02197	-11,437	571	0.13407	NS	02198	2,592	1,441	0.13407	95.98	02199	-9,931	7,174	0.13407	19.50
	P		5,815	5,467	0.13407	25.22		6,647	1,704	0.13407	80.86		20,708	1,705	0.13407	79.74
S	A		14,327	451	0.13407	NS		15,274	499	0.13407	NS		-51,087	5,886	0.13407	24.68
	P		-27,532	4,785	0.13407	29.72		-17,843	2,315	0.13407	60.89		29,955	7,742	0.13407	17.41
P	A	02200	-21,602	770	0.13407	NS	02201	-306	65	0.13407	NS	02202	4,085	839	0.13407	NS
	P		-7,438	1,809	0.13407	77.17		10,908	2,412	0.13407	56.90		16,446	177	0.13407	NS
S	A		0	0	0.13407	-		-34,782	1,506	0.13407	95.04		22,485	1,012	0.13407	NS
	P		6,357	551	0.13407	NS		10,704	1,276	0.13407	NS		-23,449	2,486	0.13407	56.99
													15,993	1,164	0.13407	NS



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
P	A	02203	45,052	2,919	0.13407	45.50										
	P		6,897	539	0.13407	NS										
S	A		-21,135	2,292	0.13407	61.68										
	P		12,471	876	0.13407	NS										
Piano Terra			PareteP4-P5-P6									Parete P4-P5				
P	A	00004	21,917	515	0.13407	NS	00051	-	1,699	0.13407	96.54	00052	0	0	0.13407	-
	P		-88,838	35,205	0.13407	4.26		197,735								
S	A		4,088	3,490	0.13407	39.57		427,335	13,868	0.13407	5.99		155,176	41,349	0.13407	2.87
	P		-	138,852	0.13407	1.13		86,708	1,045	0.13407	NS		-35,778	5,488	0.13407	26.10
			143,608					-21,508	10,742	0.13407	12.87		-44,790	15,202	0.13407	9.50
P	A	00094	0	0	0.13407	-	00095	0	0	0.13407	-	00096	0	0	0.13407	-
	P		61,715	27,050	0.13407	4.83		21,531	21,464	0.13407	6.33		-386	28,823	0.13407	4.81
S	A		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
	P		-54,622	7,411	0.13407	19.66		-73,242	5,847	0.13407	25.33		-68,840	4,885	0.13407	30.20
P	A	00097	0	0	0.13407	-	00098	0	0	0.13407	-	00099	0	0	0.13407	-
	P		5,195	35,328	0.13407	3.91		13,434	33,012	0.13407	4.15		51,889	28,128	0.13407	4.69
S	A		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
	P		-87,257	7,083	0.13407	21.16		-	8,229	0.13407	18.72		-	9,393	0.13407	16.54
								119,675					129,570			
P	A	00100	0	0	0.13407	-	00101	70,258	2,368	0.13407	54.71	00102	63,179	8,046	0.13407	16.21
	P		64,950	17,086	0.13407	7.62		21,566	11,540	0.13407	11.77		-23,719	10,395	0.13407	13.63
S	A		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
	P		-50,070	5,784	0.13407	25.09		-13,798	2,478	0.13407	56.67		29,238	1,476	0.13407	91.37
P	A	00509	0	0	0.13407	-	00510	36,030	606	0.13407	NS	00511	26,052	243	0.13407	NS
	P		13,890	12,888	0.13407	10.62		-7,782	12,215	0.13407	11.43		-24,308	8,832	0.13407	16.05
S	A		77,459	359	0.13407	NS		21,610	2,849	0.13407	47.68		10,056	3,732	0.13407	36.80
	P		-	59,458	0.13407	2.57		-	47,131	0.13407	3.25		-97,809	45,207	0.13407	3.35
			111,596					114,195								
P	A	00512	31,701	1,560	0.13407	86.24	00513	45,616	1,446	0.13407	91.80	00514	42,273	2,089	0.13407	63.75
	P		-8,259	7,755	0.13407	18.02		3,301	6,733	0.13407	20.53		-17,241	3,035	0.13407	46.42
S	A		-11,709	4,766	0.13407	29.41		1,675	6,205	0.13407	22.31		-14,371	8,900	0.13407	15.79
	P		-84,062	33,111	0.13407	4.51		-59,156	21,962	0.13407	6.66		-57,051	16,602	0.13407	8.79
P	A	00515	71,066	2,159	0.13407	59.95	00516	119,851	3,918	0.13407	31.42	00533	31,071	970	0.13407	NS
	P		-4,010	2,788	0.13407	49.91		9,676	981	0.13407	NS		-67,599	25,418	0.13407	5.80
S	A		-22,155	9,718	0.13407	14.56		-14,341	12,128	0.13407	11.58		3,609	4,223	0.13407	32.72
	P		-54,394	5,070	0.13407	28.73		-52,102	327	0.13407	NS		-	126,364	0.13407	1.23
													127,725			
P	A	00534	38,262	1,142	0.13407	NS	00535	72,636	781	0.13407	NS	00536	76,347	1,596	0.13407	80.67
	P		-42,076	25,166	0.13407	5.73		-14,838	18,825	0.13407	7.47		-10,034	15,340	0.13407	9.12
S	A		6,869	4,152	0.13407	33.18		8,733	5,888	0.13407	23.35		15,260	5,460	0.13407	25.03
	P		-	101,023	0.13407	1.51		-97,321	96,647	0.13407	1.56		-64,776	71,188	0.13407	2.06
			104,188													
P	A	00537	107,633	1,563	0.13407	79.78	00538	167,788	1,582	0.13407	73.88	00539	186,080	1,461	0.13407	78.36
	P		32,202	12,360	0.13407	10.88		36,603	6,960	0.13407	19.24		68,651	3,893	0.13407	33.33
S	A		5,187	7,169	0.13407	19.25		31,292	8,997	0.13407	14.96		49,807	7,354	0.13407	17.98
	P		-47,336	45,599	0.13407	3.17		-23,184	42,438	0.13407	3.34		-24,049	15,627	0.13407	9.07
P	A	00540	29,150	6,238	0.13407	21.62	00598	19,745	596	0.13407	NS	00599	17,806	849	0.13407	NS
	P		419,388	1,326	0.13407	63.39		-47,988	17,866	0.13407	8.11		-31,938	13,708	0.13407	10.41
S	A		127,811	3,587	0.13407	34.03		4,363	2,679	0.13407	51.54		14,610	1,786	0.13407	76.57
	P		-94,675	5,343	0.13407	28.23		-	79,336	0.13407	1.97		-	40,078	0.13407	3.89
								139,869					135,524			
P	A	00600	13,443	818	0.13407	NS	00601	-1,764	9,071	0.13407	15.31	00602	4,485	11,140	0.13407	12.39
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		16,615	924	0.13407	NS		-	20,831	0.13407	7.39		-	32,730	0.13407	4.67
	P		-	4,789	0.13407	32.41		118,243	0	0.13407	-		109,146	216	0.13407	NS
			128,612					0					29,646			
P	A	00603	13,560	15,914	0.13407	8.60	00604	16,603	15,727	0.13407	8.68	00605	19,370	15,055	0.13407	9.04
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-	40,596	0.13407	3.74		-97,625	42,262	0.13407	3.58		-89,274	37,732	0.13407	3.98
	P		101,451													
			33,732	549	0.13407	NS		38,557	540	0.13407	NS		49,192	341	0.13407	NS
P	A	00606	25,261	10,261	0.13407	13.19	00607	-2,417	830	0.13407	NS	00608	0	0	0.13407	-
	P		0	0	0.13407	-		0	0	0.13407	-		44,074	5,467	0.13407	24.32
S	A		-89,624	23,856	0.13407	6.30		-79,548	2,520	0.13407	59.09		85,048	259	0.13407	NS
	P		50,086	66	0.13407	NS		-2,252	50	0.13407	NS		-98,060	23,368	0.13407	6.47
P	A	00947	0	0	0.13407	-	00948	76,022	6,525	0.13407	19.74	00951	0	0	0.13407	-
	P		55,363	10,860	0.13407	12.11		-2,104	12,839	0.13407	10.82		66,246	23,006	0.13407	5.65
S	A		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
	P		-48,562	4,964	0.13407	29.19		10,631	1,743	0.13407	78.75		-36,006	3,307	0.13407	43.33
P	A	00953	0	0	0.13407	-	00955	0	0	0.13407	-	00957	0	0	0.13407	-
	P		14,643	25,510	0.13407	5.36		40,298	29,478	0.13407	4.53		64,508	23,522	0.13407	5.54
S	A		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
	P		-58,485	4,187	0.13407	34.92		-	9,089	0.13407	16.70		-	10,855	0.13407	14.17
								102,237					117,475			
P	A	00958	0	0	0.13407	-	00961	0	0	0.13407	-	02462	0	0	0.13407	-
	P		-1,420	30,777	0.13407	4.51		13,042	34,117	0.13407	4.01		59,188	8,027	0.13407	16.32
S	A		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
	P		-70,375	4,896	0.13407	30.17		-88,049	9,209	0.13407	16.29		-	39,771	0.13407	3.89



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
													126,155			
P	A	02463	0	0	0.13407	-	02464	-87,061	1,002	0.13407	NS	02465	20,873	825	0.13407	NS
	P		117,087	16,357	0.13407	7.55		220,653	7,230	0.13407	15.21		-64,620	16,961	0.13407	8.67
S	A		-23,619	1,814	0.13407	78.11		29,718	2,250	0.13407	59.91		3,854	3,303	0.13407	41.82
	P		-56,128	1,186	0.13407	NS		-31,808	4,286	0.13407	33.31		-	100,512	0.13407	1.55
													131,752			
P	A	02466	24,998	764	0.13407	NS	02467	48,703	699	0.13407	NS	02468	68,658	349	0.13407	NS
	P		-34,741	9,935	0.13407	14.41		-16,694	8,421	0.13407	16.72		11,216	5,124	0.13407	26.77
S	A		8,551	2,387	0.13407	57.62		10,002	2,668	0.13407	51.48		15,899	2,595	0.13407	52.63
	P		-	52,559	0.13407	2.94		-96,374	41,928	0.13407	3.60		-70,857	29,091	0.13407	5.08
			123,881													
P	A	02469	26,422	675	0.13407	NS	02470	32,678	658	0.13407	NS	02471	11,283	988	0.13407	NS
	P		22,821	3,138	0.13407	43.24		45,996	6,701	0.13407	19.80		-31,082	143	0.13407	NS
S	A		23,670	1,637	0.13407	82.82		0	0	0.13407	-		17,188	751	0.13407	NS
	P		-35,552	16,051	0.13407	8.92		-27,523	5,721	0.13407	24.86		-	6,095	0.13407	25.03
													108,223			
P	A	02472	15,884	1,255	0.13407	NS	02473	20,634	1,136	0.13407	NS	02474	0	0	0.13407	-
	P		-459	1,428	0.13407	97.13		13,309	2,573	0.13407	53.22		42,464	6,876	0.13407	19.36
S	A		14,054	257	0.13407	NS		0	0	0.13407	-		0	0	0.13407	-
	P		-82,497	5,909	0.13407	25.26		-57,940	5,368	0.13407	27.22		-62,505	4,559	0.13407	32.18
P	A	02475	1,930	7,547	0.13407	18.34	02476	6,405	4,740	0.13407	29.07	02477	10,374	2,052	0.13407	66.91
	P		0	0	0.13407	-		0	0	0.13407	-		23,539	1,053	0.13407	NS
S	A		-	23,825	0.13407	6.40		-90,853	16,704	0.13407	9.00		-83,136	10,258	0.13407	14.56
			108,048													
	P		25,478	247	0.13407	NS		22,749	905	0.13407	NS		16,804	1,857	0.13407	73.49
P	A	02478	6,295	327	0.13407	NS	02479	0	0	0.13407	-	02480	11,355	10,267	0.13407	13.36
	P		15,439	5,140	0.13407	26.58		42,441	16,303	0.13407	8.17		0	0	0.13407	-
S	A		-66,087	3,394	0.13407	43.36		0	0	0.13407	-		-96,127	32,410	0.13407	4.66
	P		-1,514	2,875	0.13407	48.29		-97,935	5,113	0.13407	29.58		29,988	1,136	0.13407	NS
P	A	02481	11,123	5,256	0.13407	26.10	02482	-1,127	1,633	0.13407	84.99	02483	0	0	0.13407	-
	P		18,469	412	0.13407	NS		24,523	2,795	0.13407	48.47		14,161	11,983	0.13407	11.42
S	A		-95,048	23,100	0.13407	6.53		-74,866	12,442	0.13407	11.92		-56,240	2,044	0.13407	71.38
	P		19,699	2,017	0.13407	67.47		1,444	2,902	0.13407	47.71		-46,917	3,022	0.13407	47.88
P	A	02484	17,865	11,659	0.13407	11.69	02485	15,254	7,828	0.13407	17.46	02486	-11,274	3,085	0.13407	45.41
	P		0	0	0.13407	-		0	0	0.13407	-		27,192	1,216	0.13407	NS
S	A		-95,190	36,300	0.13407	4.16		-90,733	26,884	0.13407	5.59		-84,338	17,588	0.13407	8.50
	P		41,221	690	0.13407	NS		26,500	1,420	0.13407	95.22		6,824	2,382	0.13407	57.83
P	A	02487	-4,806	282	0.13407	NS	02488	0	0	0.13407	-	02489	19,237	6,953	0.13407	19.58
	P		6,833	5,744	0.13407	23.98		9,670	21,571	0.13407	6.37		0	0	0.13407	-
S	A		-64,094	7,363	0.13407	19.95		0	0	0.13407	-		-95,130	18,491	0.13407	8.16
	P		-17,736	3,206	0.13407	43.96		-76,645	3,242	0.13407	45.81		39,864	255	0.13407	NS
P	A	02490	12,792	3,293	0.13407	41.60	02491	7,585	1,720	0.13407	80.04	02492	0	0	0.13407	-
	P		0	0	0.13407	-		41,752	1,622	0.13407	82.15		16,072	10,309	0.13407	13.25
S	A		-93,398	12,719	0.13407	11.85		-71,846	6,698	0.13407	22.08		-16,605	1,069	0.13407	NS
	P		12,888	769	0.13407	NS		-9,157	1,847	0.13407	75.70		-31,642	2,232	0.13407	63.95
P	A	02493	7,676	591	0.13407	NS	02494	11,053	1,291	0.13407	NS	02495	10,000	1,554	0.13407	88.39
	P		29,262	198	0.13407	NS		0	0	0.13407	-		1,788	839	0.13407	NS
S	A		76,313	888	0.13407	NS		23,839	1,495	0.13407	90.68		-8,983	2,158	0.13407	64.78
	P		-93,312	8,432	0.13407	17.87		-96,989	8,205	0.13407	18.42		-77,137	5,845	0.13407	25.42
P	A	02496	9,536	1,177	0.13407	NS	02497	0	0	0.13407	-	02498	98,278	6,027	0.13407	20.89
	P		14,550	2,112	0.13407	64.75		76,592	10,690	0.13407	12.04		80,290	18,842	0.13407	6.81
S	A		-14,884	2,231	0.13407	63.01		-13,497	440	0.13407	NS		0	0	0.13407	-
	P		-63,278	3,832	0.13407	38.31		-35,711	3,030	0.13407	47.28		-	63,927	0.13407	2.50
													163,076			
Piano Terra			Parete P4-P5-P6									Parete P5-P6				
P	A	00005	443	554	0.13407	NS	00006	0	0	0.13407	-	00007	0	0	0.13407	-
	P		67,651	19,810	0.13407	6.56		15,864	15,880	0.13407	8.60		11,544	17,693	0.13407	7.75
S	A		-26,323	372	0.13407	NS		0	0	0.13407	-		0	0	0.13407	-
	P		-36,622	3,920	0.13407	36.57		-25,612	2,875	0.13407	49.37		-42,031	3,624	0.13407	39.75
P	A	00008	0	0	0.13407	-	00009	0	0	0.13407	-	00010	0	0	0.13407	-
	P		-15,745	17,860	0.13407	7.88		11,028	14,090	0.13407	9.74		-413	11,473	0.13407	12.09
S	A		0	0	0.13407	-		2,468	825	0.13407	NS		0	0	0.13407	-
	P		-36,542	5,175	0.13407	27.70		-21,393	1,826	0.13407	77.44		-21,531	5,294	0.13407	26.71
P	A	00011	0	0	0.13407	-	00052	0	0	0.13407	-	00053	0	0	0.13407	-
	P		26,877	8,113	0.13407	16.66		155,176	41,349	0.13407	2.87		216,084	11,935	0.13407	9.27
S	A		-85,170	306	0.13407	NS		-35,778	5,488	0.13407	26.10		188,617	1,807	0.13407	61.79
	P		83,356	1,530	0.13407	83.56		-44,790	15,202	0.13407	9.50		-18,591	12,290	0.13407	11.27
P	A	00138	-23,372	758	0.13407	NS	00183	0	0	0.13407	-	00418	1,636	1,593	0.13407	86.90
	P		13,483	1,908	0.13407	71.75		-	75,200	0.13407	2.31		90,088	26,523	0.13407	4.79
								276,425								
S	A		-243	44	0.13407	NS		606,880	21,508	0.13407	2.77		-44,678	1,069	0.13407	NS
	P		-6,289	251	0.13407	NS		-	113,663	0.13407	1.48		-25,63			



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
S	A		-11,709	4,766	0.13407	29.41		1,675	6,205	0.13407	22.31		-14,371	8,900	0.13407	15.79
	P		-84,062	33,111	0.13407	4.51		-59,156	21,962	0.13407	6.66		-57,051	16,602	0.13407	8.79
P	A	00515	71,066	2,159	0.13407	59.95	00516	119,851	3,918	0.13407	31.42	00525	13,011	138	0.13407	NS
	P		-4,010	2,788	0.13407	49.91		9,676	981	0.13407	NS		-21,275	2,153	0.13407	65.67
S	A		-22,155	9,718	0.13407	14.56		-14,341	12,128	0.13407	11.58		19,301	2,718	0.13407	50.09
	P		-54,394	5,070	0.13407	28.73		-52,102	327	0.13407	NS		-33,777	6,902	0.13407	20.72
P	A	00526	15,008	644	0.13407	NS	00527	-279	872	0.13407	NS	00528	15,386	1,023	0.13407	NS
	P		7,433	2,911	0.13407	47.30		12,657	4,824	0.13407	28.40		17,937	4,105	0.13407	33.21
S	A		11,406	3,700	0.13407	37.07		8,201	3,844	0.13407	35.79		3,952	4,069	0.13407	33.95
	P		-27,226	13,396	0.13407	10.61		-30,040	15,607	0.13407	9.13		-39,700	14,965	0.13407	9.61
P	A	00529	35,447	836	0.13407	NS	00530	44,423	1,279	0.13407	NS	00531	113,327	1,002	0.13407	NS
	P		32,585	3,656	0.13407	36.77		50,075	3,377	0.13407	39.14		132,543	1,216	0.13407	99.88
S	A		12,196	5,256	0.13407	26.08		8,309	5,102	0.13407	26.96		30,117	5,584	0.13407	24.13
	P		-28,450	17,047	0.13407	8.35		-15,474	10,096	0.13407	13.93		338	6,125	0.13407	22.63
P	A	00532	14,297	5,819	0.13407	23.51	01020	0	0	0.13407	-	01021	0	0	0.13407	-
	P		173,655	2,296	0.13407	50.57		-25,793	3,908	0.13407	36.33		-44,798	9,192	0.13407	15.71
S	A		33,841	7,775	0.13407	17.27		0	0	0.13407	-		0	0	0.13407	-
	P		15,844	2,101	0.13407	65.01		-12,184	1,713	0.13407	81.86		-27,601	2,219	0.13407	64.09
P	A	01022	0	0	0.13407	-	01023	0	0	0.13407	-	01024	0	0	0.13407	-
	P		-65,825	18,975	0.13407	7.75		-40,075	17,321	0.13407	8.30		-41,904	18,269	0.13407	7.89
S	A		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
	P		-44,762	4,088	0.13407	35.33		-52,741	5,143	0.13407	28.28		-53,947	5,412	0.13407	26.90
P	A	01025	0	0	0.13407	-	01026	0	0	0.13407	-	01027	-33,861	150	0.13407	NS
	P		-33,536	19,861	0.13407	7.20		-58,284	17,375	0.13407	8.41		-73,907	13,830	0.13407	10.71
S	A		0	0	0.13407	-		-9,999	149	0.13407	NS		-4,822	721	0.13407	NS
	P		-68,192	4,681	0.13407	31.50		-64,951	3,569	0.13407	41.19		-47,984	4,680	0.13407	30.95
P	A	01028	-43,374	1,864	0.13407	77.38	01030	0	0	0.13407	-	01032	0	0	0.13407	-
	P		-	17,297	0.13407	9.01		19,601	15,999	0.13407	8.51		49,474	14,169	0.13407	9.33
			133,253													
S	A		-1,219	3,079	0.13407	45.08		-11,266	326	0.13407	NS		0	0	0.13407	-
	P		-31,203	8,754	0.13407	16.30		-36,657	2,903	0.13407	49.39		-20,559	3,518	0.13407	40.16
P	A	01033	0	0	0.13407	-	01036	0	0	0.13407	-	01037	0	0	0.13407	-
	P		25,101	16,052	0.13407	8.43		-3,004	18,201	0.13407	7.64		85,437	6,885	0.13407	18.53
S	A		4,310	337	0.13407	NS		-5,663	169	0.13407	NS		-49,219	2,291	0.13407	63.29
	P		-32,206	3,153	0.13407	45.29		-33,496	2,595	0.13407	55.09		33,678	462	0.13407	NS
P	A	01040	0	0	0.13407	-	01918	0	0	0.13407	-	01919	0	0	0.13407	-
	P		-7,897	14,090	0.13407	9.91		-22,917	1,672	0.13407	84.69		72,148	5,155	0.13407	25.08
S	A		18,703	113	0.13407	NS		-197	377	0.13407	NS		91,837	2,300	0.13407	55.11
	P		-55,518	3,021	0.13407	48.27		-16,582	1,584	0.13407	88.88		-16,082	1,455	0.13407	96.72
P	A	01920	0	0	0.13407	-	01921	0	0	0.13407	-	01922	0	0	0.13407	-
	P		121,971	16,922	0.13407	7.26		-18,657	16,196	0.13407	8.71		-49,579	6,598	0.13407	21.98
S	A		-52,189	289	0.13407	NS		0	0	0.13407	-		0	0	0.13407	-
	P		-54,367	2,153	0.13407	67.65		204,824	8,785	0.13407	12.27		-48,852	9,899	0.13407	14.64
P	A	01923	-18,731	1,699	0.13407	83.03	01924	-8,639	1,854	0.13407	75.38	01925	3,277	1,391	0.13407	99.37
	P		-1,282	1,188	0.13407	NS		635	1,016	0.13407	NS		-5,403	1,031	0.13407	NS
S	A		0	0	0.13407	-		8,829	643	0.13407	NS		-9,779	117	0.13407	NS
	P		-51,332	7,370	0.13407	19.71		-58,667	4,808	0.13407	30.41		-13,299	3,026	0.13407	46.39
P	A	01926	0	0	0.13407	-	01927	-18,743	2,344	0.13407	60.18	01928	-15,800	5,702	0.13407	24.67
	P		69,211	9,171	0.13407	14.14		-71,422	3,324	0.13407	44.48		-30,028	854	0.13407	NS
S	A		0	0	0.13407	-		-66,743	1,733	0.13407	84.97		-58,024	2,896	0.13407	50.46
	P		-28,447	2,750	0.13407	51.75		28,691	1,684	0.13407	80.13		22,062	1,765	0.13407	76.93
P	A	01929	-3,648	4,073	0.13407	34.16	01930	0	0	0.13407	-	01931	0	0	0.13407	-
	P		606	999	0.13407	NS		27,460	4,915	0.13407	27.49		-73,442	6,739	0.13407	21.98
S	A		-48,469	2,473	0.13407	58.59		-44,082	782	0.13407	NS		-51,728	1,129	0.13407	NS
	P		6,147	2,006	0.13407	68.72		-15,390	1,985	0.13407	70.85		1,853	1,117	0.13407	NS
P	A	01932	-15,142	7,252	0.13407	19.39	01933	-8,836	7,333	0.13407	19.06	01934	-5,884	2,720	0.13407	51.25
	P		-55,642	1,863	0.13407	78.27		-29,082	1,144	0.13407	NS		-6,707	2,813	0.13407	49.59
S	A		-51,410	5,813	0.13407	24.99		-45,017	6,232	0.13407	23.18		-37,784	3,468	0.13407	41.38
	P		22,652	1,978	0.13407	68.61		19,624	2,415	0.13407	56.36		6,190	2,632	0.13407	52.37
P	A	01935	0	0	0.13407	-	01936	-21,798	4,592	0.13407	30.81	01937	-6,775	8,359	0.13407	16.69
	P		10,357	10,313	0.13407	13.31		-63,306	2,568	0.13407	57.17		-41,056	1,134	0.13407	NS
S	A		-9,232	78	0.13407	NS		-40,859	4,352	0.13407	33.07		-40,612	7,178	0.13407	20.05
	P		-19,366	1,969	0.13407	71.68		8,785	1,208	0.13407	NS		20,914	1,764	0.13407	77.06
P	A	01938	-550	5,433	0.13407	25.53	01939	0	0	0.13407	-	01940	0	0	0.13407	-
	P		-21,390	1,580	0.13407	89.50		-7,703	4,404	0.13407	31.71		-56,581	3,958	0.13407	36.87
S	A		-33,885	5,687	0.13407	25.15		-28,388	1,682	0.13407	84.61		-29,782	1,258	0.13407	NS
	P		18,332	2,060	0.13407	66.15		-2,582	1,822	0.13407	76.28		-2,566	729	0.13407	NS
P	A	01941	-4,884	6,189	0.13407	22.50	01942	6,321	5,545	0.13407	24.86	01943	8,251	1,722	0.13407	79.89
	P		-38,361	1,002	0.13407	NS		-20,467	560	0.13407	NS		-8,892	1,816	0.13407	76.98
S	A		-36,552	5,085	0.13407	28.19		-33,297	4,958	0.13407	28.83		-22,650	2,537	0.13407	55.80
	P		13,797	633	0.13407	NS		18,013	712	0.13407	NS		18,071	1,093	0.13407	NS
P	A	01944	0	0	0.13407	-	01945	-5,928	2,051	0.13407	67.97	01946	11,754	2,578	0.13407	53.19
	P		-1,054	8,305	0.13407	16.71		-23,912	731	0.13407	NS		0	0	0.13407	-
S	A		14,527	426	0.13407	NS		7,617	602	0.13407	NS		12,963	1,374	0.13407	99.69
	P		-13,808	1,623	0.13407	86.52		0	0	0.13407	-		-35,386	1,287	0.13407	NS
P	A	01947	28,230	1,271	0.13407	NS	01948	5,208	868	0.13407	NS	02498	98,278	6,027	0.13407	20.89
	P		9,099	32	0.13407	NS		36,122	2,393	0.13407	55.98		80,290	18,842	0.13407	6.81
S	A		15,318	1,470	0.13407	92.97		21,128	1,345	0.13407	NS		0	0	0.13407	-
	P		-25,625	1,658	0.13407	85.62		-6,109	1,328	0.13407	NS		-	63,927	0.13407	2.50
													163,076			



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
Piano Terra			PareteP1-P4				Parete P1-P4									
P	A	00004	19,416	679	0.13407	NS	00048	20,289	621	0.13407	NS	00051	-28,777	24,054	0.13407	5.92
	P		-68,959	31,117	0.13407	4.74		-66,478	30,189	0.13407	4.88		445,642	28,538	0.13407	2.83
S	A		4,226	3,525	0.13407	39.18		2,888	3,513	0.13407	39.36		91,522	49,677	0.13407	2.44
	P		-	136,184	0.13407	1.15		-	136,601	0.13407	1.14		-57,485	34,372	0.13407	4.09
			138,414					136,569								
P	A	00054	-	27,453	0.13407	5.66	00103	-	3,724	0.13407	42.36	00104	0	0	0.13407	-
	P		129,944					148,465								
			456,070	26,157	0.13407	3.03		180,477	12,379	0.13407	9.31		69,074	21,236	0.13407	6.11
S	A		109,021	43,307	0.13407	2.76		120,487	2,734	0.13407	43.28		0	0	0.13407	-
	P		-64,802	30,060	0.13407	4.72		104,295	9,913	0.13407	12.15		54,983	5,309	0.13407	23.71
P	A	00105	0	0	0.13407	-	00106	0	0	0.13407	-	00107	0	0	0.13407	-
	P		-6,616	51,908	0.13407	2.69		49,858	77,448	0.13407	1.71		-32,142	107,391	0.13407	1.33
S	A		47,389	990	0.13407	NS		0	0	0.13407	-		16,480	3,851	0.13407	33.87
	P		82,510	18,802	0.13407	6.52		-45,095	12,695	0.13407	11.00		-23,804	18,419	0.13407	7.36
P	A	00108	0	0	0.13407	-	00109	0	0	0.13407	-	00110	0	0	0.13407	-
	P		188,370	119,596	0.26813	2.09		30,052	145,179	0.26813	1.85		63,369	153,175	0.26813	1.73
S	A		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
	P		-39,379	20,181	0.13407	6.90		13,486	25,577	0.13407	5.16		22,250	27,241	0.13407	4.86
P	A	00111	0	0	0.13407	-	00112	0	0	0.13407	-	00113	0	0	0.13407	-
	P		94,675	159,847	0.26813	1.63		47,493	168,313	0.26813	1.58		90,262	172,263	0.26813	1.52
S	A		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
	P		24,976	29,916	0.13407	4.39		63,551	39,227	0.13407	3.23		-9,429	35,207	0.13407	3.89
P	A	00114	0	0	0.13407	-	00115	0	0	0.13407	-	00116	0	0	0.13407	-
	P		51,946	180,064	0.26813	1.48		164,531	176,408	0.26813	1.43		57,044	187,462	0.26813	1.41
S	A		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
	P		7,376	32,606	0.13407	4.22		11,550	34,753	0.13407	3.95		-1,326	35,586	0.13407	3.90
P	A	00117	0	0	0.13407	-	00118	0	0	0.13407	-	00119	0	0	0.13407	-
	P		68,101	175,844	0.26813	1.50		59,247	173,566	0.26813	1.53		104,485	168,486	0.26813	1.54
S	A		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
	P		-10,682	37,898	0.13407	3.62		66,155	39,170	0.13407	3.23		35,299	30,983	0.13407	4.20
P	A	00120	0	0	0.13407	-	00121	0	0	0.13407	-	00122	0	0	0.13407	-
	P		-19,489	163,132	0.26813	1.68		54,688	161,400	0.26813	1.64		200,926	139,131	0.26813	1.78
S	A		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
	P		68,850	36,833	0.13407	3.43		9,297	30,080	0.13407	4.42		-31,891	24,848	0.13407	5.58
P	A	00123	0	0	0.13407	-	00124	0	0	0.13407	-	00125	0	0	0.13407	-
	P		-18,441	130,860	0.26813	2.09		54,367	104,494	0.13407	1.26		-8,848	82,355	0.13407	1.70
S	A		-19,586	72	0.13407	NS		0	0	0.13407	-		0	0	0.13407	-
	P		-31,001	24,685	0.13407	5.54		-48,429	18,891	0.13407	7.41		84,817	25,051	0.13407	4.88
P	A	00126	0	0	0.13407	-	00127	0	0	0.13407	-	00128	72,613	4,396	0.13407	29.40
	P		72,715	52,855	0.13407	2.44		43,550	30,602	0.13407	4.35		-12,880	17,161	0.13407	8.18
S	A		0	0	0.13407	-		60,027	164	0.13407	NS		116,888	1,658	0.13407	71.63
	P		27,246	10,554	0.13407	12.22		34,027	5,626	0.13407	23.13		86,478	2,591	0.13407	47.36
P	A	00415	82,976	11,673	0.13407	10.96	00430	23,281	395	0.13407	NS	00431	-24,768	4,179	0.13407	33.94
	P		-821	12,113	0.13407	11.45		-43,003	10,521	0.13407	13.71		0	0	0.13407	-
S	A		123,531	3,052	0.13407	38.64		3,200	2,752	0.13407	50.23		2,910	1,788	0.13407	77.33
	P		73,135	2,424	0.13407	51.35		-	82,038	0.13407	1.87		-	39,867	0.13407	3.83
								117,727					107,683			
P	A	00432	-7,097	20,744	0.13407	6.73	00433	6,343	36,558	0.13407	3.77	00434	16,080	51,987	0.13407	2.63
	P		-13,986	32	0.13407	NS		1,904	353	0.13407	NS		-5,531	755	0.13407	NS
S	A		3,097	1,007	0.13407	NS		-98,701	12,678	0.13407	11.94		-85,656	25,833	0.13407	5.79
	P		-	12,239	0.13407	12.45		0	0	0.13407	-		5,783	341	0.13407	NS
			106,873													
P	A	00435	23,529	64,015	0.13407	2.12	00436	31,678	75,118	0.13407	1.79	00437	35,461	85,806	0.13407	1.56
	P		-13,576	1,056	0.13407	NS		-17,265	1,417	0.13407	99.42		-21,955	1,929	0.13407	73.34
S	A		-84,982	34,521	0.13407	4.33		-79,062	45,354	0.13407	3.28		-67,518	45,589	0.13407	3.23
	P		4,009	761	0.13407	NS		4,262	1,179	0.13407	NS		4,012	1,289	0.13407	NS
P	A	00438	35,275	94,668	0.13407	1.42	00439	41,974	101,075	0.13407	1.32	00440	44,231	106,730	0.13407	1.25
	P		-26,557	2,081	0.13407	68.27		-28,745	2,428	0.13407	58.63		-30,891	2,885	0.13407	49.44
S	A		-63,807	45,447	0.13407	3.23		-59,360	49,683	0.13407	2.94		-51,486	46,453	0.13407	3.13
	P		2,593	1,405	0.13407	98.44		2,067	1,577	0.13407	87.75		1,091	1,527	0.13407	90.70
P	A	00441	40,316	114,791	0.13407	1.16	00442	44,629	115,647	0.13407	1.15	00443	41,841	122,311	0.13407	1.09
	P		-33,152	2,975	0.13407	48.04		-35,595	3,246	0.13407	44.13		-37,410	3,276	0.13407	43.80
S	A		-47,825	46,315	0.13407	3.13		-45,218	43,755	0.13407	3.30		-42,616	43,463	0.13407	3.32
	P		-3	1,510	0.13407	91.82		-1,120	1,597	0.13407	86.91		-1,351	1,611	0.13407	86.17
P	A	00444	47,857	120,160	0.13407	1.10	00445	47,596	123,893	0.13407	1.07	00446	43,352	125,989	0.13407	1.06
	P		-37,433	3,610	0.13407	39.74		-38,975	3,594	0.13407	39.98		-40,209	3,507	0.13407	41.01
S	A		-41,199	42,50												



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	P		-211	1,544	0.13407	89.81		1,376	1,633	0.13407	84.79		1,653	1,576	0.13407	87.84
P	A	00456	38,032	96,333	0.13407	1.39	00457	35,441	86,010	0.13407	1.56	00458	29,957	78,332	0.13407	1.72
	P		-27,040	2,335	0.13407	60.87		-23,100	1,901	0.13407	74.50		-20,106	1,520	0.13407	92.92
S	A		-61,449	46,057	0.13407	3.18		-72,251	47,975	0.13407	3.08		-78,684	43,679	0.13407	3.41
	P		2,477	1,377	0.13407	NS		4,119	1,379	0.13407	NS		3,575	1,185	0.13407	NS
P	A	00459	24,161	67,191	0.13407	2.02	00460	16,238	52,669	0.13407	2.59	00461	7,210	39,290	0.13407	3.50
	P		-14,057	1,222	0.13407	NS		-7,410	743	0.13407	NS		-2,732	387	0.13407	NS
S	A		-81,666	35,007	0.13407	4.26		-92,061	27,517	0.13407	5.47		-98,787	13,010	0.13407	11.64
	P		4,837	750	0.13407	NS		3,575	372	0.13407	NS		0	0	0.13407	-
P	A	00462	-5,388	23,428	0.13407	5.95	00463	-23,959	5,538	0.13407	25.59	00464	18,156	464	0.13407	NS
	P		6,742	77	0.13407	NS		0	0	0.13407	-		-47,257	11,873	0.13407	12.19
S	A		4,625	965	0.13407	NS		-644	1,885	0.13407	73.60		354	2,731	0.13407	50.75
	P		-	10,582	0.13407	14.35		-	41,386	0.13407	3.69		-	81,920	0.13407	1.88
			102,221					109,275					116,786			
P	A	00533	24,347	1,258	0.13407	NS	00534	48,176	943	0.13407	NS	00535	55,071	1,492	0.13407	88.15
	P		-65,466	27,327	0.13407	5.38		-33,259	23,803	0.13407	6.01		-26,996	19,992	0.13407	7.11
S	A		-2,848	4,137	0.13407	33.60		2,587	5,229	0.13407	26.45		6,625	5,111	0.13407	26.96
	P		-99,160	119,822	0.13407	1.26		-89,606	119,763	0.13407	1.25		-76,089	90,796	0.13407	1.64
P	A	00536	98,310	1,109	0.13407	NS	00537	100,971	1,799	0.13407	69.79	00538	139,905	1,747	0.13407	68.97
	P		1,646	15,983	0.13407	8.66		16,452	11,777	0.13407	11.59		42,884	9,074	0.13407	14.67
S	A		9,376	6,951	0.13407	19.77		17,989	7,063	0.13407	19.30		11,507	7,555	0.13407	18.15
	P		-67,763	75,590	0.13407	1.95		-46,067	59,956	0.13407	2.41		-14,314	26,644	0.13407	5.27
P	A	00539	259,953	968	0.13407	NS	00540	32,536	2,799	0.13407	48.03	00541	57,798	2,652	0.13407	49.46
	P		54,543	3,406	0.13407	38.63		399,085	1,670	0.13407	51.92		429,275	965	0.13407	85.76
S	A		53,821	9,191	0.13407	14.33		172,691	5,125	0.13407	22.68		135,069	4,869	0.13407	24.88
	P		-24,587	22,062	0.13407	6.43		-	3,878	0.13407	39.54		-89,284	6,183	0.13407	24.28
								114,123								
P	A	00542	177,555	903	0.13407	NS	00543	167,340	1,428	0.13407	81.88	00544	107,430	1,943	0.13407	64.19
	P		40,423	5,417	0.13407	24.63		56,413	6,866	0.13407	19.13		30,798	13,756	0.13407	9.79
S	A		42,485	7,741	0.13407	17.20		28,267	8,237	0.13407	16.39		3,575	7,508	0.13407	18.40
	P		-21,278	12,745	0.13407	11.09		-33,671	34,388	0.13407	4.16		-24,623	48,213	0.13407	2.94
P	A	00545	76,623	1,315	0.13407	97.89	00546	69,779	1,508	0.13407	85.95	00547	39,629	1,090	0.13407	NS
	P		-13,224	15,724	0.13407	8.93		-29,970	18,743	0.13407	7.60		-25,435	25,872	0.13407	5.49
S	A		11,923	6,093	0.13407	22.50		6,102	5,540	0.13407	24.88		3,102	4,615	0.13407	29.96
	P		-72,183	73,670	0.13407	2.01		-71,137	91,860	0.13407	1.61		-81,131	109,547	0.13407	1.36
P	A	00548	27,500	1,295	0.13407	NS	00891	0	0	0.13407	-	00892	0	0	0.13407	-
	P		-77,347	24,691	0.13407	6.02		42,749	17,302	0.13407	7.69		-45,492	134,315	0.26813	2.05
S	A		-108	4,228	0.13407	32.80		81,884	5,566	0.13407	22.18		-35,384	515	0.13407	NS
	P		-	123,076	0.13407	1.23		87,011	7,669	0.13407	16.01		46,702	36,311	0.13407	3.53
			103,078													
P	A	00894	0	0	0.13407	-	00896	0	0	0.13407	-	00898	0	0	0.13407	-
	P		166,417	142,536	0.26813	1.77		66,737	178,137	0.26813	1.48		70,536	179,443	0.26813	1.47
S	A		0	0	0.13407	-		-6,632	379	0.13407	NS		0	0	0.13407	-
	P		47,258	29,865	0.13407	4.26		-11,010	36,558	0.13407	3.74		-34,298	36,375	0.13407	3.93
P	A	00901	0	0	0.13407	-	00902	0	0	0.13407	-	00904	0	0	0.13407	-
	P		-10,662	162,164	0.26813	1.68		137,991	162,818	0.26813	1.57		34,166	67,420	0.13407	1.99
S	A		14,106	826	0.13407	NS		0	0	0.13407	-		0	0	0.13407	-
	P		-62,404	33,258	0.13407	4.27		-46,744	34,376	0.13407	4.10		6,293	14,240	0.13407	9.38
P	A	00906	0	0	0.13407	-	00909	0	0	0.13407	-	00910	0	0	0.13407	-
	P		-712	43,408	0.13407	3.20		-63,631	112,889	0.13407	1.30		56,529	90,296	0.13407	1.45
S	A		80,658	5,936	0.13407	20.65		-40,406	886	0.13407	NS		0	0	0.13407	-
	P		16,859	6,318	0.13407	20.71		43,452	32,969	0.13407	3.89		16,259	17,822	0.13407	7.35
P	A	00912	0	0	0.13407	-	00914	-40,988	7,271	0.13407	19.80	00917	0	0	0.13407	-
	P		77,737	13,269	0.13407	9.69		193,341	7,882	0.13407	14.41		39,264	179,553	0.26813	1.49
S	A		-17,769	6,408	0.13407	21.32		120,366	4,579	0.13407	25.59		0	0	0.13407	-
	P		-10,520	7,242	0.13407	18.73		59,428	3,383	0.13407	36.98		20,043	41,527	0.13407	3.21
P	A	00918	0	0	0.13407	-	00921	0	0	0.13407	-	00922	0	0	0.13407	-
	P		99,917	179,522	0.26813	1.45		66,651	180,130	0.26813	1.47		68,029	178,248	0.26813	1.48
S	A		-9,784	99	0.13407	NS		0	0	0.13407	-		0	0	0.13407	-
	P		-5,230	36,893	0.13407	3.70		-3,083	40,596	0.13407	3.43		-4,979	39,515	0.13407	3.52
P	A	00923	0	0	0.13407	-	00924	0	0	0.13407	-	00928	0	0	0.13407	-
	P		107,132	183,947	0.26813	1.41		104,632	179,151	0.26813	1.45		70,284	175,010	0.26813	1.51
S	A		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
	P		-16,722	37,614	0.13407	3.74		12,298	36,345	0.13407	3.77		-32,463	35,660	0.13407	4.01
P	A	00930	0	0	0.13407	-	00932	0	0	0.13407	-	00935	0	0	0.13407	-
	P		51,320	147,342	0.26813	1.80		144,645	123,458	0.26813	2.07		47,811	171,556	0.26813	1.55
S	A		-35,554	<												



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D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
S	A		107,160	3,023	0.13407	40.16		123,533	3,390	0.13407	35.24		443	3,336	0.13407	41.54
	P		20,212	1,010	0.13407	NS		-39,121	4,091	0.13407	34.35		-	100,732	0.13407	1.52
													114,973			
P	A	01953	23,495	370	0.13407	NS	01954	46,305	192	0.13407	NS	01955	0	0	0.13407	-
	P		-31,972	1,567	0.13407	91.11		-14,468	3,105	0.13407	45.25		6,727	5,486	0.13407	25.11
S	A		491	2,595	0.13407	53.40		4,185	2,991	0.13407	46.17		13,284	2,848	0.13407	48.08
	P		-99,243	59,079	0.13407	2.56		-73,470	47,237	0.13407	3.14		-51,908	32,334	0.13407	4.50
P	A	01956	0	0	0.13407	-	01957	0	0	0.13407	-	01958	-5,160	15,260	0.13407	9.13
	P		20,806	7,278	0.13407	18.68		26,206	10,253	0.13407	13.19		17,735	302	0.13407	NS
S	A		24,989	1,679	0.13407	80.65		69,341	1,025	0.13407	NS		4,149	984	0.13407	NS
	P		-25,662	17,665	0.13407	8.04		-3,858	4,972	0.13407	27.99		-85,282	13,372	0.13407	11.19
P	A	01959	4,536	5,221	0.13407	26.44	01960	0	0	0.13407	-	01961	0	0	0.13407	-
	P		30,052	926	0.13407	NS		11,559	7,527	0.13407	18.22		24,807	23,449	0.13407	5.78
S	A		10,043	545	0.13407	NS		-2,321	396	0.13407	NS		23,757	678	0.13407	NS
	P		-58,244	11,747	0.13407	12.44		-29,376	9,183	0.13407	15.51		-20,255	6,873	0.13407	20.55
P	A	01962	11,654	36,605	0.13407	3.75	01963	16,393	23,474	0.13407	5.82	01964	2,923	4,276	0.13407	32.34
	P		800	761	0.13407	NS		7,216	1,530	0.13407	90.01		10,660	2,888	0.13407	47.53
S	A		-87,582	14,288	0.13407	10.49		-67,967	9,561	0.13407	15.42		-46,878	3,964	0.13407	36.50
	P		4,734	82	0.13407	NS		8,199	552	0.13407	NS		12,847	1,265	0.13407	NS
P	A	01965	0	0	0.13407	-	01966	0	0	0.13407	-	01967	26,667	46,274	0.13407	2.92
	P		34,392	20,607	0.13407	6.51		34,540	50,902	0.13407	2.64		-8,034	1,883	0.13407	74.18
S	A		1,200	944	0.13407	NS		0	0	0.13407	-		-72,741	28,021	0.13407	5.28
	P		-20,936	3,245	0.13407	43.56		-7,948	9,308	0.13407	15.01		5,777	1,123	0.13407	NS
P	A	01968	32,807	21,549	0.13407	6.24	01969	0	0	0.13407	-	01970	0	0	0.13407	-
	P		-3,373	3,162	0.13407	43.98		22,842	11,242	0.13407	12.07		52,685	47,993	0.13407	2.75
S	A		-52,496	17,784	0.13407	8.18		-31,016	6,327	0.13407	22.55		3,985	375	0.13407	NS
	P		8,067	1,602	0.13407	85.89		5,217	2,075	0.13407	66.49		-7,136	5,076	0.13407	27.50
P	A	01971	34,140	68,984	0.13407	1.95	01972	40,024	44,069	0.13407	3.03	01973	27,342	10,120	0.13407	13.35
	P		-18,445	2,065	0.13407	68.29		-13,736	3,276	0.13407	42.86		-9,036	4,999	0.13407	27.97
S	A		-71,408	40,143	0.13407	3.68		-55,925	29,825	0.13407	4.89		-36,547	15,978	0.13407	8.97
	P		4,307	1,405	0.13407	98.28		4,676	1,760	0.13407	78.43		2,039	2,082	0.13407	66.46
P	A	01974	0	0	0.13407	-	01975	0	0	0.13407	-	01976	43,343	69,032	0.13407	1.93
	P		53,345	34,842	0.13407	3.78		76,336	88,561	0.26813	2.97		-22,734	3,246	0.13407	43.62
S	A		-13,535	577	0.13407	NS		0	0	0.13407	-		-57,298	38,857	0.13407	3.76
	P		-6,819	2,281	0.13407	61.17		-1,500	14,029	0.13407	9.90		2,385	1,789	0.13407	77.33
P	A	01977	51,604	32,567	0.13407	4.05	01978	0	0	0.13407	-	01979	0	0	0.13407	-
	P		-16,618	4,779	0.13407	29.46		36,392	15,998	0.13407	8.37		64,118	70,535	0.13407	1.85
S	A		-40,531	25,204	0.13407	5.71		-20,215	8,649	0.13407	16.33		0	0	0.13407	-
	P		-1	2,073	0.13407	66.88		-6,926	2,242	0.13407	62.24		-8,789	8,887	0.13407	15.73
P	A	01980	44,238	91,223	0.13407	1.46	01981	53,959	57,958	0.13407	2.27	01982	62,778	11,869	0.13407	11.00
	P		-29,389	3,134	0.13407	45.45		-23,742	4,529	0.13407	31.29		-16,950	6,265	0.13407	22.48
S	A		-54,301	43,688	0.13407	3.33		-42,930	32,643	0.13407	4.42		-25,994	16,701	0.13407	8.50
	P		1,126	1,785	0.13407	77.59		-1,259	2,020	0.13407	68.72		-6,423	2,181	0.13407	63.95
P	A	01983	0	0	0.13407	-	01984	0	0	0.13407	-	01985	52,182	83,411	0.13407	1.58
	P		69,718	46,299	0.13407	2.80		55,063	117,024	0.26813	2.27		-30,711	4,193	0.13407	34.01
S	A		0	0	0.13407	-		0	0	0.13407	-		-44,292	37,844	0.13407	3.81
	P		-14,842	2,724	0.13407	51.60		9,468	18,728	0.13407	7.34		-1,777	1,950	0.13407	71.22
P	A	01986	64,063	39,178	0.13407	3.33	01987	0	0	0.13407	-	01988	0	0	0.13407	-
	P		-23,627	5,792	0.13407	24.46		71,023	17,944	0.13407	7.21		85,588	85,900	0.13407	1.48
S	A		-30,148	24,014	0.13407	5.94		-12,507	6,532	0.13407	21.47		0	0	0.13407	-
	P		-5,874	2,123	0.13407	65.66		-12,798	2,193	0.13407	63.98		-3,274	11,467	0.13407	12.13
P	A	01989	49,186	104,275	0.13407	1.27	01990	62,487	66,078	0.13407	1.98	01991	74,047	13,067	0.13407	9.88
	P		-35,638	3,843	0.13407	37.27		-29,764	5,305	0.13407	26.86		-22,685	7,004	0.13407	20.21
S	A		-42,108	40,473	0.13407	3.56		-33,314	30,042	0.13407	4.76		-18,088	14,243	0.13407	9.90
	P		-1,872	1,828	0.13407	75.98		-5,117	2,038	0.13407	68.35		-10,889	2,168	0.13407	64.60
P	A	01992	0	0	0.13407	-	01993	0	0	0.13407	-	01994	57,233	91,198	0.13407	1.44
	P		81,742	53,406	0.13407	2.40		65,135	134,202	0.26813	1.97		-35,563	4,744	0.13407	30.19
S	A		0	0	0.13407	-		0	0	0.13407	-		-36,102	34,513	0.13407	4.15
	P		-10,283	5,420	0.13407	25.83		14,670	21,627	0.13407	6.32		-4,188	1,947	0.13407	71.49
P	A	01995	72,160	42,600	0.13407	3.04	01996	0	0	0.13407	-	01997	0	0	0.13407	-
	P		-28,835	6,355	0.13407	22.40		80,360	20,180	0.13407	6.35		92,344	95,213	0.13407	1.33
S	A		-23,552	21,362	0.13407	6.63		-6,542	4,548	0.13407	30.67		0	0	0.13407	-
	P		-8,690	2,119	0.13407	65.96		-15,747	2,215	0.13407	63.51		-1,055	11,827	0.13407	11.73
P	A	01998	51,747	110,427	0.13407	1.19	01999	67,576	69,906	0.13407	1.86	02000	82,037	13,490	0.13407	9.49
	P		-39,012	4,207	0.13407	34.15		-33,638	5,688	0.13407	25.14		-27,793	7,371	0.13407	19.30
S	A		-35,662	37,375	0.13407	3.83		-28,285	27,534	0.13407	5.17		-14,219	12,366	0.13407	11.36
	P		-3,398	1,804	0.13407	77.10		-6,819	2,027	0.13407	68.83		-12,408	2,188	0.13407	64.10
P	A	02001	0	0	0.13407	-	02002	0	0	0.13407	-	02003	59,313	94,180	0.13407	1.39
	P		93,032	56,851	0.13407	2.23		72,533	140,632	0.26813	1.87		-37,518	4,962	0.13407	28.92
S	A		0	0	0.13407	-		0	0	0.13407	-		-32,708	32,661	0.13407	4.37
	P		-7,494	6,700	0.13407	20.84		25,457	22,901	0.13407	5.91		-5,208	1,920	0.13407	72.56
P	A	02004	76,060	43,823	0.13407	2.94	02005	0	0	0.13407	-	02006	0	0	0.13407	-
	P		-31,314	6,564	0.13407	21.74		86,318	21,108	0.13407	6.04		102,000	98,044	0.13407	1.28
S	A		-20,929	19,896	0.13407	7.10		-4,469	3,545	0.13407	39.27		0	0	0.13407	-
	P		-9,659	2,112	0.13407	66.24		-16,556	2,253	0.13407	62.49		17,355	14,211	0.13407	9.60
P	A	02007	51,768	111,394	0.13407	1.18	02008	67,883	70,576	0.13407	1.84	02009	82,276	13,480	0.13407	9.49
	P		-39,131	4,271	0.13407	33.64		-33,637	5,751	0.13407	24.86		-27,330	7,411	0.13407	19.18
S	A		-34,420	36,766	0.13407	3.89		-27,164	26,903	0.13407	5.28		-13,276	11,855	0.13407	11.84
	P		-3,814	1,780	0.13407	78.17		-7,357	1,994	0.13407	70.01		-12,998	2,150	0.13407	65.27
P	A	02010	0													



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D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	P		92,291	57,665	0.13407	2.20		69,559	141,448	0.26813	1.87		-36,018	4,887	0.13407	29.32
S	A		0	0	0.13407	-		0	0	0.13407	-		-33,617	33,378	0.13407	4.28
	P		-7,433	6,974	0.13407	20.02		18,713	23,068	0.13407	5.91		-5,153	1,891	0.13407	73.67
P	A	02013	73,365	43,392	0.13407	2.98	02014	0	0	0.13407	-	02015	0	0	0.13407	-
	P		-28,975	6,471	0.13407	22.00		82,158	20,912	0.13407	6.12		94,987	96,574	0.13407	1.31
S	A		-21,613	20,234	0.13407	6.99		-5,378	3,543	0.13407	39.33		0	0	0.13407	-
	P		-9,719	2,054	0.13407	68.11		-16,594	2,147	0.13407	65.57		-1,612	13,887	0.13407	10.00
P	A	02016	49,877	107,259	0.13407	1.23	02017	64,160	68,422	0.13407	1.90	02018	76,890	13,227	0.13407	9.73
	P		-36,402	4,047	0.13407	35.42		-30,603	5,506	0.13407	25.90		-23,420	7,156	0.13407	19.80
S	A		-38,431	39,153	0.13407	3.67		-30,162	28,460	0.13407	5.01		-15,936	12,888	0.13407	10.92
	P		-2,972	1,783	0.13407	77.97		-6,510	1,973	0.13407	70.70		-12,161	2,081	0.13407	67.38
P	A	02019	0	0	0.13407	-	02020	0	0	0.13407	-	02021	54,978	87,211	0.13407	1.51
	P		86,759	55,831	0.13407	2.28		77,224	138,950	0.26813	1.89		-31,859	4,513	0.13407	31.63
S	A		0	0	0.13407	-		0	0	0.13407	-		-39,048	36,250	0.13407	3.96
	P		-10,350	6,442	0.13407	21.73		18,423	22,043	0.13407	6.18		-3,297	1,867	0.13407	74.49
P	A	02022	67,259	41,091	0.13407	3.16	02023	0	0	0.13407	-	02024	0	0	0.13407	-
	P		-25,017	6,062	0.13407	23.40		75,211	19,441	0.13407	6.63		88,898	92,326	0.13407	1.38
S	A		-26,651	22,478	0.13407	6.32		-9,939	5,254	0.13407	26.63		0	0	0.13407	-
	P		-7,700	2,040	0.13407	68.45		-14,431	2,107	0.13407	66.69		-3,657	11,285	0.13407	12.33
P	A	02025	45,700	98,967	0.13407	1.34	02026	57,522	62,655	0.13407	2.09	02027	67,897	12,465	0.13407	10.42
	P		-31,808	3,581	0.13407	39.86		-25,946	4,922	0.13407	28.85		-18,878	6,599	0.13407	21.38
S	A		-46,471	42,037	0.13407	3.44		-37,742	31,174	0.13407	4.60		-22,476	15,336	0.13407	9.23
	P		-888	1,757	0.13407	78.97		-3,490	1,985	0.13407	70.07		-8,787	2,114	0.13407	66.12
P	A	02028	0	0	0.13407	-	02029	0	0	0.13407	-	02030	47,118	76,626	0.13407	1.73
	P		76,263	50,542	0.13407	2.55		56,120	128,080	0.26813	2.07		-26,603	3,728	0.13407	38.11
S	A		0	0	0.13407	-		0	0	0.13407	-		-50,407	38,799	0.13407	3.74
	P		-13,745	4,447	0.13407	31.58		13,503	20,530	0.13407	6.67		111	1,849	0.13407	74.98
P	A	02031	57,178	36,214	0.13407	3.62	02032	0	0	0.13407	-	02033	0	0	0.13407	-
	P		-19,494	5,285	0.13407	26.71		63,241	16,513	0.13407	7.90		67,580	80,898	0.13407	1.61
S	A		-35,393	24,975	0.13407	5.73		-17,524	7,729	0.13407	18.23		0	0	0.13407	-
	P		-3,185	2,081	0.13407	66.82		-9,721	2,184	0.13407	64.06		-9,911	9,732	0.13407	14.38
P	A	02034	38,636	82,406	0.13407	1.62	02035	46,614	51,844	0.13407	2.56	02036	53,854	10,647	0.13407	12.37
	P		-24,391	2,674	0.13407	53.03		-18,682	3,924	0.13407	35.95		-12,533	5,641	0.13407	24.86
S	A		-61,013	42,337	0.13407	3.46		-49,135	32,171	0.13407	4.51		-31,363	16,985	0.13407	8.40
	P		2,592	1,588	0.13407	87.10		1,669	1,916	0.13407	72.25		-2,625	2,154	0.13407	64.52
P	A	02037	0	0	0.13407	-	02038	0	0	0.13407	-	02039	35,402	58,444	0.13407	2.29
	P		59,500	41,221	0.13407	3.18		28,768	106,499	0.26813	2.52		-16,269	2,578	0.13407	54.59
S	A		-21,556	21	0.13407	NS		0	0	0.13407	-		-65,134	35,246	0.13407	4.17
	P		-11,679	2,269	0.13407	61.77		1,352	18,687	0.13407	7.41		4,409	1,535	0.13407	89.95
P	A	02040	42,014	27,581	0.13407	4.83	02041	0	0	0.13407	-	02042	0	0	0.13407	-
	P		-10,587	4,009	0.13407	34.92		28,430	13,787	0.13407	9.79		53,841	60,416	0.13407	2.18
S	A		-46,730	23,132	0.13407	6.25		-26,079	8,288	0.13407	17.13		0	0	0.13407	-
	P		4,072	1,897	0.13407	72.81		-1,566	2,206	0.13407	62.94		-11,963	7,545	0.13407	18.58
P	A	02043	24,594	55,476	0.13407	2.44	02044	29,106	34,608	0.13407	3.90	02045	15,745	7,516	0.13407	18.18
	P		-10,667	1,463	0.13407	95.71		-4,722	2,423	0.13407	57.47		-1,448	4,023	0.13407	34.51
S	A		-79,205	30,567	0.13407	4.87		-62,390	22,768	0.13407	6.44		-42,434	12,111	0.13407	11.90
	P		4,934	905	0.13407	NS		7,281	1,339	0.13407	NS		7,895	1,840	0.13407	74.80
P	A	02046	0	0	0.13407	-	02047	0	0	0.13407	-	02048	13,307	31,955	0.13407	4.28
	P		43,227	28,062	0.13407	4.74		70,573	70,017	0.13407	1.85		3,249	1,094	0.13407	NS
S	A		-5,600	867	0.13407	NS		0	0	0.13407	-		-79,883	12,030	0.13407	12.38
	P		582	2,247	0.13407	61.67		-5,723	10,946	0.13407	12.73		5,769	271	0.13407	NS
P	A	02049	19,718	14,086	0.13407	9.66	02050	0	0	0.13407	-	02051	0	0	0.13407	-
	P		9,888	2,070	0.13407	66.36		16,762	9,261	0.13407	14.74		47,779	34,564	0.13407	3.83
S	A		-57,332	6,880	0.13407	21.23		-4,699	1,521	0.13407	91.55		17,634	819	0.13407	NS
	P		10,698	876	0.13407	NS		13,435	1,653	0.13407	82.82		-9,554	4,762	0.13407	29.37
P	A	02052	-6,253	19,297	0.13407	7.23	02053	62	10,733	0.13407	12.92	02054	22,226	782	0.13407	NS
	P		11,364	164	0.13407	NS		24,706	566	0.13407	NS		33,832	1,453	0.13407	92.41
S	A		3,599	1,059	0.13407	NS		6,810	830	0.13407	NS		-10,206	183	0.13407	NS
	P		-95,405	14,450	0.13407	10.45		-71,928	12,760	0.13407	11.59		-41,727	10,424	0.13407	13.82
P	A	02055	0	0	0.13407	-	02056	0	0	0.13407	-	02057	31,279	345	0.13407	NS
	P		17,612	14,853	0.13407	9.18		39,762	29,176	0.13407	4.58		-28,731	1,574	0.13407	90.44
S	A		6,157	543	0.13407	NS		44,211	691	0.13407	NS		1,743	2,733	0.13407	50.65
	P		-18,704	8,205	0.13407	17.19		-7,886	6,325	0.13407	21.69		-85,875	53,032		



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
P	A	00386	-36,017	8,659	0.13407	16.55	00387	-33,559	7,604	0.13407	18.80	00388	-38,410	10,726	0.13407	13.39
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A	00389	-4,171	8,482	0.13407	16.41	00390	1,996	10,007	0.13407	13.83	00391	9,025	11,804	0.13407	11.65
	P		-5,536	10,837	0.13407	12.86		-4,855	8,470	0.13407	16.44		-5,237	3,903	0.13407	35.70
P	A	00392	-35,033	12,930	0.13407	11.07	00393	-34,034	13,097	0.13407	10.92	00394	-33,755	13,913	0.13407	10.28
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A	00395	19,844	12,118	0.13407	11.23	00396	16,262	10,509	0.13407	12.99	00397	6,081	13,847	0.13407	9.96
	P		6,903	1,534	0.13407	89.80		0	0	0.13407	-		0	0	0.13407	-
P	A	00398	-34,684	14,411	0.13407	9.93	00399	-38,190	17,265	0.13407	8.32	00400	-32,731	16,325	0.13407	8.75
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A	00401	15,419	18,181	0.13407	7.52	00402	4,734	21,196	0.13407	6.51	00403	8,166	24,128	0.13407	5.70
	P		0	0	0.13407	-		0	0	0.13407	-		24,745	1,403	0.13407	96.54
P	A	00404	-34,521	15,749	0.13407	9.09	00405	-40,317	17,466	0.13407	8.24	00406	-32,966	17,143	0.13407	8.34
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A	00407	13,123	26,161	0.13407	5.23	00408	4,094	26,848	0.13407	5.14	00409	8,501	25,985	0.13407	5.29
	P		29,946	2,394	0.13407	56.29		21,876	2,124	0.13407	63.94		27,600	1,646	0.13407	82.06
P	A	00410	-33,476	16,460	0.13407	8.69	00411	-40,451	17,032	0.13407	8.45	00412	-33,096	16,808	0.13407	8.50
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A	00413	9,777	26,343	0.13407	5.22	00414	4,249	25,528	0.13407	5.41	00415	8,462	22,858	0.13407	6.02
	P		31,555	1,917	0.13407	70.19		26,309	1,311	0.13407	NS		26,783	446	0.13407	NS
P	A	00416	-32,013	16,753	0.13407	8.52	00417	-45,040	15,849	0.13407	9.11	00418	-31,210	13,017	0.13407	10.96
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A	00419	10,779	20,943	0.13407	6.55	00420	6,541	17,553	0.13407	7.85	00421	10,332	13,006	0.13407	10.56
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	00422	-34,291	12,308	0.13407	11.62	00423	-42,644	12,481	0.13407	11.55	00424	-33,516	10,188	0.13407	14.03
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A	00425	22,331	10,231	0.13407	13.27	00426	18,361	12,526	0.13407	10.88	00427	21,890	11,720	0.13407	11.59
	P		0	0	0.13407	-		6,808	1,813	0.13407	75.99		12,328	5,207	0.13407	26.32
P	A	00428	-33,947	8,390	0.13407	17.05	00429	-40,928	7,368	0.13407	19.53	00430	-33,011	5,018	0.13407	28.48
	P		0	0	0.13407	-		0	0	0.13407	-		-28,687	2,031	0.13407	70.09
S	A	00431	16,952	10,275	0.13407	13.28	00432	9,110	8,352	0.13407	16.46	00433	10,383	5,296	0.13407	25.93
	P		8,862	7,270	0.13407	18.91		7,045	10,784	0.13407	12.77		12,150	13,359	0.13407	10.26
P	A	00434	-30,729	3,502	0.13407	40.72	00435	-75,404	2,195	0.13407	67.59	00436	-23,061	750	0.13407	NS
	P		-28,108	1,629	0.13407	87.34		-32,360	915	0.13407	NS		-21,974	3,278	0.13407	43.16
S	A	00437	9,748	2,208	0.13407	62.22	00438	-37,557	379	0.13407	NS	00439	0	0	0.13407	-
	P		12,785	13,271	0.13407	10.32		10,833	14,709	0.13407	9.33		12,827	15,571	0.13407	8.80
P	A	00440	-40,152	71	0.13407	NS	00441	0	0	0.13407	-	00442	29,629	8,584	0.13407	15.70
	P		-22,245	2,715	0.13407	52.12		-28,522	3,966	0.13407	35.89		0	0	0.13407	-
S	A	00443	-13,921	39	0.13407	NS	00444	0	0	0.13407	-	00445	36,150	34,366	0.13407	3.82
	P		17,834	14,104	0.13407	9.67		52,829	15,426	0.13407	8.54		-24,251	1,485	0.13407	93.65
P	A	00446	2,450	6,521	0.13407	21.21	00447	-5,551	4,229	0.13407	32.95	00448	-36,372	1,512	0.13407	94.80
	P		0	0	0.13407	-		-7,459	907	0.13407	NS		-9,380	1,848	0.13407	75.68
S	A	00449	-10,202	23,307	0.13407	6.01	00450	-28,923	13,430	0.13407	10.60	00451	-30,399	6,858	0.13407	20.79
	P		-7,444	2,611	0.13407	53.47		-756	3,610	0.13407	38.43		3,336	4,177	0.13407	33.09
P	A	00452	-53,583	793	0.13407	NS	00453	-66,535	831	0.13407	NS	00454	-74,627	890	0.13407	NS
	P		-13,521	2,466	0.13407	56.93		-23,311	4,275	0.13407	33.14		-24,988	7,015	0.13407	20.22
S	A	00455	-33,311	1,479	0.13407	96.65	00456	9,140	79	0.13407	NS	00457	9,301	241	0.13407	NS
	P		602	4,518	0.13407	30.67		2,861	4,048	0.13407	34.16		-32,800	5,309	0.13407	26.91
P	A	00458	-83,712	1,050	0.13407	NS	00459	-89,937	1,151	0.13407	NS	00460	-99,275	1,276	0.13407	NS
	P		-30,006	8,857	0.13407	16.09		-33,418	11,150	0.13407	12.82		-34,972	13,388	0.13407	10.69
S	A	00461	9,918	422	0.13407	NS	00462	5,692	541	0.13407	NS	00463	4,281	689	0.13407	NS
	P		-32,509	7,258	0.13407	19.68		-30,726	7,754	0.13407	18.39		-30,325	8,795	0.13407	16.21
P	A	00464	-	1,386	0.13407	NS	00465	-	1,520	0.13407	NS	00466	-	1,622	0.13407	93.89
	P		102,542	-37,513	0.13407	10.22		104,661	-39,831	0.13407	9.23		105,978	-41,374	0.13407	8.27
S	A	00467	3,631	800	0.13407	NS	00468	5,967	1,514	0.13407	91.06	00469	5,514	2,418	0.13407	57.04
	P		-29,021	9,413	0.13407	15.13		-27,134	8,895	0.13407	15.98		-26,755	9,038	0.13407	15.72
P	A	00470	-	1,678	0.13407	90.87	00471	-	1,766	0.13407	86.38	00472	-	1,828	0.13407	83.49
	P		107,361	-42,138	0.13407	8.36		107,967	-43,241	0.13407	8.07		108,469	-44,528	0.13407	7.43
S	A	00473	5,815	2,993	0.13407	46.07	00474	6,023	4,120	0.13407	33.46	00475	5,494	4,673	0.13407	29.52
	P		-26,268	9,250	0.13407	15.36		-24,970	8,779	0.13407	16.16		-24,779	8,667	0.13407	16.37
P	A	00476	-	1,844	0.13407	82.79	00477	-	1,866	0.13407	81.80	00478	-	1,877	0.13407	81.33
	P		108,875	-44,265	0.13407	7.70		108,632	-44,297	0.13407	7.81		108,715	-44,745	0.13407	7.29
S	A	00479	5,715	4,802	0.13407	28.72	00480	6,162	5,009	0.13407	27.52	00481	5,539	4,882	0.13407	28.25
	P		-24,812	8,764	0.13407	16.19		-24,302	8,679	0.13407	16.34		-24,481	8,649	0.13407	16.40
P	A	00482	-	1,850	0.13407	82.49	00483	-	1,800	0.13407	84.70	00484	-	1,761	0.13407	86.55
	P		108,445	-43,899	0.13407	7.71		107,320	-42,836	0.13407	8.19		106,830	-41,960	0.13407	7.71
S	A	00485	4,956	4,598	0.13407	30.01	00486	5,684	3,919	0.13407	35.19	00487	5,075	3,105	0.13407	44.44
	P		-24,850	8,646	0.13407	16.41		-25,162	8,908	0.13407	15.93		-26,002	9,095	0.13407	15.61
P	A	00488	-	1,648	0.13407	92.42	00489	-	1,568	0.13407	96.87	00490	-	1,448	0.13407	NS
	P		106,015	-39,797	0.13407	8.82		102,797	-36,997	0.13407	8.71		101,913	-34,447	0.13407	10.27
S	A	00491	5,661	2,485	0.13407	55.50	00492	5,113	971	0.13407	NS	00493	2,712	858	0.13407	NS
	P		-26,856	8,7,												



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D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	P		-31,899	9,039	0.13407	15.79		-32,565	7,507	0.13407	19.03		-32,528	6,739	0.13407	21.20
P	A	00502	-72,136	864	0.13407	NS	00503	-61,093	687	0.13407	NS	00504	-49,585	633	0.13407	NS
	P		-21,613	6,560	0.13407	21.56		-16,994	4,030	0.13407	34.95		-8,315	2,725	0.13407	51.27
S	A		8,496	452	0.13407	NS		8,259	193	0.13407	NS		-35,381	1,448	0.13407	98.90
	P		-37,928	5,328	0.13407	26.94		617	3,981	0.13407	34.81		946	4,254	0.13407	32.56
P	A	00505	-34,206	1,151	0.13407	NS	00506	-2,692	3,830	0.13407	36.29	00507	4,548	7,317	0.13407	18.87
	P		-5,224	1,725	0.13407	80.76		-3,890	1,215	0.13407	NS		0	0	0.13407	-
S	A		-38,775	7,264	0.13407	19.78		-31,932	14,054	0.13407	10.16		-30,572	21,870	0.13407	6.52
	P		-5,346	4,176	0.13407	33.37		-7,096	3,620	0.13407	38.55		-7,695	2,815	0.13407	49.60
P	A	00508	28,969	7,678	0.13407	17.57	00509	17,540	6,296	0.13407	21.66	00510	-5,014	5,743	0.13407	24.25
	P		0	0	0.13407	-		26,298	457	0.13407	NS		11,843	907	0.13407	NS
S	A		15,893	33,932	0.13407	3.95		-60,889	29,756	0.13407	4.83		-89,869	26,324	0.13407	5.7
	P		-43,526	1,871	0.13407	75.66		-15,241	2,891	0.13407	47.70		-16,257	4,443	0.13407	31.68
P	A	00511	-18,570	4,069	0.13407	34.66	00512	-2,927	3,368	0.13407	41.28	00513	-393	2,052	0.13407	67.59
	P		4,864	989	0.13407	NS		8,029	1,395	0.13407	98.64		4,652	1,798	0.13407	76.78
S	A		-87,606	20,059	0.13407	7.47		-82,949	14,811	0.13407	10.08		-47,712	11,974	0.13407	12.09
	P		-11,743	5,521	0.13407	25.39		-11,723	7,764	0.13407	18.05		-3,283	8,924	0.13407	15.58
P	A	00514	6,715	1,572	0.13407	87.64	00515	52,793	896	0.13407	NS	00516	80,887	366	0.13407	NS
	P		-2,290	1,638	0.13407	84.82		13,489	2,736	0.13407	50.04		21,266	3,578	0.13407	37.98
S	A		-38,196	5,894	0.13407	24.36		10,099	4,641	0.13407	28.91		118,322	1,880	0.13407	63.39
	P		-5,347	10,608	0.13407	13.13		12,306	12,902	0.13407	10.38		54,554	15,755	0.13407	8.09
P	A	00517	67,001	1,407	0.13407	92.37	00518	17,503	1,616	0.13407	84.39	00519	33,995	1,953	0.13407	68.74
	P		10,744	2,306	0.13407	59.52		3,653	2,075	0.13407	66.59		8,512	1,629	0.13407	84.43
S	A		33,845	4,023	0.13407	32.53		240	5,554	0.13407	24.51		-27,138	7,135	0.13407	19.53
	P		1,746	13,685	0.13407	9.87		-866	11,547	0.13407	11.80		-3,138	8,744	0.13407	15.58
P	A	00520	10,160	2,956	0.13407	46.46	00521	-1,091	3,167	0.13407	43.82	00522	-11,262	4,560	0.13407	30.72
	P		7,741	1,336	0.13407	NS		7,774	1,288	0.13407	NS		11,348	882	0.13407	NS
S	A		-60,732	10,699	0.13407	13.69		-69,363	16,093	0.13407	9.17		-82,726	19,043	0.13407	7.84
	P		-12,919	9,087	0.13407	15.44		-8,364	6,956	0.13407	20.09		-11,166	5,050	0.13407	27.74
P	A	00523	7,312	5,818	0.13407	23.67	00524	43,269	5,256	0.13407	25.31	01806	18,567	4,846	0.13407	28.11
	P		15,321	685	0.13407	NS		34,149	292	0.13407	NS		0	0	0.13407	-
S	A		-73,802	26,780	0.13407	5.53		-22,031	31,139	0.13407	4.45		-3,026	32,875	0.13407	4.14
	P		-11,839	3,824	0.13407	36.66		-6,183	1,808	0.13407	75.59		-13,047	2,337	0.13407	58.75
P	A	01807	0	0	0.13407	-	01808	-5,272	876	0.13407	NS	01809	78,798	2,808	0.13407	45.74
	P		-15,307	2,601	0.13407	54.06		-657	1,437	0.13407	96.54		0	0	0.13407	-
S	A		53,630	1,129	0.13407	NS		32,689	3,554	0.13407	37.82		26,635	34,541	0.13407	3.83
	P		92,960	14,252	0.13407	8.88		4,172	15,308	0.13407	9.02		-5,997	1,491	0.13407	91.50
P	A	01810	8,929	3,984	0.13407	34.51	01811	11,789	3,104	0.13407	44.17	01812	3,218	2,029	0.13407	68.13
	P		14,909	181	0.13407	NS		9,274	284	0.13407	NS		-4,679	612	0.13407	NS
S	A		-34,805	24,849	0.13407	5.65		-75,220	16,679	0.13407	8.74		-60,415	10,432	0.13407	13.74
	P		-11,456	3,069	0.13407	44.75		-9,307	5,437	0.13407	25.23		-6,934	7,964	0.13407	17.14
P	A	01813	-12,653	663	0.13407	NS	01814	-22,008	32	0.13407	NS	01815	-6,623	2,782	0.13407	50.14
	P		-9,355	1,416	0.13407	98.77		-11,039	1,801	0.13407	77.77		-7,389	670	0.13407	NS
S	A		-29,892	5,737	0.13407	24.29		2,496	2,263	0.13407	61.12		-42,797	13,000	0.13407	11.09
	P		-1,805	10,078	0.13407	13.47		4,334	11,729	0.13407	11.77		-4,189	4,822	0.13407	28.86
P	A	01816	-1,432	2,057	0.13407	67.49	01817	-13,593	1,340	0.13407	NS	01818	-27,249	955	0.13407	NS
	P		-12,453	693	0.13407	NS		-19,694	1,112	0.13407	NS		-28,275	1,888	0.13407	75.37
S	A		-55,379	9,130	0.13407	15.97		-43,796	5,174	0.13407	27.89		-34,785	696	0.13407	NS
	P		-4,648	6,931	0.13407	20.09		-2,245	9,482	0.13407	14.65		-4,688	13,082	0.13407	10.64
P	A	01819	-40,277	1,225	0.13407	NS	01820	-41,347	1,538	0.13407	93.62	01821	-17,564	1,678	0.13407	83.98
	P		-10,963	1,568	0.13407	89.32		-15,586	1,301	0.13407	NS		-21,413	1,350	0.13407	NS
S	A		-33,967	5,867	0.13407	24.38		-42,795	5,316	0.13407	27.12		-44,024	3,701	0.13407	39.00
	P		-472	4,711	0.13407	29.44		-725	6,045	0.13407	22.95		-681	8,021	0.13407	17.30
P	A	01822	-25,667	2,224	0.13407	63.83	01823	-30,066	1,369	0.13407	NS	01824	-64,217	792	0.13407	NS
	P		-28,544	1,713	0.13407	83.09		-31,895	3,256	0.13407	43.85		-16,443	2,256	0.13407	62.40
S	A		-40,979	1,560	0.13407	92.27		0	0	0.13407	-		-40,465	249	0.13407	NS
	P		-2,527	10,725	0.13407	12.96		-15,320	13,941	0.13407	10.09		2,045	4,794	0.13407	28.87
P	A	01825	-19,833	1,647	0.13407	85.74	01826	-25,287	3,033	0.13407	46.79	01827	-32,512	4,008	0.13407	35.64
	P		-21,262	1,899	0.13407	74.46		-27,587	1,863	0.13407	76.33		-33,010	2,166	0.13407	65.98
S	A		-39,183	907	0.13407	NS		229	650	0.13407	NS		-5,430	2,048	0.13407	68.04
	P		1,342	6,106	0.13407	22.68		-450	7,979	0.13407	17.38		-5,599	10,431	0.13407	13.36
P	A	01828	-77,424	925	0.13407	NS	01829	-21,338	811	0.13407	NS	01830	-25,022	2,882	0.13407	49.23
	P		-27,225	4,561	0.13407	31.17		-20,281	2,631	0.13407	53.69		-24,409	2,164	0.13407	65.53
S	A		8,678	179	0.13407	NS		4,720	376	0.13407	NS		3,770	1,837	0.13407	75.21
	P		-32,791	4,190	0.13407	34.10		2,970	4,068	0.13407	33.99		1,522	4,989	0.13407	27.75
P	A	01831	-29,668	4,819	0.13407	29.57	01832	-31,299	6,838	0.13407	20.87	01833	-88,910	1,118	0.13407	NS
	P		-28,839	1,737	0.13407	81.96		-29,873	1,262	0.13407	NS		-32,403	5,132	0.13407	27.83
S	A		1,348	3,871	0.13407	35.77		-2,901	6,845	0.13407	20.31		4,298	419	0.13407	NS
	P		-1,665	6,506	0.13407	21.34		-6,904	8,845	0.13407	15.78		-32,875	5,310	0.13407	26.91
P	A	01834	-25,513	1,866	0.13407	76.07	01835	-28,428	4,502	0.13407	31.61	01836	-33,804	7,293	0.13407	19.61
	P		-22,329	2,606	0.13407	54.31		-26,102	1,846	0.13407	76.93		-30,120			



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D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	P		-33,187	1,129	0.13407	NS		0	0	0.13407	-		-30,307	6,786	0.13407	21.01
P	A	01843	-96,726	1,698	0.13407	88.99	01844	-29,626	4,769	0.13407	29.87	01845	-34,797	8,873	0.13407	16.13
	P		-38,547	3,599	0.13407	39.91		-24,784	708	0.13407	NS		0	0	0.13407	-
S	A		6,036	4,088	0.13407	33.72		5,648	5,748	0.13407	23.99		8,597	7,296	0.13407	18.85
	P		-31,618	4,583	0.13407	31.14		-31,344	2,365	0.13407	60.33		-27,750	228	0.13407	NS
P	A	01846	-	1,615	0.13407	94.32	01847	-	1,772	0.13407	85.53	01848	-29,145	2,680	0.13407	53.14
	P		106,190	-41,158	13,194	0.13407		10.91	100,234	-38,655	6,959		0.13407	20.64	-37,750	1,841
S	A		5,875	3,521	0.13407	39.16		6,406	5,757	0.13407	23.94		6,381	8,337	0.13407	16.53
	P		-28,192	7,888	0.13407	18.04		-30,354	5,858	0.13407	24.34		-29,860	3,592	0.13407	39.67
P	A	01849	-31,272	6,690	0.13407	21.33	01850	-31,351	11,742	0.13407	12.15	01851	-	1,795	0.13407	84.68
	P		0	0	0.13407	-		0	0	0.13407	-		103,619	-41,637	10,956	0.13407
S	A		6,657	11,359	0.13407	12.13		7,543	15,057	0.13407	9.14		6,377	6,233	0.13407	22.11
	P		-28,898	1,304	0.13407	NS		0	0	0.13407	-		-28,296	6,785	0.13407	20.97
P	A	01852	-99,363	2,083	0.13407	72.71	01853	-30,282	4,454	0.13407	32.01	01854	-34,526	9,372	0.13407	15.27
	P		-39,986	4,927	0.13407	29.19		0	0	0.13407	-		0	0	0.13407	-
S	A		6,668	9,422	0.13407	14.62		6,879	13,064	0.13407	10.54		9,688	17,491	0.13407	7.85
	P		-28,718	4,707	0.13407	30.24		-28,090	2,427	0.13407	58.62		-24,350	63	0.13407	NS
P	A	01855	-	1,844	0.13407	82.76	01856	-	2,034	0.13407	74.64	01857	-29,710	2,289	0.13407	62.25
	P		108,404	-43,833	15,009	0.13407		9.61	102,236	-40,449	8,246		0.13407	17.45	-38,536	2,442
S	A		5,944	6,138	0.13407	22.46		6,762	9,313	0.13407	14.79		7,095	13,064	0.13407	10.54
	P		-26,410	7,625	0.13407	18.63		-27,822	5,731	0.13407	24.82		-27,440	3,545	0.13407	40.11
P	A	01858	-31,778	6,813	0.13407	20.95	01859	-31,624	12,385	0.13407	11.52	01860	-	1,951	0.13407	78.00
	P		0	0	0.13407	-		0	0	0.13407	-		104,993	-42,914	11,896	0.13407
S	A		7,579	17,439	0.13407	7.89		8,300	22,508	0.13407	6.11		6,582	8,093	0.13407	17.03
	P		-26,156	1,238	0.13407	NS		22,916	1,516	0.13407	89.50		-27,174	6,612	0.13407	21.50
P	A	01861	-	2,281	0.13407	66.45	01862	-31,052	4,450	0.13407	32.06	01863	-34,626	9,662	0.13407	14.81
	P		100,248	-40,624	5,491	0.13407		26.20	0	0	0.13407		-	0	0	0.13407
S	A		7,142	11,905	0.13407	11.57		7,509	16,169	0.13407	8.51		9,291	21,154	0.13407	6.50
	P		-27,072	4,616	0.13407	30.79		-26,228	2,373	0.13407	59.85		21,940	1,324	0.13407	NS
P	A	01864	-	1,908	0.13407	80.01	01865	-	2,116	0.13407	71.77	01866	-29,840	2,289	0.13407	62.25
	P		108,797	-44,076	15,303	0.13407		9.43	102,636	-40,714	8,486		0.13407	16.96	-38,739	2,548
S	A		6,069	6,570	0.13407	20.98		7,102	9,959	0.13407	13.83		7,575	13,859	0.13407	9.93
	P		-25,939	7,561	0.13407	18.78		-27,022	5,678	0.13407	25.03		-26,400	3,512	0.13407	40.45
P	A	01867	-32,346	6,989	0.13407	20.44	01868	-32,030	12,677	0.13407	11.26	01869	-	1,936	0.13407	78.58
	P		0	0	0.13407	-		0	0	0.13407	-		104,653	-42,148	11,587	0.13407
S	A		7,951	18,263	0.13407	7.54		7,718	23,073	0.13407	5.97		5,940	7,396	0.13407	18.64
	P		-24,975	1,221	0.13407	NS		25,068	1,333	0.13407	NS		-27,170	6,711	0.13407	21.18
P	A	01870	-	2,266	0.13407	66.88	01871	-31,002	4,560	0.13407	31.28	01872	-34,718	9,565	0.13407	14.96
	P		100,157	-40,305	5,280	0.13407		27.24	0	0	0.13407		-	0	0	0.13407
S	A		6,522	10,947	0.13407	12.59		6,874	14,924	0.13407	9.23		8,156	19,611	0.13407	7.02
	P		-26,891	4,643	0.13407	30.61		-25,805	2,390	0.13407	59.40		23,181	452	0.13407	NS
P	A	01873	-	1,790	0.13407	85.19	01874	-	2,006	0.13407	75.64	01875	-29,364	2,581	0.13407	55.19
	P		107,426	-41,644	14,059	0.13407		10.24	101,655	-39,307	7,712		0.13407	18.64	-38,151	2,146
S	A		5,523	4,786	0.13407	28.82		6,566	7,691	0.13407	17.92		7,092	10,941	0.13407	12.59
	P		-26,969	7,860	0.13407	18.08		-28,358	5,801	0.13407	24.53		-26,739	3,561	0.13407	39.90
P	A	01876	-32,059	6,996	0.13407	20.41	01877	-31,794	12,304	0.13407	11.60	01878	-	1,752	0.13407	86.62
	P		0	0	0.13407	-		0	0	0.13407	-		101,786	-38,965	9,862	0.13407
S	A		7,623	14,669	0.13407	9.38		8,334	18,911	0.13407	7.27		6,390	4,503	0.13407	30.61
	P		-25,086	1,269	0.13407	NS		0	0	0.13407	-		-28,269	6,906	0.13407	20.60
P	A	01879	-98,672	2,052	0.13407	73.76	01880	-30,371	4,807	0.13407	29.66	01881	-33,543	9,318	0.13407	15.34
	P		-38,820	4,283	0.13407	33.54		0	0	0.13407	-		0	0	0.13407	-
S	A		7,045	6,864	0.13407	20.07		7,556	9,543	0.13407	14.43		7,659	12,828	0.13407	10.73
	P		-28,172	4,682	0.13407	30.39		-26,565	2,399	0.13407	59.22		-25,046	46	0.13407	NS
P	A	01882	-98,857	1,528	0.13407	99.07	01883	-97,989	1,724	0.13407	87.74	01884	-28,335	3,197	0.13407	44.51
	P		-37,346	11,660	0.13407	12.30		-38,641	5,959	0.13407	24.10		-22,310	1,493	0.13407	94.79
S	A		5,573	1,747	0.13407	78.95		6,840	3,270	0.13407	42.13		7,524	4,829	0.13407	28.51
	P		-29,141	7,770	0.13407	18.33		-29,762	5,584	0.13407	25.52		-28,302	3,390	0.13407	41.98
P	A	01885	-31,331	6,910	0.13407	20.65	01886	-31,462	11,375	0.13407	12.55	01887	-94,899	1,419	0.13407	NS
	P		0	0	0.13407	-		0	0	0.13407	-		-33,680	6,978	0.13407	20.49
S	A		8,269	6,464	0.13407	21.28		14,022	7,864	0.13407	17.40		1,043	785	0.13407	NS
	P		-26,001	1,247	0.13407	NS		0	0	0.13407	-		-31,257	6,205	0.13407	22.99
P	A	01888	-25,278	1,854	0.13407	76.54	01889	-28,839	5,075	0.13407	28.05	01890	-33,910	9,013	0.13407	15.87
	P		-20,330	2,542	0.13407	55.57		-24,436	1,307	0.13407	NS		0	0	0.13407	-
S	A		8,199	2,198	0.13407	62.59		11,821	4,343	0.13407	31.57		17,215	7,516	0.13407	18.15
	P		-30,977	4,037	0.13407	35.33		-28,137	1,989	0.13407	71.53		-24,390	95	0.13407	NS
P	A	01891	-87,287	1,160	0.13407	NS	01892	-88,196	1,315	0.13407	NS	01893	-25,236	3,406	0.13407	41.66
	P		-29,528	7,548	0.13407	18.87		-17,904	3,064	0.13407	46.00		-21,932	2,149	0.13407	65.83
S	A		4,909	642	0.13407	NS		5,070	1,212	0.13407	NS		8,295	3,068	0.13407	44.84
	P		-33,378	6,067	0.13407	23.56		-32,589	4,015	0.13407	35.58		8,200	2,167	0.13407	63.49
P	A	01894	-29,772	6,185	0.13407	23.04	01895	-31,449	9,558	0.13407	14.93	01896	-77,815	1,008	0.13407	NS



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D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	P		-26,438	1,107	0.13407	NS		0	0	0.13407	-		-14,770	3,045	0.13407	46.16
S	A		12,002	5,591	0.13407	24.52		17,240	8,977	0.13407	15.20		7,140	387	0.13407	NS
	P		9,577	2,988	0.13407	45.99		10,424	4,701	0.13407	29.21		4,028	3,491	0.13407	39.57
P	A	01897	-19,803	2,008	0.13407	70.32	01898	-25,447	4,221	0.13407	33.62	01899	-32,516	6,573	0.13407	21.73
	P		-19,037	2,399	0.13407	58.82		-23,557	1,799	0.13407	78.76		-29,578	985	0.13407	NS
S	A		4,623	1,341	0.13407	NS		7,994	3,128	0.13407	43.99		12,276	5,728	0.13407	23.93
	P		6,376	4,196	0.13407	32.85		8,867	5,437	0.13407	25.29		11,755	7,539	0.13407	18.19
P	A	01900	-61,635	752	0.13407	NS	01901	-12,578	866	0.13407	NS	01902	-18,071	2,552	0.13407	55.24
	P		-10,548	2,802	0.13407	49.97		-15,267	2,183	0.13407	64.41		-20,140	1,839	0.13407	76.81
S	A		8,370	107	0.13407	NS		-35,487	1,059	0.13407	NS		-33,690	1,389	0.13407	NS
	P		851	4,228	0.13407	32.77		2,975	5,132	0.13407	26.94		6,466	6,504	0.13407	21.19
P	A	01903	-25,762	4,095	0.13407	34.67	01904	-31,030	5,814	0.13407	24.54	01905	-37,482	1,054	0.13407	NS
	P		-25,299	1,555	0.13407	91.26		-29,067	1,263	0.13407	NS		-9,098	1,658	0.13407	84.33
S	A		7,313	1,740	0.13407	79.14		9,932	3,389	0.13407	40.53		-42,770	5,781	0.13407	24.94
	P		10,368	8,519	0.13407	16.12		12,256	11,545	0.13407	11.87		-1,982	4,989	0.13407	27.84
P	A	01906	-39,845	1,604	0.13407	89.64	01907	-15,864	2,258	0.13407	62.31	01908	-26,724	3,045	0.13407	46.67
	P		-15,255	1,468	0.13407	95.79		-20,804	1,475	0.13407	95.82		-26,927	1,306	0.13407	NS
S	A		-44,254	4,902	0.13407	29.45		-34,469	3,366	0.13407	42.51		-26,495	1,513	0.13407	93.90
	P		1,205	6,565	0.13407	21.09		7,396	8,608	0.13407	16.00		13,074	11,295	0.13407	12.13
P	A	01909	-9,617	2,759	0.13407	50.70	01910	-1,555	2,233	0.13407	62.18	01911	-20,077	1,746	0.13407	80.89
	P		-4,268	1,043	0.13407	NS		-8,540	868	0.13407	NS		-14,235	1,048	0.13407	NS
S	A		-39,643	14,095	0.13407	10.20		-56,693	10,932	0.13407	13.35		-48,689	7,391	0.13407	19.26
	P		-7,549	4,168	0.13407	33.50		-5,958	5,811	0.13407	23.99		-310	7,806	0.13407	17.43
P	A	01912	-12,242	1,139	0.13407	NS	01913	-23,565	1,088	0.13407	NS	01914	8,957	3,037	0.13407	45.27
	P		-20,187	1,495	0.13407	94.48		-24,198	1,269	0.13407	NS		13,688	554	0.13407	NS
S	A		-24,363	3,994	0.13407	34.85		-11,760	907	0.13407	NS		-63,780	20,517	0.13407	7.03
	P		10,944	10,236	0.13407	13.15		18,916	13,191	0.13407	10.32		-13,604	4,177	0.13407	32.98
P	A	01915	6,317	2,553	0.13407	53.99	01916	-3,912	1,393	0.13407	99.89	01917	-8,069	633	0.13407	NS
	P		-5,364	442	0.13407	NS		-11,073	1,064	0.13407	NS		-14,577	1,597	0.13407	87.99
S	A		-74,372	12,892	0.13407	11.27		-39,158	7,344	0.13407	19.11		14,453	2,821	0.13407	47.36
	P		-10,344	6,823	0.13407	20.08		-1,804	9,274	0.13407	14.62		23,222	11,020	0.13407	12.02
P	A	02498	82,781	2,361	0.13407	54.18										
	P		0	0	0.13407	-										
S	A		75,380	42,394	0.13407	2.96										
	P		-42,686	5,725	0.13407	24.62										
Piano Terra			Parete P3-P6				Parete P3-P6									
P	A	00012	65,798	7,012	0.13407	18.56	00013	-23,286	15,762	0.13407	8.99	00014	1,629	19,408	0.13407	7.13
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		51,403	927	0.13407	NS		-65,081	4,281	0.13407	34.35		-21,928	4,567	0.13407	30.38
	P		32,718	1,257	0.13407	NS		0	0	0.13407	-		-19,434	548	0.13407	NS
P	A	00015	-22,638	24,208	0.13407	5.85	00016	-8,105	25,783	0.13407	5.42	00017	-13,102	24,985	0.13407	5.62
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-18,899	6,920	0.13407	20.39		-23,012	4,265	0.13407	33.20		-33,922	6,886	0.13407	20.77
	P		0	0	0.13407	-		-25,972	522	0.13407	NS		0	0	0.13407	-
P	A	00018	-21,584	30,361	0.13407	4.66	00019	-30,958	30,236	0.13407	4.72	00020	-33,473	30,525	0.13407	4.68
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-39,047	6,205	0.13407	23.16		-52,964	6,269	0.13407	23.21		-51,295	6,271	0.13407	23.16
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	00021	-31,731	29,674	0.13407	4.81	00022	-35,356	30,032	0.13407	4.77	00023	-29,408	30,507	0.13407	4.67
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-64,688	7,409	0.13407	19.84		-56,680	7,614	0.13407	19.17		-58,874	6,016	0.13407	24.31
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	00024	-42,740	30,814	0.13407	4.68	00025	-29,047	32,816	0.13407	4.34	00026	-36,637	30,806	0.13407	4.65
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-64,172	7,220	0.13407	20.35		-61,509	6,862	0.13407	21.36		-67,299	7,055	0.13407	20.88
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	00027	-33,152	30,827	0.13407	4.64	00028	-34,985	30,076	0.13407	4.76	00029	-36,313	29,981	0.13407	4.78
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-62,466	6,278	0.13407	23.37		-61,458	7,394	0.13407	19.82		-65,043	7,814	0.13407	18.82
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	00030	-31,814	30,702	0.13407	4.65	00031	-29,846	30,075	0.13407	4.74	00032	-22,893	31,783	0.13407	4.46
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-54,650	6,251	0.13407	23.31		-55,062	6,843	0.13407	21.30		-45,847	6,667	0.13407	21.68
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	00033	-38,614	29,426	0.13407	4.88	00034	-16,516	28,112	0.13407	5.01	00035	-26,642	26,721	0.13407	5.32
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-44,786	6,980	0.13407	20.69		-31,431	5,290	0.13407	26.98		-24,028	6,704	0.13407	21.14
	P		0	0	0.13407	-		-30,063	116	0.13407	NS		0	0	0.13407	-
P	A	00036	-21,773	24,076	0.13407	5.88	00037	-39,445	21,634	0.13407	6.64	00038	-33,189	15,697	0.13407	9.11
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-7,075	5,058	0.13407	27.59		-13,564	3,534	0.13407	39.73		-75,829	1,440	0.13407	NS
	P		-16,931	688	0.13407	NS		24,542	863	0.13407	NS		64,845	3,396	0.13407	38.35
P	A	00039	1,647	9,302	0.13407	14.88	00053	215,565	13,818	0.13407	8.01	00055	215,195	11,477	0.13407	9.65
	P		0	0	0.13407	-		0	0	0.13407	-		121,521	3,388	0.13407	36.27
S	A		-	5,010	0.13407	31.05		-29,114	16,850	0.13407	8.29		-	20,754	0.13407	7.25
	P		131,536	0	0.13407	-		218,952	4,832	0.13407	22.25		115,513	0	0.13407	-
P	A	00138	13,177	2,264	0.13407	60.49	00139	13,252	2,674	0.13407	51.21	00417	21,211	8,765	0.13407	15.50
	P		-25,145	2,104	0.13407	67.44		-27,095	2,086	0.13407	68.14		0	0	0.13407	-
S	A		3,292	274	0.13407	NS		5,230	550	0.13407	NS		72,489	1,000	0.13407	NS



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	P		-7,384	34	0.13407	NS		0	0	0.13407	-		-62,245	3,005	0.13407	48.81
P	A	00525	-13,925	2,186	0.13407	64.25	00526	6,976	2,767	0.13407	49.78	00527	11,382	4,642	0.13407	29.55
	P		10,078	14	0.13407	NS		15,089	649	0.13407	NS		-393	939	0.13407	NS
S	A		-34,242	6,679	0.13407	21.42		-27,358	13,272	0.13407	10.71		-30,624	15,876	0.13407	8.98
	P		18,784	2,642	0.13407	51.56		11,417	3,740	0.13407	36.68		6,996	3,782	0.13407	36.42
P	A	00528	22,579	4,175	0.13407	32.51	00529	26,871	3,722	0.13407	36.32	00530	48,112	3,407	0.13407	38.87
	P		26,419	1,142	0.13407	NS		23,797	1,028	0.13407	NS		44,213	1,386	0.13407	95.90
S	A		-35,040	19,932	0.13407	7.18		-26,784	14,331	0.13407	9.92		-13,960	9,981	0.13407	14.07
	P		9,066	4,850	0.13407	28.34		10,940	4,221	0.13407	32.51		7,557	5,184	0.13407	26.56
P	A	00531	133,107	1,378	0.13407	88.09	00532	177,458	2,244	0.13407	51.52	00549	200,675	8,715	0.13407	12.92
	P		113,784	1,056	0.13407	NS		23,923	5,589	0.13407	24.25		43,275	2,194	0.13407	60.64
S	A		1,423	6,163	0.13407	22.47		18,957	1,768	0.13407	77.03		20,896	8,728	0.13407	15.58
	P		30,892	5,554	0.13407	24.24		38,967	8,019	0.13407	16.66		31,370	3,289	0.13407	40.92
P	A	00550	97,490	3,727	0.13407	33.81	00551	86,968	2,929	0.13407	43.49	00552	34,077	4,576	0.13407	29.33
	P		8,044	695	0.13407	NS		64,260	984	0.13407	NS		26,282	1,004	0.13407	NS
S	A		413	6,578	0.13407	21.07		-9,243	15,010	0.13407	9.32		-29,620	14,972	0.13407	9.52
	P		17,432	2,884	0.13407	47.29		16,676	4,377	0.13407	31.18		2,123	4,004	0.13407	34.56
P	A	00553	12,672	4,109	0.13407	33.34	00554	10,540	4,360	0.13407	31.49	00555	-1,100	2,972	0.13407	46.70
	P		10,414	1,111	0.13407	NS		15,324	664	0.13407	NS		-1,702	682	0.13407	NS
S	A		-31,596	15,904	0.13407	8.97		-34,388	20,495	0.13407	6.98		-26,418	10,268	0.13407	13.83
	P		8,794	3,533	0.13407	38.92		9,482	4,154	0.13407	33.08		11,522	2,910	0.13407	47.13
P	A	00556	-18,361	2,705	0.13407	52.13	00763	-34,320	4,457	0.13407	32.10	00764	-49,022	11,961	0.13407	12.12
	P		19,700	234	0.13407	NS		0	0	0.13407	-		0	0	0.13407	-
S	A		-28,669	6,933	0.13407	20.53		-17,969	2,039	0.13407	69.13		-31,681	4,130	0.13407	34.56
	P		18,198	2,666	0.13407	51.12		0	0	0.13407	-		0	0	0.13407	-
P	A	00765	-48,277	16,802	0.13407	8.62	00766	-47,127	23,310	0.13407	6.21	00767	-39,992	22,404	0.13407	6.42
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-43,248	3,723	0.13407	38.74		-59,714	5,257	0.13407	27.84		-60,957	6,650	0.13407	22.03
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	00768	-49,705	23,510	0.13407	6.17	00769	-39,669	27,946	0.13407	5.14	00770	-32,556	23,990	0.13407	5.95
	P		0	0	0.13407	-		0	0	0.13407	-		-13,317	24	0.13407	NS
S	A		-66,660	5,437	0.13407	27.08		-80,991	5,947	0.13407	25.07		-81,922	6,573	0.13407	22.70
	P		0	0	0.13407	-		0	0	0.13407	-		6,095	134	0.13407	NS
P	A	00771	-44,041	23,989	0.13407	6.02	00772	-34,854	28,093	0.13407	5.10	00773	-25,921	23,512	0.13407	6.04
	P		-16,348	294	0.13407	NS		-14,781	205	0.13407	NS		-12,912	654	0.13407	NS
S	A		-83,213	5,845	0.13407	25.56		-94,539	5,684	0.13407	26.54		-95,728	6,101	0.13407	24.75
	P		6,234	25	0.13407	NS		-11,819	48	0.13407	NS		7,448	167	0.13407	NS
P	A	00774	-37,344	23,482	0.13407	6.11	00775	-30,809	27,218	0.13407	5.24	00776	-24,258	23,089	0.13407	6.14
	P		-15,757	753	0.13407	NS		-14,670	659	0.13407	NS		-13,153	921	0.13407	NS
S	A		-93,230	6,011	0.13407	25.06		-	5,268	0.13407	28.88		-	5,671	0.13407	26.81
	P		-12,760	95	0.13407	NS		104,693	160	0.13407	NS		104,102	190	0.13407	NS
P	A	00777	-33,066	23,058	0.13407	6.20	00778	-29,309	26,561	0.13407	5.36	00779	-24,663	22,920	0.13407	6.19
	P		-15,046	918	0.13407	NS		-14,397	824	0.13407	NS		-13,089	1,025	0.13407	NS
S	A		-	6,208	0.13407	24.44		-	5,064	0.13407	30.12		-	5,362	0.13407	28.47
	P		101,527	128	0.13407	NS		107,857	205	0.13407	NS		108,688	225	0.13407	NS
P	A	00780	-31,462	23,019	0.13407	6.20	00781	-29,425	25,977	0.13407	5.48	00782	-27,605	23,047	0.13407	6.17
	P		-14,708	976	0.13407	NS		-14,056	916	0.13407	NS		-14,370	1,054	0.13407	NS
S	A		-	6,586	0.13407	23.18		-	4,946	0.13407	30.85		-	5,169	0.13407	29.54
	P		108,582	129	0.13407	NS		108,027	226	0.13407	NS		108,915	239	0.13407	NS
P	A	00783	-31,823	23,260	0.13407	6.14	00784	-31,598	25,873	0.13407	5.52	00785	-26,445	22,912	0.13407	6.20
	P		-14,523	1,015	0.13407	NS		-14,114	932	0.13407	NS		-14,941	1,030	0.13407	NS
S	A		-	6,803	0.13407	22.42		-	5,079	0.13407	29.91		-	5,117	0.13407	29.68
	P		107,639	139	0.13407	NS		102,961	217	0.13407	NS		102,557	224	0.13407	NS
P	A	00786	-31,545	25,622	0.13407	5.57	00787	-29,837	23,774	0.13407	5.99	00788	-22,959	23,841	0.13407	5.94
	P		-14,197	812	0.13407	NS		-13,323	843	0.13407	NS		-13,566	631	0.13407	NS
S	A		-	5,108	0.13407	29.67		-93,883	7,119	0.13407	21.17		-91,948	5,151	0.13407	29.22
	P		100,187	197	0.13407	NS		6,959	207	0.13407	NS		-11,869	182	0.13407	NS
P	A	00789	-32,258	26,325	0.13407	5.42	00790	-35,085	23,774	0.13407	6.02	00791	-27,836	23,524	0.13407	6.05
	P		-13,503	371	0.13407	NS		-13,304	227	0.13407	NS		0	0	0.13407	-
S	A		-94,344	5,263	0.13407	28.65		-78,243	6,863	0.13407	21.67		-78,206	5,685	0.13407	26.16
	P		-11,881	108	0.13407	NS		5,725	42	0.13407	NS		0	0	0.13407	-
P	A	00792	-37,774	26,162	0.13407	5.49	00793	-40,679	21,715	0.13407	6.63	00794	-34,617	19,105	0.13407	7.49
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-74,159	5,229	0.13407	28.34		-63,670	6,201	0.13407	23.68		-55,828	5,513	0.13407	26.46
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	00795	-38,129	18,520	0.13407	7.75	00796	-48,412	11,450	0.13407	12.65	00797	-26,168	4,647	0.13407	30.56
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-50,071	4,065	0.13407	35.70		-34,931	2,825	0.13407	50.67		-16,365	2,167	0.13407	64.96
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	01059	-35,215	30,400	0.13407	4.71	01061	-30,904	30,463	0.13407	4.68	01062	-34,744	31,025	0.13407	4.61
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-60,133	6,952	0.13407	21.06		-55,630	5,221	0.13407	27.93		-53,716	5,611	0.13407	25.94
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	01064	-34,072	31,399	0.13407	4.56	01067	-35,360	30,711	0.13407	4.66	01069	-33,103	30,855	0.13407	4.63



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D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
S	A		-54,312	5,672	0.13407	25.68		-58,381	5,464	0.13407	26.75		-50,207	5,553	0.13407	26.13
P	P	01071	0	0	0.13407	-	01072	0	0	0.13407	-	01075	0	0	0.13407	-
S	A		-31,687	30,408	0.13407	4.69		-29,898	30,269	0.13407	4.71		-34,447	31,427	0.13407	4.55
P	P	01077	0	0	0.13407	-	01079	0	0	0.13407	-	01080	0	0	0.13407	-
S	A		-38,538	4,819	0.13407	29.80		-61,468	6,702	0.13407	21.87		-53,219	5,734	0.13407	25.38
P	P	01077	14	0	0.13407	NS		0	0	0.13407	-		0	0	0.13407	-
S	A		-24,631	26,315	0.13407	5.39		-25,373	28,689	0.13407	4.95		-46,304	18,479	0.13407	7.83
P	P	01082	0	0	0.13407	-		0	0	0.13407	-	01087	0	0	0.13407	-
S	A		-14,155	4,328	0.13407	32.46		-24,507	5,093	0.13407	27.84		8,058	2,169	0.13407	62.26
P	P	01082	0	0	0.13407	-		0	0	0.13407	-		31,558	950	0.13407	NS
S	A		-28,800	23,151	0.13407	6.15		-15,461	28,395	0.13407	4.95		-33,936	29,984	0.13407	4.77
P	P	01089	0	0	0.13407	-		0	0	0.13407	-	01093	0	0	0.13407	-
S	A		1,282	2,772	0.13407	49.96		-26,294	5,956	0.13407	23.85		-53,785	7,119	0.13407	20.45
P	P	01089	3,868	1,668	0.13407	82.82		0	0	0.13407	-		0	0	0.13407	-
S	A		-35,490	30,877	0.13407	4.64		-30,157	29,775	0.13407	4.79		-24,036	29,358	0.13407	4.83
P	P	01095	0	0	0.13407	-		0	0	0.13407	-	01098	0	0	0.13407	-
S	A		-48,661	5,143	0.13407	28.18		-41,768	5,453	0.13407	26.41		-38,590	4,835	0.13407	29.71
P	P	01095	0	0	0.13407	-		0	0	0.13407	-		-26,385	627	0.13407	NS
S	A		-35,981	28,687	0.13407	4.99		-3,627	26,784	0.13407	5.19		-37,880	29,411	0.13407	4.88
P	P	01101	0	0	0.13407	-		0	0	0.13407	-	01105	0	0	0.13407	-
S	A		-41,127	5,625	0.13407	25.59		-24,732	5,548	0.13407	25.57		-46,564	7,213	0.13407	20.05
P	P	01101	0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-24,849	28,596	0.13407	4.96		-24,984	26,622	0.13407	5.33		-16,815	12,195	0.13407	11.55
P	P	01106	0	0	0.13407	-		0	0	0.13407	-	01111	0	0	0.13407	-
S	A		-30,785	6,033	0.13407	23.64		-30,010	5,165	0.13407	27.59		-9,087	3,900	0.13407	35.85
P	P	01106	-45,546	392	0.13407	NS		0	0	0.13407	-		0	0	0.13407	-
S	A		-16,644	22,630	0.13407	6.22		-4,369	17,609	0.13407	7.91		-30,966	4,384	0.13407	32.54
P	P	01113	0	0	0.13407	-		0	0	0.13407	-	01111	-4,824	1,654	0.13407	84.20
S	A		-23,507	4,018	0.13407	35.26		-20,626	2,645	0.13407	53.42		44,007	813	0.13407	NS
P	P	01113	0	0	0.13407	-		-1,182	625	0.13407	NS		-94,848	1,488	0.13407	99.19
S	A		-7,074	11,063	0.13407	12.61		-22,025	1,812	0.13407	78.08		74,403	5,148	0.13407	25.06
P	P	02063	0	0	0.13407	-		0	0	0.13407	-	02062	0	0	0.13407	-
S	A		-25,508	844	0.13407	NS		-20,528	2,309	0.13407	61.19		-16,416	1,155	0.13407	NS
P	P	02063	4,739	3,503	0.13407	38.35		4,863	301	0.13407	NS		99,283	2,775	0.13407	45.33
S	A		150,896	4,581	0.13407	25.99		-27,446	1,971	0.13407	72.14		-30,386	1,663	0.13407	85.73
P	P	02066	0	0	0.13407	-		0	0	0.13407	-	02065	0	0	0.13407	-
S	A		-57,847	2,376	0.13407	61.49		-19,511	1,919	0.13407	73.56		-23,802	336	0.13407	NS
P	P	02066	49,530	1,207	0.13407	NS		6,823	256	0.13407	NS		-1,805	31	0.13407	NS
S	A		-11,578	246	0.13407	NS		157	346	0.13407	NS		16,806	1,370	0.13407	99.61
P	P	02069	909	3,245	0.13407	42.69		13,798	2,554	0.13407	53.59		1,509	300	0.13407	NS
S	A		-33,879	575	0.13407	NS		-28,104	2,374	0.13407	59.93		-11,449	2,239	0.13407	62.58
P	P	02069	7,954	853	0.13407	NS		9,512	1,100	0.13407	NS		945	854	0.13407	NS
S	A		41,112	6,136	0.13407	21.73		-43,415	1,409	0.13407	NS		-29,348	1,030	0.13407	NS
P	P	02072	0	0	0.13407	-		-18,622	4,415	0.13407	31.95		-4,558	7,945	0.13407	17.52
S	A		-22,204	1,817	0.13407	77.88		8,062	647	0.13407	NS		9,489	536	0.13407	NS
P	P	02072	26,110	681	0.13407	NS		-35,620	3,108	0.13407	46.09		-32,348	4,476	0.13407	31.91
S	A		-23,808	1,950	0.13407	72.68		-19,066	5,198	0.13407	27.15		-45,036	6,103	0.13407	23.67
P	P	02075	-2,130	4,561	0.13407	30.46		0	0	0.13407	-	02074	-13,857	11	0.13407	NS
S	A		9,476	762	0.13407	NS		-4,344	925	0.13407	NS		1,932	731	0.13407	NS
P	P	02075	-20,092	3,276	0.13407	43.11		25,617	1,458	0.13407	92.82		-46,075	456	0.13407	NS
S	A		-47,814	1,741	0.13407	83.18		-38,693	2,326	0.13407	61.75		-38,097	3,958	0.13407	36.27
P	P	02078	-19,692	9,923	0.13407	14.23		-10,823	10,122	0.13407	13.84		-11,550	2,595	0.13407	54.00
S	A		7,941	1,033	0.13407	NS		8,189	1,229	0.13407	NS		1,986	1,426	0.13407	97.05
P	P	02078	-39,514	5,039	0.13407	28.53		-29,347	5,540	0.13407	25.71		-17,508	3,117	0.13407	45.21
S	A		-27,727	14,052	0.13407	10.12		-53,645	2,012	0.13407	72.35		-49,722	2,571	0.13407	56.42
P	P	02081	0	0	0.13407	-		-28,220	5,228	0.13407	27.22		-20,084	13,283	0.13407	10.63
S	A		-19,124	1,292	0.13407	NS		2,623	813	0.13407	NS		4,948	1,228	0.13407	NS
P	P	02081	5,485	955	0.13407	NS		-53,478	3,111	0.13407	46.78		-40,290	5,477	0.13407	26.26
S	A		-41,723	3,863	0.13407	37.28		-29,647	7,295	0.13407	19.53		-42,999	8,163	0.13407	17.66
P	P	02084	-13,130	8,589	0.13407	16.34		0	0	0.13407	-	02083	-14,024	654	0.13407	NS
S	A		157	1,471	0.13407	94.24		-16,393	1,397	0.13407	NS		2,090	413	0.13407	NS
P	P	02084	-29,450	4,371	0.13407	32.59		-19,541	1,387	0.13407	NS		-10,077	213	0.13407	NS
S	A		-53,343	2,500	0.13407	58.21		-46,561	3,690	0.13407	39.20		-38,910	5,409	0.13407	26.56
P	P	02087	-26,030	12,098	0.13407	11.74		-18,965	13,349	0.13407	10.57		-14,872	3,557	0.13407	39.52
S	A		1,884	955	0.13407	NS		-1,135	1,323	0.13407	NS		-9,478	1,561	0.13407	89.60
P	P	02087	-53,987	4,170	0.13407	34.92		-41,421	4,585	0.13407	31.40		-31,607	2,086	0.13407	68.42
S	A		-25,385	18,159	0.13407	7.82		-56,285	2,017	0.13407	72.34		-51,323	3,342	0.13407	43.47
P	P	02090	0	0	0.13407	-		-27,942	5,340	0.13407	26.64		-23,423	15,019	0.13407	9.43
S	A		-36,878	2,514	0.13407	57.04		-21	612	0.13407	NS		-2,195	1,049	0.13407	NS
P	P	02090	0	0	0.13407	-		-70,964	2,668	0.13407	55.40		-54,298	4,385	0.13407	33.22
S	A		-42,755	4,949	0.13407	29.13		-31,672	8,479	0.13407	16.83		-31,240	7,940	0.13407	17.97
P	P	02093	-19,345	9,968	0.13407	14.16		0	0	0.13407	-	02092	-14,522	1,230	0.13407	NS
S	A		-8,375	1,424	0.13407	98.12		-18,324	1,560	0.13407	90.39		-5,262	420	0.13407	NS
P	P	02093	-42,767	3,178	0.13407	45.36		-33,869	274	0.13407	NS		-12,311	326	0.13407	NS
S	A		-54,665	2,778	0.13407	52.45		-46,435	4,381	0.13407	33.01		-38,066	6,250	0.13407	22.97
P	P	02096	-26,064	12,777	0.13407	11.11		-21,061	14,241	0.13407	9.93		-17,742	3,587	0.13407	39.29
S	A		-1,924	779	0.13407	NS		-6,992	1,199	0.13407	NS		-14,509	1,557	0.13407	90.25
P	P	02096	-67,975	3,575	0.13407	41.23		-54,309	3,725	0.13407	39.10		-43,401	1,379	0.13407	NS
S	A		-27,507	19,305	0.13407	7.37		-58,656	1,982	0.13407	73.77		-51,905	3,691	0.13407	39.38
P	P	02097	0	0	0.13407	-		-26,681	5,587	0.13407	25.43		-23,849	15,512	0.13407	9.14



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
S	A		-48,430	2,911	0.13407	49.78		-1,137	538	0.13407	NS		-5,510	959	0.13407	NS
P	A	02099	0	0	0.13407	-		-83,530	2,572	0.13407	58.09		-65,768	3,941	0.13407	37.33
P	A		-42,777	5,531	0.13407	26.07	02100	-36,145	9,255	0.13407	15.48	02101	-30,755	7,598	0.13407	18.77
P	A		-21,348	10,208	0.13407	13.85		0	0	0.13407	-		-15,081	1,539	0.13407	91.35
S	A		-11,849	1,359	0.13407	NS		-20,311	1,597	0.13407	88.46		-7,017	398	0.13407	NS
P	A	02102	-53,306	2,680	0.13407	54.30		0	0	0.13407	-		-14,074	407	0.13407	NS
P	A		-56,089	2,904	0.13407	50.23	02103	-46,864	4,720	0.13407	30.66	02104	-38,209	6,709	0.13407	21.40
P	A		-25,485	13,070	0.13407	10.86		-21,905	14,453	0.13407	9.79		-19,280	3,496	0.13407	40.37
S	A		-3,462	722	0.13407	NS		-9,284	1,146	0.13407	NS		-16,412	1,546	0.13407	91.05
P	A	02105	-77,630	3,444	0.13407	43.16		-63,408	3,461	0.13407	42.42		-51,795	1,111	0.13407	NS
P	A		-31,977	20,358	0.13407	7.01	02106	-60,704	1,993	0.13407	73.50	02107	-52,648	3,855	0.13407	37.73
S	A		0	0	0.13407	-		-26,067	5,849	0.13407	24.28		-23,832	15,681	0.13407	9.04
S	A		-56,518	3,075	0.13407	47.46		-1,056	525	0.13407	NS		-6,812	929	0.13407	NS
P	A	02108	0	0	0.13407	-		-90,790	2,565	0.13407	58.61		-73,101	3,861	0.13407	38.35
P	A		-43,123	5,818	0.13407	24.79	02109	-37,468	9,967	0.13407	14.40	02110	-29,290	7,318	0.13407	19.46
P	A		-22,380	10,223	0.13407	13.84		0	0	0.13407	-		-14,868	1,670	0.13407	84.17
S	A		-13,318	1,336	0.13407	NS		-21,151	1,575	0.13407	89.76		-8,354	384	0.13407	NS
P	A	02111	-60,230	2,588	0.13407	56.57		-49,188	277	0.13407	NS		-15,139	444	0.13407	NS
P	A		-56,804	2,963	0.13407	49.27	02112	-47,273	4,872	0.13407	29.71	02113	-38,583	6,920	0.13407	20.76
P	A		-24,957	13,222	0.13407	10.73		-22,152	14,507	0.13407	9.75		-20,224	3,430	0.13407	41.18
S	A		-4,157	716	0.13407	NS		-10,188	1,131	0.13407	NS		-17,156	1,532	0.13407	91.95
P	A	02114	-82,952	3,448	0.13407	43.31		-68,592	3,428	0.13407	43.03		-56,747	1,074	0.13407	NS
P	A		-34,275	20,668	0.13407	6.92	02115	-61,846	1,999	0.13407	73.35	02116	-51,344	3,889	0.13407	37.35
P	A		0	0	0.13407	-		-25,701	6,000	0.13407	23.66		-23,681	15,744	0.13407	9.00
S	A		-62,032	3,142	0.13407	46.67		-809	513	0.13407	NS		-7,315	923	0.13407	NS
P	A	02117	0	0	0.13407	-		-93,600	2,569	0.13407	58.66		-76,361	3,869	0.13407	38.38
P	A		-43,234	5,919	0.13407	24.37	02118	-38,757	9,787	0.13407	14.68	02119	-27,993	7,220	0.13407	19.70
P	A		-22,633	10,220	0.13407	13.85		0	0	0.13407	-		-14,546	1,713	0.13407	82.03
S	A		-13,841	1,334	0.13407	NS		-21,407	1,623	0.13407	87.13		-9,079	369	0.13407	NS
P	A	02120	-63,411	2,564	0.13407	57.26		0	0	0.13407	-		-15,202	456	0.13407	NS
P	A		-56,975	2,958	0.13407	49.36	02121	-47,322	4,886	0.13407	29.63	02122	-38,424	6,954	0.13407	20.65
P	A		-24,789	13,284	0.13407	10.68		-22,083	14,517	0.13407	9.75		-20,285	3,396	0.13407	41.60
S	A		-4,353	699	0.13407	NS		-10,427	1,130	0.13407	NS		-17,491	1,538	0.13407	91.61
P	A	02123	-84,158	3,449	0.13407	43.34		-69,862	3,448	0.13407	42.82		-58,012	1,136	0.13407	NS
P	A		-33,153	20,312	0.13407	7.04	02124	-61,656	1,974	0.13407	74.26	02125	-52,807	3,867	0.13407	37.62
P	A		0	0	0.13407	-		-25,562	6,057	0.13407	23.43		-23,566	15,753	0.13407	8.99
S	A		-62,781	3,068	0.13407	47.83		-468	503	0.13407	NS		-7,263	920	0.13407	NS
P	A	02126	0	0	0.13407	-		-92,127	2,511	0.13407	59.94		-75,617	3,879	0.13407	38.26
P	A		-43,150	5,863	0.13407	24.60	02127	-38,193	9,745	0.13407	14.73	02128	-26,571	7,153	0.13407	19.86
P	A		-22,399	10,227	0.13407	13.84		0	0	0.13407	-		-14,259	1,722	0.13407	81.58
S	A		-13,708	1,333	0.13407	NS		-21,225	1,619	0.13407	87.33		-8,694	371	0.13407	NS
P	A	02129	-62,773	2,576	0.13407	56.97		0	0	0.13407	-		-14,775	444	0.13407	NS
P	A		-56,378	2,887	0.13407	50.54	02130	-47,114	4,768	0.13407	30.35	02131	-38,533	6,795	0.13407	21.14
P	A		-24,910	13,205	0.13407	10.74		-21,833	14,505	0.13407	9.75		-19,685	3,454	0.13407	40.88
S	A		-4,108	700	0.13407	NS		-9,892	1,129	0.13407	NS		-16,768	1,527	0.13407	92.21
P	A	02132	-81,356	3,506	0.13407	42.54		-67,202	3,457	0.13407	42.61		-55,546	1,092	0.13407	NS
P	A		-33,968	20,585	0.13407	6.95	02133	-59,623	1,951	0.13407	75.01	02134	-52,338	3,723	0.13407	39.05
P	A		0	0	0.13407	-		-26,282	6,198	0.13407	22.92		-23,528	15,710	0.13407	9.02
S	A		-61,050	3,129	0.13407	46.83		-1,250	467	0.13407	NS		-6,488	925	0.13407	NS
P	A	02135	0	0	0.13407	-		-86,585	1,846	0.13407	81.15		-70,863	3,802	0.13407	38.87
P	A		-43,063	5,636	0.13407	25.59	02136	-36,334	9,829	0.13407	14.58	02137	-31,696	7,319	0.13407	19.50
P	A		-21,714	10,240	0.13407	13.81		0	0	0.13407	-		-14,360	1,604	0.13407	87.59
S	A		-12,670	1,340	0.13407	NS		-20,815	1,563	0.13407	90.42		-6,978	369	0.13407	NS
P	A	02138	-58,334	2,625	0.13407	55.68		-47,575	312	0.13407	NS		-13,704	385	0.13407	NS
P	A		-55,124	2,763	0.13407	52.75	02139	-46,659	4,488	0.13407	32.23	02140	-38,344	6,424	0.13407	22.35
P	A		-25,225	13,080	0.13407	10.85		-21,236	14,447	0.13407	9.79		-18,171	3,560	0.13407	39.60
S	A		-3,205	734	0.13407	NS		-8,220	1,169	0.13407	NS		-15,206	1,559	0.13407	90.19
P	A	02141	-74,223	3,539	0.13407	41.88		-60,616	3,555	0.13407	41.20		-49,553	1,154	0.13407	NS
P	A		-29,389	20,121	0.13407	7.08	02142	-57,483	1,907	0.13407	76.59	02143	-51,334	3,437	0.13407	42.27
P	A		0	0	0.13407	-		-27,933	5,741	0.13407	24.78		-23,254	15,489	0.13407	9.15
S	A		-53,635	2,971	0.13407	49.00		-2,058	553	0.13407	NS		-4,349	1,006	0.13407	NS
P	A	02144	0	0	0.13407	-		-79,689	2,457	0.13407	60.61		-61,975	4,107	0.13407	35.70
P	A		-42,769	5,165	0.13407	27.91	02145	-33,256	9,231	0.13407	15.48	02146	-34,902	7,688	0.13407	18.62
P	A		-20,351	10,191	0.13407	13.86		0	0	0.13407	-		-14,341	1,193	0.13407	NS
S	A		-9,788	1,407	0.13407	99.44		-18,220	1,555	0.13407	90.67		704	372	0.13407	NS
P	A	02147	-50,283	2,862	0.13407	50.71		-40,854	386	0.13407	NS		-12,167	301	0.13407	NS
P	A		-53,370	2,555	0.13407	56.96	02148	-46,027	3,935	0.13407	36.74	02149	-37,874	5,719	0.13407	25.10
P	A		-25,337	12,778	0.13407	11.11		-19,802	14,090	0.13407	10.02		-16,497	3,649	0.13407	38.58
S	A		-1,025	850	0.13407	NS		-4,191	1,289	0.13407	NS		-11,522	1,601	0.13407	87.53
P	A	02150	-62,732	3,773	0.13407	38.89		-50,295	4,000	0.13407	36.28		-40,463	1,531	0.13407	93.97
P	A		-22,509	18,997	0.13407	7.45	02151	-54,928	1,971	0.13407	73.94	02152	-49,882	2,865	0.13407	50.64
P	A		0	0	0.13407	-		-29,437	5,571	0.13407	25.57		-21,468	14,646	0.13407	9.66
S	A		-43,306	2,893	0.13407	49.86		-723	713	0.13407	NS		777	1,176	0.13407	NS
P	A	02153	0	0	0.13407	-		-64,091	2,820	0.13407	52.10		-49,374	4,805	0.13407	30.18
P	A		-42,028	4,252	0.13407	33.88	02154	-29,394	7,798	0.13407	18.27	02155	-46,457	7,312	0.13407	19.78
P	A		-14,648	9,597	0.13407	14.64		0	0	0.13407	-		-13,980	490	0.13407	NS
S	A		-3,568	1,524	0.13407	91.28		-14,925	1,600	0.13407	87.86		-1,459	604	0.13407	NS
P	A	02156	-39,296	3,529	0.13407	40.72		-31,664	404	0.13407	NS		-63,047	415	0.13407	NS
P	A		-50,477	2,079	0.134											



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
S	A		3,751	1,050	0.13407	NS		4,054	1,376	0.13407	NS		-2,456	1,614	0.13407	86.10
	P		-48,170	4,631	0.13407	31.28		-37,734	5,054	0.13407	28.40		-29,389	2,377	0.13407	59.92
P	A	02159	-24,008	16,514	0.13407	8.58	02160	-51,758	1,818	0.13407	79.94	02161	-41,717	1,698	0.13407	84.82
	P		0	0	0.13407	-		-25,925	5,398	0.13407	26.30		-12,367	11,568	0.13407	12.12
S	A		-36,531	2,477	0.13407	57.88		2,836	841	0.13407	NS		8,056	1,045	0.13407	NS
	P		0	0	0.13407	-		-45,213	3,525	0.13407	40.99		-37,186	5,721	0.13407	25.07
P	A	02162	-32,936	2,653	0.13407	53.86	02163	-20,384	5,837	0.13407	24.20	02164	-53,339	4,110	0.13407	35.41
	P		-5,124	7,357	0.13407	18.94		0	0	0.13407	-		0	0	0.13407	-
S	A		7,643	1,285	0.13407	NS		-8,459	1,374	0.13407	NS		-309	673	0.13407	NS
	P		-27,800	4,334	0.13407	32.82		-20,467	1,140	0.13407	NS		-38,058	1,189	0.13407	NS
P	A	02165	-34,615	958	0.13407	NS	02166	-20,053	1,045	0.13407	NS	02167	-17,296	2,321	0.13407	60.70
	P		-8,683	7,698	0.13407	18.16		864	7,218	0.13407	19.19		3,030	1,859	0.13407	74.37
S	A		8,113	396	0.13407	NS		9,257	350	0.13407	NS		11,040	812	0.13407	NS
	P		-36,890	4,364	0.13407	32.86		-29,123	4,080	0.13407	34.90		-16,889	1,835	0.13407	76.74
P	A	02168	-6,893	10,273	0.13407	13.58	02169	-23,593	616	0.13407	NS	02170	-1,182	60	0.13407	NS
	P		0	0	0.13407	-		-8,815	2,387	0.13407	58.56		10,750	3,104	0.13407	44.22
S	A		-22,444	1,588	0.13407	89.13		0	0	0.13407	-		-34,280	1,285	0.13407	NS
	P		21,486	386	0.13407	NS		7,636	526	0.13407	NS		7,437	1,532	0.13407	89.87
P	A	02171	10,122	353	0.13407	NS	02172	33,435	3,092	0.13407	43.44					
	P		22,840	1,771	0.13407	76.62		-70	753	0.13407	NS					
S	A		-22,945	1,984	0.13407	71.37		-4,031	1,440	0.13407	96.64					
	P		11,781	1,573	0.13407	87.17		24,460	1,479	0.13407	91.60					
Piano Fondo Vasca			Parete P1-P2				Parete P1-P2									
P	A	00003	-27,237	1,789	0.13407	79.46	00047	94,076	30,140	0.13407	4.20	00048	-94,066	26,707	0.13407	5.65
	P		957	1,489	0.13407	93.03		150,215	843	0.13407	NS		13,355	898	0.13407	NS
S	A		-53,497	1,764	0.13407	82.51		-76,188	67,829	0.13407	2.19		-	135,387	0.13407	1.18
	P		6,452	734	0.13407	NS		0	0	0.13407	-		162,335	1,488	0.13407	37.96
P	A	00049	0	0	0.13407	-	00465	-91,509	31,791	0.13407	4.73	00466	-74,873	36,752	0.13407	4.04
	P		-54,258	7,804	0.13407	18.66		8,740	361	0.13407	NS		-2,095	644	0.13407	NS
S	A		0	0	0.13407	-		-	142,659	0.13407	1.11		-	136,381	0.13407	1.16
	P		-14,171	5,416	0.13407	25.94		150,549	5,108	0.13407	45.45		154,347	2,432	0.13407	52.42
P	A	00467	-81,363	36,240	0.13407	4.12	00468	-	27,535	0.13407	5.59	00469	-62,717	31,055	0.13407	4.73
	P		-30,422	533	0.13407	NS		119,363	492	0.13407	NS		-37,887	602	0.13407	NS
S	A		-	134,549	0.13407	1.18		-30,439	137,341	0.13407	1.15		-	116,089	0.13407	1.36
	P		156,708	2,484	0.13407	55.69		154,811	2,682	0.13407	51.54		145,119	3,241	0.13407	53.27
P	A	00470	-93,596	21,129	0.13407	7.13	00471	-48,669	17,387	0.13407	8.34	00472	3,475	13,563	0.13407	10.19
	P		-32,648	507	0.13407	NS		-37,415	695	0.13407	NS		-36,086	592	0.13407	NS
S	A		-	104,357	0.13407	1.48		-	76,113	0.13407	2.01		-52,935	43,358	0.13407	3.36
	P		120,205	4,779	0.13407	47.06		113,236	7,981	0.13407	45.25		9,788	3,367	0.13407	40.80
P	A	00473	-28,564	6,176	0.13407	23.05	00578	119,597	8,276	0.13407	14.88	00579	51,764	15,566	0.13407	8.48
	P		-8,894	206	0.13407	NS		0	0	0.13407	-		52,342	399	0.13407	NS
S	A		-69,101	17,968	0.13407	8.21		-26,303	57,854	0.13407	2.46		-43,374	59,077	0.13407	2.44
	P		21,980	3,181	0.13407	42.69		39,280	990	0.13407	NS		8,284	1,404	0.13407	97.99
P	A	00580	23,954	16,983	0.13407	7.98	00581	-1,154	13,489	0.13407	10.29	00582	3,584	16,547	0.13407	8.35
	P		-7,941	97	0.13407	NS		-12,701	471	0.13407	NS		-27,870	496	0.13407	NS
S	A		-54,639	62,504	0.13407	2.33		-59,298	68,575	0.13407	2.13		-61,346	60,618	0.13407	2.42
	P		3,793	1,592	0.13407	86.78		3,545	2,265	0.13407	61.01		3,347	2,290	0.13407	60.35
P	A	00583	-29,910	11,898	0.13407	11.98	00584	-21,478	10,556	0.13407	13.40	00585	-11,588	8,285	0.13407	16.92
	P		-25,600	432	0.13407	NS		-33,845	862	0.13407	NS		-36,337	531	0.13407	NS
S	A		-58,581	58,888	0.13407	2.48		-63,423	43,629	0.13407	3.39		-37,705	23,734	0.13407	6.05
	P		5,619	2,987	0.13407	46.17		9,689	3,227	0.13407	42.58		12,467	3,611	0.13407	37.95
P	A	00586	-24,449	6,157	0.13407	23.03	00587	35,359	5,523	0.13407	24.27	00588	31,139	32	0.13407	NS
	P		-5,921	145	0.13407	NS		13,666	172	0.13407	NS		22,424	4,317	0.13407	31.44
S	A		-45,704	12,231	0.13407	11.82		-	23,114	0.13407	6.61		0	0	0.13407	-
	P		26,873	3,635	0.13407	37.18		109,809	345	0.13407	NS		-81,519	4,397	0.13407	33.92
P	A	00589	0	0	0.13407	-	00590	0	0	0.13407	-	00591	0	0	0.13407	-
	P		15,481	7,666	0.13407	17.82		14,630	11,821	0.13407	11.57		18,152	14,441	0.13407	9.44
S	A		57,994	128	0.13407	NS		41,668	324	0.13407	NS		41,033	587	0.13407	NS
	P		-94,228	22,924	0.13407	6.58		-95,235	36,022	0.13407	4.19		-96,033	41,724	0.13407	3.62
P	A	00592	0	0	0.13407	-	00593	0	0	0.13407	-	00594	0	0	0.13407	-
	P		12,701	12,785	0.13407	10.72		6,019	11,605	0.13407	11.88		-7,079	4,231	0.13407	32.98
S	A		32,695	658	0.13407	NS		23,804	271	0.13407	NS		0	0	0.13407	-
	P		-	39,136	0.13407	3.88		-	33,157	0.13407	4.63		-	17,939	0.13407	8.58
			101,521					116,663					118,155			
P	A	00595	-11,222	2,553	0.13407	54.87	00596	-26,749	5,932	0.13407	23.95	00597	-47,988	16,898	0.13407	8.57
	P		4,845	892	0.13407	NS		5,570	684	0.13407	NS		13,120	804	0.13407	NS
S	A		-	5,341	0.13407	29.06		-	37,039	0.13407	4.23		-	80,579	0.13407	1.95
	P		128,790	942	0.13407	NS		139,126	1,716	0.13407	80.28		141,802	2,727	0.13407	50.58
P	A	00844	-67,819	4,215	0.13407	34.97	00845	66,318	15,662	0.13407	8.30	00846	40,578	38,415	0.13407	3.47
	P		92,071	7,586	0.13407	16.70		27,066	313	0.13407	NS		0	0	0.13407	-
S	A		-8,400	1,229	0.13407	NS		-2,394	6,829	0.13407	20.35		-2,081	8,268	0.13407	16.80
	P		-803	1,985	0.13407	69.90		4,191	15	0.13407	NS		0	0	0.13407	-
P	A	00847	13,058	53,885	0.13407	2.54	00848	-9,897	72,819	0.13407	1.92	00849	-19,857	83,363	0.13407	1.69



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-14,118	16,042	0.13407	8.76		-15,431	22,096	0.13407	6.36		-3,090	16,310	0.13407	8.53
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	00850	-31,414	80,341	0.13407	1.78	00851	-25,647	71,700	0.13407	1.98	00852	-15,036	61,212	0.13407	2.30
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-22,986	23,720	0.13407	5.97		-20,784	21,149	0.13407	6.68		-12,677	12,766	0.13407	10.99
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	00853	-8,860	40,573	0.13407	3.45	00854	-40,928	14,929	0.13407	9.64	02383	-49,883	6,454	0.13407	22.48
	P		0	0	0.13407	-		6,969	555	0.13407	NS		43	162	0.13407	NS
S	A		-18,317	13,850	0.13407	10.18		-16,991	4,909	0.13407	28.69		-24,852	3,740	0.13407	37.93
	P		0	0	0.13407	-		297	165	0.13407	NS		8,050	509	0.13407	NS
P	A	02384	76,439	6,559	0.13407	19.63	02385	-71,975	20,168	0.13407	7.33	02386	3,912	2,609	0.13407	52.95
	P		40,029	537	0.13407	NS		13,262	505	0.13407	NS		11,997	519	0.13407	NS
S	A		-64,330	38,475	0.13407	3.82		-	106,500	0.13407	1.48		-39,082	4,150	0.13407	34.62
	P		0	0	0.13407	-		150,174								
			4,383	2,901	0.13407	47.60		4,383	2,901	0.13407	47.60		6,269	369	0.13407	NS
P	A	02387	-66,342	2,552	0.13407	57.68	02388	-53,518	528	0.13407	NS	02389	11,472	197	0.13407	NS
	P		21,114	637	0.13407	NS		-639	4,016	0.13407	34.54		-28,863	1,749	0.13407	81.40
S	A		-35,605	4,342	0.13407	32.99		-78,398	15,925	0.13407	9.34		-	33,894	0.13407	4.55
	P		0	0	0.13407	-		8,111	705	0.13407	NS		121,902	1,275	0.13407	NS
P	A	02390	-44,726	2,355	0.13407	61.32	02391	-41,310	8,193	0.13407	17.57	02392	-50,727	9,074	0.13407	16.00
	P		-15,176	350	0.13407	NS		-5,193	544	0.13407	NS		8,602	549	0.13407	NS
S	A		-	49,614	0.13407	3.18		-	57,177	0.13407	2.78		-	59,363	0.13407	2.65
	P		150,193					158,846					143,359			
			5,641	1,541	0.13407	89.50		7,260	1,693	0.13407	81.34		7,648	2,049	0.13407	67.18
P	A	02393	-80,724	2,666	0.13407	55.91	02394	-60,437	703	0.13407	NS	02395	0	0	0.13407	-
	P		23,086	2,872	0.13407	47.23		4,343	15,830	0.13407	8.72		-5,597	15,690	0.13407	8.88
S	A		4,430	857	0.13407	NS		8,819	293	0.13407	NS		0	0	0.13407	-
	P		-52,700	5,867	0.13407	24.79		-91,631	8,850	0.13407	17.00		-	6,974	0.13407	22.08
													119,209			
P	A	02396	0	0	0.13407	-	02397	0	0	0.13407	-	02398	-8,284	28,857	0.13407	4.84
	P		-11,255	10,212	0.13407	13.72		-22,885	4,826	0.13407	29.34		0	0	0.13407	-
S	A		-10,973	23	0.13407	NS		-	2,027	0.13407	77.41		-26,881	2,147	0.13407	66.19
	P		-	2,952	0.13407	52.85		142,016					-284	57	0.13407	NS
			135,056					14,732	913	0.13407	NS					
P	A	02399	-73,815	1,983	0.13407	74.72	02400	-58,312	506	0.13407	NS	02401	0	0	0.13407	-
	P		3,563	16,076	0.13407	8.60		5,154	27,283	0.13407	5.06		4,894	25,606	0.13407	5.39
S	A		5,839	1,155	0.13407	NS		11,477	721	0.13407	NS		14,217	301	0.13407	NS
	P		-62,688	18,170	0.13407	8.08		-91,275	29,534	0.13407	5.09		-	34,307	0.13407	4.46
													111,998			
P	A	02402	0	0	0.13407	-	02403	0	0	0.13407	-	02404	-73,343	5,501	0.13407	26.92
	P		4,194	19,430	0.13407	7.11		2,402	12,417	0.13407	11.14		0	0	0.13407	-
S	A		13,213	72	0.13407	NS		14,018	20	0.13407	NS		-2,824	1,225	0.13407	NS
	P		-	33,802	0.13407	4.56		-	29,242	0.13407	5.26		-28,838	10,677	0.13407	13.33
			120,751					118,776								
P	A	02405	-67,485	1,287	0.13407	NS	02406	-42,399	127	0.13407	NS	02407	0	0	0.13407	-
	P		789	27,061	0.13407	5.12		7,563	32,856	0.13407	4.19		10,403	28,961	0.13407	4.74
S	A		9,553	1,138	0.13407	NS		14,532	802	0.13407	NS		18,482	494	0.13407	NS
	P		-66,689	31,052	0.13407	4.74		-87,908	43,393	0.13407	3.46		-	48,068	0.13407	3.15
													100,870			
P	A	02408	0	0	0.13407	-	02409	-32,572	36,260	0.13407	3.94	02410	-75,169	1,972	0.13407	75.22
	P		12,681	21,856	0.13407	6.27		0	0	0.13407	-		-8,189	15,940	0.13407	8.76
S	A		23,348	358	0.13407	NS		-23,004	3,382	0.13407	41.87		6,858	1,270	0.13407	NS
	P		-	46,432	0.13407	3.28		0	0	0.13407	-		-48,090	21,344	0.13407	6.79
			105,088													
P	A	02411	-56,577	493	0.13407	NS	02412	0	0	0.13407	-	02413	0	0	0.13407	-
	P		3,683	30,312	0.13407	4.56		9,890	30,413	0.13407	4.52		13,063	25,075	0.13407	5.46
S	A		12,362	875	0.13407	NS		15,972	520	0.13407	NS		22,590	335	0.13407	NS
	P		-68,172	37,022	0.13407	3.98		-81,856	45,204	0.13407	3.30		-88,051	46,669	0.13407	3.21
P	A	02414	0	0	0.13407	-	02415	-74,133	2,997	0.13407	49.45	02416	-59,237	661	0.13407	NS
	P		17,200	18,110	0.13407	7.53		0	0	0.13407	-		-1,450	19,578	0.13407	7.09
S	A		39,577	389	0.13407	NS		7,273	964	0.13407	NS		10,251	468	0.13407	NS
	P		-92,858	42,716	0.13407	3.53		-31,394	8,676	0.13407	16.45		-55,094	21,504	0.13407	6.78
P	A	02417	0	0	0.13407	-	02418	0	0	0.13407	-	02419	0	0	0.13407	-
	P		6,539	23,330	0.13407	5.91		12,037	20,374	0.13407	6.73		17,738	15,462	0.13407	8.82
S	A		9,033	77	0.13407	NS		0	0	0.13407	-		0	0	0.13407	-
	P		-68,467	28,156	0.13407	5.24		-72,946	29,795	0.13407	4.97		-75,642	27,793	0.13407	5.34
P	A	02420	-38,481	9,957	0.13407	14.42	02421	-54,014	491	0.13407	NS	02422	0	0	0.13407	-
	P		0	0	0.13407	-		-8,823	6,369	0.13407	21.95		-4,159	9,617	0.13407	14.47
S	A		-22,370	2,161	0.13407	65.49		-5,751	327	0.13407	NS		-63,465	2,935	0.13407	50.03
	P		2,752	14	0.13407	NS		10,234	706	0.13407	NS		6,979	1,091	0.13407	NS
P	A	02423	0	0	0.13407	-	02424	0	0	0.13407	-	02425	40,137	118	0.13407	NS
	P		7,280	8,855	0.13407	15.55		18,362	6,398	0.13407	21.30		32,736	3,848	0.13407	34.93
S	A		-66,718	5,883	0.13407	25.03		-66,662	7,042	0.13407	20.91		-63,399	8,762	0.13407	16.76
	P		6,842	1,048	0.13407	NS		13,424	800	0.13407	NS		35,263	476	0.13407	NS
Piano Fondo Vasca			Parete P4-P5				Parete P4-P5				Parete P4-P5					
P	A	00001	138,304	1,446	0.13407	83.48	00002	1,750	1,416	0.13407	97.75	00004	13,853	898	0.13407	NS
	P		77,688	27,789	0.13407	4.63		-21,704	1,245	0.13407	NS		-90,315	26,345	0.13407	5.70



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
S	A		0	0	0.13407	-		6,299	708	0.13407	NS		1,532	3,633	0.13407	38.11
	P		-59,893	69,135	0.13407	2.12		-50,350	1,863	0.13407	77.91		-	136,187	0.13407	1.17
													158,506			
P	A	00050	-48,745	7,960	0.13407	18.21	00421	-8,438	167	0.13407	NS	00422	-35,639	593	0.13407	NS
	P		0	0	0.13407	-		-49,823	7,125	0.13407	20.36		14,005	11,329	0.13407	12.08
S	A		-10,858	5,389	0.13407	25.99		22,085	3,235	0.13407	41.97		9,935	3,202	0.13407	42.90
	P		0	0	0.13407	-		-60,085	22,091	0.13407	6.63		-52,362	35,227	0.13407	4.13
P	A	00423	-38,261	682	0.13407	NS	00424	-32,224	543	0.13407	NS	00425	-37,982	601	0.13407	NS
	P		-39,147	19,177	0.13407	7.49		-87,490	22,417	0.13407	6.69		-78,712	28,688	0.13407	5.19
S	A		7,817	3,149	0.13407	43.71		4,950	3,237	0.13407	42.63		3,201	2,509	0.13407	55.09
	P		-98,841	83,435	0.13407	1.81		-	110,369	0.13407	1.42		-	109,934	0.13407	1.44
								136,251					149,613			
P	A	00426	-30,197	425	0.13407	NS	00427	-29,829	638	0.13407	NS	00428	-1,884	488	0.13407	NS
	P		-	29,153	0.13407	5.22		-76,987	36,753	0.13407	4.04		-84,787	34,101	0.13407	4.39
S	A		3,139	2,823	0.13407	48.97		2,802	2,516	0.13407	54.96		2,249	2,552	0.13407	54.21
	P		-	150,421	0.13407	1.06		-	135,872	0.13407	1.18		-	130,098	0.13407	1.22
			159,174					166,098					153,112			
P	A	00429	8,206	447	0.13407	NS	00557	-6,247	64	0.13407	NS	00558	-37,947	772	0.13407	NS
	P		-92,972	33,271	0.13407	4.53		-32,787	6,610	0.13407	21.62		-13,732	7,670	0.13407	18.31
S	A		5,232	3,084	0.13407	44.74		27,522	3,694	0.13407	36.57		12,743	3,829	0.13407	35.78
	P		-	147,848	0.13407	1.07		-40,198	13,863	0.13407	10.38		-43,465	21,540	0.13407	6.70
			154,858													
P	A	00559	-36,123	591	0.13407	NS	00560	-28,626	535	0.13407	NS	00561	-31,206	578	0.13407	NS
	P		-25,269	10,126	0.13407	14.01		-25,120	12,949	0.13407	10.96		-4,384	15,066	0.13407	9.24
S	A		10,073	2,970	0.13407	46.24		5,733	3,490	0.13407	39.51		3,438	2,309	0.13407	59.85
	P		-56,850	42,924	0.13407	3.40		-62,957	64,825	0.13407	2.26		-64,520	57,292	0.13407	2.57
P	A	00562	-17,293	152	0.13407	NS	00563	-13,895	431	0.13407	NS	00564	6,472	63	0.13407	NS
	P		-5,108	15,104	0.13407	9.22		21,560	17,034	0.13407	7.98		48,195	14,380	0.13407	9.21
S	A		3,868	2,290	0.13407	60.32		3,565	1,848	0.13407	74.77		8,705	1,333	0.13407	NS
	P		-58,600	75,661	0.13407	1.93		-55,523	63,925	0.13407	2.28		-41,607	55,535	0.13407	2.59
P	A	00565	0	0	0.13407	-	00598	13,119	806	0.13407	NS	00599	5,390	686	0.13407	NS
	P		100,686	9,930	0.13407	12.65		-48,392	17,309	0.13407	8.37		-26,802	5,968	0.13407	23.81
S	A		39,002	1,100	0.13407	NS		5,502	2,698	0.13407	51.12		6,710	1,690	0.13407	81.52
	P		-24,560	60,915	0.13407	2.33		-	80,536	0.13407	1.95		-	36,894	0.13407	4.24
								140,854					139,458			
P	A	00600	4,504	895	0.13407	NS	00601	-8,154	4,287	0.13407	32.59	00602	4,352	11,632	0.13407	11.87
	P		-11,752	2,583	0.13407	54.26		0	0	0.13407	-		0	0	0.13407	-
S	A		12,884	933	0.13407	NS		-	18,024	0.13407	8.53		-	33,197	0.13407	4.63
	P		-	5,216	0.13407	29.76		117,528	0	0.13407	-		116,294	260	0.13407	NS
			129,045					0					23,707			
P	A	00603	10,722	12,796	0.13407	10.73	00604	15,846	14,452	0.13407	9.45	00605	10,379	11,806	0.13407	11.63
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-	39,180	0.13407	3.87		-93,805	41,735	0.13407	3.61		-93,468	36,011	0.13407	4.18
	P		101,010					41,650	556	0.13407	NS		42,033	284	0.13407	NS
P	A	00606	13,020	7,558	0.13407	18.12	00607	17,387	4,324	0.13407	31.54	00608	7,512	163	0.13407	NS
	P		0	0	0.13407	-		29,520	44	0.13407	NS		27,748	5,684	0.13407	23.76
S	A		-89,112	22,883	0.13407	6.56		-74,105	4,207	0.13407	35.23		75,753	273	0.13407	NS
	P		59,834	79	0.13407	NS		0	0	0.13407	-		-95,887	23,641	0.13407	6.39
P	A	00833	88,978	6,838	0.13407	18.59	00834	24,592	205	0.13407	NS	00835	0	0	0.13407	-
	P		-68,161	4,240	0.13407	34.77		64,395	15,706	0.13407	8.30		38,811	38,420	0.13407	3.48
S	A		1,164	1,876	0.13407	73.82		0	0	0.13407	-		0	0	0.13407	-
	P		-8,621	1,235	0.13407	NS		-2,606	6,986	0.13407	19.89		-2,715	8,276	0.13407	16.79
P	A	00836	0	0	0.13407	-	00837	0	0	0.13407	-	00838	0	0	0.13407	-
	P		11,448	53,916	0.13407	2.54		-11,950	72,892	0.13407	1.92		-21,782	83,470	0.13407	1.69
S	A		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
	P		-14,157	16,060	0.13407	8.75		-16,287	22,129	0.13407	6.36		-7,361	16,580	0.13407	8.42
P	A	00839	0	0	0.13407	-	00840	0	0	0.13407	-	00841	0	0	0.13407	-
	P		-33,171	80,455	0.13407	1.78		-28,149	71,871	0.13407	1.98		-17,322	61,475	0.13407	2.29
S	A		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
	P		-23,177	23,765	0.13407	5.96		-21,607	21,232	0.13407	6.66		-13,536	12,833	0.13407	10.94
P	A	00842	0	0	0.13407	-	00843	4,485	410	0.13407	NS	02204	-953	95	0.13407	NS
	P		-11,029	40,954	0.13407	3.42		-45,918	15,350	0.13407	9.42		-50,876	6,744	0.13407	21.53
S	A		0	0	0.13407	-		348	127	0.13407	NS		8,171	510	0.13407	NS
	P		-18,818	14,010	0.13407	10.07		-14,967	4,998	0.13407	28.13		-21,872	4,109	0.13407	34.43
P	A	02205	84,277	494	0.13407	NS	02206	13,495	504	0.13407	NS	02207	12,007	473	0.13407	NS
	P		60,619	6,475	0.13407	20.20		-71,235	20,456	0.13407	7.23		4,310	2,868	0.13407	48.15
S	A		0	0	0.13407	-		4,400	2,890	0.13407	47.78		6,254	370	0.13407	NS
	P		-55,186	39,836	0.13407	3.66		-	107,788	0.13407	1.47		-35,367	4,971	0.13407	28.81
								150,044								
P	A	02208	18,104	565	0.13407	NS	02209	-7,608	4,124	0.13407	33.86	02210	-25,900	1,488	0.13407	95.42
	P		4,843	2,137	0.13407	64.58		-53,995	553	0.13407	NS		10,411	209	0.13407	NS
S	A		0	0	0.13407	-		7,968	690	0.13407	NS		6,073	1,263	0.13407	NS
	P		-39,786	3,473	0.13407	41.40		-74,762	15,889	0						



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
	P		[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	P		-	48,762	0.13407	3.23		-	56,624	0.13407	2.80		-	58,141	0.13407	2.70
			147,332					153,931					143,193			
P	A	02214	21,864	2,780	0.13407	48.85	02215	2,159	15,755	0.13407	8.78	02216	-7,083	15,559	0.13407	8.97
	P		-81,575	2,707	0.13407	55.10		-61,244	720	0.13407	NS		0	0	0.13407	-
S	A		-52,553	5,785	0.13407	25.14		-92,061	8,817	0.13407	17.07		-	7,004	0.13407	22.00
	P		4,337	867	0.13407	NS		8,736	305	0.13407	NS		119,691	0	0.13407	-
P	A	02217	-11,591	10,238	0.13407	13.69	02218	-24,114	4,960	0.13407	28.58	02219	0	0	0.13407	-
	P		0	0	0.13407	-		0	0	0.13407	-		-9,974	28,939	0.13407	4.84
S	A		-	2,963	0.13407	52.66		14,612	905	0.13407	NS		-460	35	0.13407	NS
	P		135,107					-					-27,124	2,176	0.13407	65.33
	P		-10,930	14	0.13407	NS		141,090	2,004	0.13407	78.24					
P	A	02220	1,812	16,027	0.13407	8.64	02221	3,639	27,207	0.13407	5.08	02222	3,497	25,547	0.13407	5.41
	P		-75,038	2,021	0.13407	73.39		-59,543	519	0.13407	NS		0	0	0.13407	-
S	A		-62,872	18,131	0.13407	8.09		-91,717	29,519	0.13407	5.10		-	34,316	0.13407	4.46
	P		5,742	1,170	0.13407	NS		11,440	735	0.13407	NS		111,969	310	0.13407	NS
P	A	02223	2,661	19,527	0.13407	7.08	02224	1,369	12,429	0.13407	11.14	02225	0	0	0.13407	-
	P		0	0	0.13407	-		0	0	0.13407	-		-76,549	5,622	0.13407	26.42
S	A		-	33,780	0.13407	4.56		-	29,297	0.13407	5.25		-29,001	10,651	0.13407	13.37
	P		120,118					118,182					-3,005	1,255	0.13407	NS
	P		13,235	72	0.13407	NS		14,029	16	0.13407	NS		8,420	28,966	0.13407	4.75
P	A	02226	-1,083	27,020	0.13407	5.14	02227	5,727	32,811	0.13407	4.20	02228	0	0	0.13407	-
	P		-69,172	1,316	0.13407	NS		-43,233	133	0.13407	NS		0	0	0.13407	-
S	A		-68,531	31,189	0.13407	4.73		-87,879	43,374	0.13407	3.46		-	48,055	0.13407	3.15
	P		9,527	1,156	0.13407	NS		14,545	813	0.13407	NS		100,372	497	0.13407	NS
P	A	02229	10,524	21,880	0.13407	6.27	02230	0	0	0.13407	-	02231	-10,456	15,942	0.13407	8.78
	P		0	0	0.13407	-		-34,619	36,381	0.13407	3.93		-77,254	2,016	0.13407	73.71
S	A		-	46,436	0.13407	3.27		0	0	0.13407	-		-47,976	21,288	0.13407	6.80
	P		104,147					-23,292	3,437	0.13407	41.21		6,856	1,291	0.13407	NS
	P		23,413	349	0.13407	NS		-23,292	3,437	0.13407	41.21		6,856	1,291	0.13407	NS
P	A	02232	1,463	30,283	0.13407	4.57	02233	7,554	30,376	0.13407	4.53	02234	10,403	25,116	0.13407	5.47
	P		-58,779	506	0.13407	NS		0	0	0.13407	-		0	0	0.13407	-
S	A		-68,051	36,994	0.13407	3.99		-81,500	45,192	0.13407	3.30		-87,058	46,628	0.13407	3.21
	P		12,420	887	0.13407	NS		16,059	523	0.13407	NS		22,738	327	0.13407	NS
P	A	02235	13,964	18,101	0.13407	7.56	02236	0	0	0.13407	-	02237	-4,378	19,613	0.13407	7.10
	P		0	0	0.13407	-		-77,865	3,055	0.13407	48.67		-61,740	686	0.13407	NS
S	A		-90,933	42,709	0.13407	3.52		-31,310	8,628	0.13407	16.54		-54,589	21,480	0.13407	6.78
	P		39,982	359	0.13407	NS		7,261	987	0.13407	NS		10,302	473	0.13407	NS
P	A	02238	3,906	23,274	0.13407	5.94	02239	9,098	20,372	0.13407	6.75	02240	13,691	15,494	0.13407	8.83
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-68,219	28,174	0.13407	5.23		-72,443	29,770	0.13407	4.97		-73,196	27,705	0.13407	5.35
	P		9,123	76	0.13407	NS		0	0	0.13407	-		0	0	0.13407	-
P	A	02241	0	0	0.13407	-	02242	-8,783	6,694	0.13407	20.88	02243	-7,131	9,165	0.13407	15.23
	P		-40,041	10,202	0.13407	14.10		-56,178	520	0.13407	NS		0	0	0.13407	-
S	A		0	0	0.13407	-		10,051	691	0.13407	NS		6,992	1,070	0.13407	NS
	P		-21,304	1,809	0.13407	78.16		-5,630	288	0.13407	NS		-62,577	2,430	0.13407	60.38
P	A	02244	3,146	8,249	0.13407	16.76	02245	14,189	6,588	0.13407	20.77	02246	26,862	3,627	0.13407	37.27
	P		0	0	0.13407	-		0	0	0.13407	-		37,584	113	0.13407	NS
S	A		7,205	1,092	0.13407	NS		13,507	827	0.13407	NS		35,926	443	0.13407	NS
	P		-66,199	5,466	0.13407	26.93		-64,937	6,900	0.13407	21.31		-60,327	8,356	0.13407	17.52
Piano Fondo Vasca			Parete P1-P4				Parete P1-P4				Parete P1-P4					
P	A	00002	-54,286	17,816	0.20947	12.47	00003	-56,890	16,994	0.20947	13.10	00004	13,295	1,242	0.20947	NS
	P		-7,951	3,277	0.20947	65.99		-8,877	3,517	0.20947	61.52		-	32,838	0.20947	6.96
S	A		-11,089	8,416	0.20947	25.74		-9,851	7,751	0.20947	27.93		103,954	3,661	0.20947	58.85
	P		-3,067	227	0.20947	NS		3,747	385	0.20947	NS		-1,594	138,176	0.20947	1.68
P	A	00048	12,111	1,285	0.20947	NS	00421	-15,030	167	0.20947	NS	00422	-22,974	620	0.20947	NS
	P		-	31,566	0.20947	7.25		-18,255	7,840	0.20947	27.75		-18,223	10,573	0.20947	20.58
S	A		105,177					22,551	3,140	0.20947	67.62		12,909	3,927	0.20947	54.39
	P		-535	3,731	0.20947	57.71		-69,100	14,910	0.20947	15.03		-68,073	59,438	0.20947	3.77
	P		-	138,347	0.20947	1.68										
P	A	00423	-38,427	870	0.20947	NS	00424	-37,787	773	0.20947	NS	00425	-34,340	619	0.20947	NS
	P		-34,935	20,553	0.20947	10.69		-74,101	22,903	0.20947	9.81		-95,851	27,018	0.20947	8.42
S	A		6,097	3,166	0.20947	67.73		3,346	2,670	0.20947	80.45		2,111	3,009	0.20947	71.44
	P		-	63,353	0.20947	3.65		-	94,766	0.20947	2.45		-	136,567	0.20947	1.71
	P		127,106					132,388					143,330			
P	A	00426	-16,277	714	0.20947	NS	00427	-8,731	653	0.20947	NS	00428	-5,373	837	0.20947	NS
	P		-85,172	31,112	0.20947	7.27		-80,169	34,521	0.20947	6.53		-82,579	32,222	0.20947	7.01
S	A		1,403	2,529	0.20947	85.03		-1,679	2,744	0.20947	78.52		396	2,879	0.20947	74.74
	P		-	123,718	0.20947	1.90		-	146,907	0.20947	1.59		-	160,808	0.20947	1.44
	P		156,908					139,329					132,509			
P	A	00429	8,529	691	0.20947	NS	00430	7,440	556	0.20947	NS	00431	-25,695	6,666	0.20947	32.78
	P		-89,209	32,049	0.20947	7.07		-45,874	6,511	0.20947	33.96		0	0	0.20947	-
S	A		2,658	3,010	0.20947	71.39		-2,464	2,704	0.20947	79.72		-217	1,778	0.20947	NS
	P		-	138,802	0.20947	1.68		-	82,253	0.20947	2.82		-	40,390	0.20947	5.69



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N·m]	[cm²/cm]			[N]	[N·m]	[cm²/cm]			[N]	[N·m]	[cm²/cm]	
			140,513					128,576					113,666			
P	A	00432	-8,284	19,544	0.20947	11.07	00433	5,919	35,788	0.20947	5.99	00434	16,595	51,445	0.20947	4.14
	P		3,997	83	0.20947	NS		-4,572	430	0.20947	NS		-12,189	771	0.20947	NS
S	A		818	993	0.20947	NS		-	12,321	0.20947	18.55		-91,231	24,922	0.20947	9.11
	P	00435	-	12,475	0.20947	18.33	00436	103,686	0	0.20947	-	00437	3,181	399	0.20947	NS
			104,250					0	0							
P	A		22,498	61,779	0.20947	3.44		28,097	73,576	0.20947	2.88		31,550	86,286	0.20947	2.45
	P	00438	-16,385	1,171	0.20947	NS	00439	-22,030	1,541	0.20947	NS	00440	-27,179	1,876	0.20947	NS
S	A		-84,266	34,079	0.20947	6.63		-83,409	44,092	0.20947	5.12		-69,315	44,165	0.20947	5.08
	P		3,308	785	0.20947	NS		3,070	1,241	0.20947	NS		2,407	1,376	0.20947	NS
P	A	00438	34,658	90,571	0.20947	2.33	00439	35,478	99,536	0.20947	2.12	00440	35,843	109,044	0.20947	1.93
	P		-29,732	2,320	0.20947	94.42		-33,504	2,536	0.20947	86.57		-36,988	2,710	0.20947	81.18
S	A		-65,023	44,640	0.20947	5.01		-63,959	48,227	0.20947	4.63		-52,493	44,901	0.20947	4.94
	P	00441	1,797	1,453	0.20947	NS	00442	1,372	1,676	0.20947	NS	00443	-464	1,644	0.20947	NS
P	A		33,043	112,636	0.20947	1.87		35,757	118,621	0.20947	1.78		41,072	116,989	0.20947	1.79
	P		-39,110	3,020	0.20947	72.94		-40,388	3,350	0.20947	65.80		-41,083	3,601	0.20947	61.24
S	A	00444	-52,290	44,520	0.20947	4.99	00445	-46,883	42,388	0.20947	5.22	00446	-45,544	42,416	0.20947	5.21
	P		-1,371	1,631	0.20947	NS		-1,443	1,658	0.20947	NS		-2,484	1,677	0.20947	NS
P	A		35,493	123,377	0.20947	1.71		37,795	123,465	0.20947	1.70		43,086	120,933	0.20947	1.73
	P	00447	-43,195	3,424	0.20947	64.48	00448	-43,674	3,625	0.20947	60.92	00449	-43,584	3,821	0.20947	57.80
S	A		-42,352	40,577	0.20947	5.44		-41,378	39,580	0.20947	5.57		-40,888	39,248	0.20947	5.62
	P		-2,996	1,662	0.20947	NS		-2,932	1,639	0.20947	NS		-3,256	1,650	0.20947	NS
P	A	00447	36,989	125,710	0.20947	1.67	00448	38,503	124,173	0.20947	1.69	00449	43,411	120,105	0.20947	1.75
	P		-44,739	3,586	0.20947	61.63		-44,513	3,636	0.20947	60.77		-43,459	3,751	0.20947	58.87
S	A		-39,110	38,999	0.20947	5.65		-41,357	39,664	0.20947	5.56		-41,932	39,537	0.20947	5.58
	P	00450	-3,341	1,668	0.20947	NS	00451	-2,833	1,683	0.20947	NS	00452	-2,798	1,660	0.20947	NS
P	A		37,172	122,901	0.20947	1.71		37,726	119,435	0.20947	1.76		41,578	113,893	0.20947	1.84
	P		-43,506	3,476	0.20947	63.53		-42,345	3,374	0.20947	65.41		-40,164	3,401	0.20947	64.81
S	A	00453	-41,379	40,186	0.20947	5.49	00454	-46,609	42,702	0.20947	5.18	00455	-48,308	42,930	0.20947	5.16
	P		-2,722	1,676	0.20947	NS		-1,748	1,739	0.20947	NS		-1,316	1,688	0.20947	NS
P	A		35,888	113,936	0.20947	1.85		35,592	107,604	0.20947	1.96		37,655	100,086	0.20947	2.10
	P	00456	-39,285	3,069	0.20947	71.78	00457	-37,166	2,811	0.20947	78.27	00458	-33,848	2,714	0.20947	80.91
S	A		-49,223	43,300	0.20947	5.12		-58,235	46,916	0.20947	4.75		-60,797	46,802	0.20947	4.77
	P		-918	1,659	0.20947	NS		299	1,716	0.20947	NS		1,085	1,618	0.20947	NS
P	A	00456	32,268	96,214	0.20947	2.19	00457	30,395	85,802	0.20947	2.46	00458	28,939	75,442	0.20947	2.80
	P		-31,718	2,316	0.20947	94.70		-28,056	1,937	0.20947	NS		-22,881	1,679	0.20947	NS
S	A		-63,343	44,600	0.20947	5.01		-76,488	46,375	0.20947	4.85		-78,753	43,108	0.20947	5.23
	P	00459	1,759	1,492	0.20947	NS	00460	2,410	1,469	0.20947	NS	00461	2,954	1,217	0.20947	NS
P	A		21,766	66,485	0.20947	3.20		15,609	51,734	0.20947	4.12		7,433	37,386	0.20947	5.73
	P		-19,321	1,232	0.20947	NS		-13,514	846	0.20947	NS		-4,644	466	0.20947	NS
S	A	00462	-82,956	33,882	0.20947	6.67	00463	-98,195	26,517	0.20947	8.59	00464	-97,701	12,623	0.20947	18.05
	P		3,300	820	0.20947	NS		1,957	424	0.20947	NS		0	0	0.20947	-
P	A		-7,394	23,172	0.20947	9.33		-23,970	8,212	0.20947	26.59		11,953	581	0.20947	NS
	P	00465	-23,235	56	0.20947	NS	00466	0	0	0.20947	-	00467	-43,965	8,700	0.20947	25.39
S	A		356	927	0.20947	NS		-1,277	1,859	0.20947	NS		251	2,723	0.20947	79.03
	P		-	11,361	0.20947	20.13		-	41,859	0.20947	5.50		-	82,384	0.20947	2.81
P	A	00465	104,688				00466	115,460				00467	126,498			
P	A		5,888	587	0.20947	NS		-1,491	793	0.20947	NS		-11,960	762	0.20947	NS
	P	00468	-82,095	30,519	0.20947	7.40	00469	-75,006	35,235	0.20947	6.38	00470	-81,397	35,745	0.20947	6.31
S	A		1,169	3,033	0.20947	70.91		-1,791	2,847	0.20947	75.68		1,155	2,667	0.20947	80.65
	P		-	141,461	0.20947	1.64		-	143,396	0.20947	1.61		-	140,343	0.20947	1.67
P	A	00468	133,659				00469	126,266				00470	149,748			
P	A		-15,638	690	0.20947	NS		-36,915	719	0.20947	NS		-34,407	730	0.20947	NS
	P	00471	-	27,632	0.20947	8.32	00472	-66,466	30,539	0.20947	7.33	00473	-90,375	21,346	0.20947	10.63
S	A		1,476	2,695	0.20947	79.79		1,668	2,661	0.20947	80.80		3,506	2,962	0.20947	72.51
	P		-	135,748	0.20947	1.73		-	119,405	0.20947	1.96		-	103,441	0.20947	2.23
P	A	00471	150,093				00472	142,737				00473	123,900			
P	A		-36,574	683	0.20947	NS		-36,074	813	0.20947	NS		-9,614	512	0.20947	NS
	P	00798	-54,417	17,279	0.20947	12.86	00799	410	14,880	0.20947	14.46	00800	-23,507	10,086	0.20947	21.64
S	A		5,870	2,932	0.20947	73.15		11,350	3,224	0.20947	66.31		21,167	3,246	0.20947	65.47
	P		-	75,361	0.20947	3.06		-74,619	38,424	0.20947	5.85		-74,440	19,145	0.20947	11.74
P	A	00798	118,319				00799					00800				
P	A		16,986	930	0.20947	NS		0	0	0.20947	-		0	0	0.20947	-
	P	00801	4,802	5,859	0.20947	36.63	00802	68,533	40,330	0.20947	5.12	00803	32,961	82,505	0.20947	2.56
S	A		843	52	0.20947	NS		0	0	0.20947	-		0	0	0.20947	-
	P		-4,665	4,700	0.20947	45.92		-15,463	5,819	0.20947	37.33		953	17,473	0.20947	12.15
P	A	00801	0	0	0.20947	-	00802	0	0	0.20947	-	00803	0	0	0.20947	-
	P		-31,091	103,799	0.20947	2.11		177	142,518	0.20947	1.51		-28,980	181,689	0.20947	1.21
S	A		0	0	0.20947	-		0	0	0.20947	-		0	0	0.20947	-
	P	00804	928	30,119	0.20947	7.14	00805	-15,053	31,918	0.20947	6.80	00806	-10,286	37,051	0.20947	5.77
P	A		-29,077	143	0.20947	NS		-42,270	688	0.20947	NS		-46,188	1,265	0.20947	NS
	P		-94,383	187,492	0.20947	1.21		-47,385	210,530	0.41893	1.98		-80,573	240,048	0.41893	1.75
S	A	00807	-7,988	97	0.20947	NS	00808	-6,564	96	0.20947	NS	00809	-8,677	255	0.20947	NS
	P		-6,311	46,271	0.20947	4.67		-23,259	51,663	0.20947	4.22		-17,158	48,761	0.20947	4.46
P	A		-43,673	1,387	0.20947	NS		-42,477	1,751	0.20947	NS		-51			



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	P		-15,077	53,256	0.20947	4.08		-24,369	61,755	0.20947	3.54		-7,432	65,947	0.20947	3.28
P	A	00810	-52,116	2,356	0.20947	94.30	00811	-47,909	2,499	0.20947	88.68	00812	-50,159	2,397	0.20947	92.58
	P		-63,568	266,461	0.41893	1.57		-94,500	279,936	0.41893	1.50		-96,443	265,131	0.41893	1.59
S	A		-13,993	491	0.20947	NS		-12,997	531	0.20947	NS		-12,174	560	0.20947	NS
	P		-24,928	55,383	0.20947	3.94		-11,607	57,091	0.20947	3.80		-13,839	69,485	0.20947	3.12
P	A	00813	-49,259	2,665	0.20947	83.23	00814	-64,959	3,008	0.20947	74.41	00815	-50,771	2,503	0.20947	88.69
	P		-80,935	254,629	0.41893	1.65		-93,331	276,983	0.41893	1.52		-99,986	249,572	0.41893	1.69
S	A		-13,414	598	0.20947	NS		-13,706	609	0.20947	NS		-10,698	555	0.20947	NS
	P		-19,265	59,354	0.20947	3.67		-15,370	59,394	0.20947	3.66		-16,046	68,204	0.20947	3.19
P	A	00816	-62,011	2,833	0.20947	78.88	00817	-65,415	2,983	0.20947	75.06	00818	-51,108	2,409	0.20947	92.17
	P		-90,483	254,818	0.41893	1.65		-90,857	278,171	0.41893	1.51		-96,766	268,218	0.41893	1.57
S	A		-13,024	633	0.20947	NS		-13,908	604	0.20947	NS		-10,356	509	0.20947	NS
	P		-16,173	61,554	0.20947	3.53		-16,746	59,640	0.20947	3.65		-19,254	64,893	0.20947	3.35
P	A	00819	-44,217	2,408	0.20947	91.84	00820	-48,853	2,496	0.20947	88.84	00821	-52,699	2,114	0.20947	NS
	P		-93,695	263,353	0.41893	1.60		-82,958	268,616	0.41893	1.56		-85,555	255,209	0.41893	1.64
S	A		-12,071	584	0.20947	NS		-14,254	525	0.20947	NS		-6,979	426	0.20947	NS
	P		-10,526	62,206	0.20947	3.48		-18,569	57,344	0.20947	3.80		-17,867	59,594	0.20947	3.65
P	A	00822	-41,771	1,782	0.20947	NS	00823	-48,586	1,600	0.20947	NS	00824	-53,524	1,278	0.20947	NS
	P		-89,595	249,127	0.41893	1.69		-82,198	258,246	0.41893	1.62		-45,673	229,332	0.41893	1.82
S	A		-12,672	466	0.20947	NS		-9,725	324	0.20947	NS		-7,763	214	0.20947	NS
	P		-4,285	60,852	0.20947	3.55		-15,158	52,354	0.20947	4.15		-19,315	50,154	0.20947	4.34
P	A	00825	-41,129	714	0.20947	NS	00826	-34,742	228	0.20947	NS	00827	-39,166	21	0.20947	NS
	P		-54,123	210,475	0.41893	1.98		-48,796	206,605	0.41893	2.02		-3,663	174,849	0.20947	1.23
S	A		-9,872	233	0.20947	NS		-6,381	45	0.20947	NS		0	0	0.20947	-
	P		-1,651	55,018	0.20947	3.92		-6,743	42,266	0.20947	5.11		-15,487	34,971	0.20947	6.21
P	A	00828	0	0	0.20947	-	00829	0	0	0.20947	-	00830	0	0	0.20947	-
	P		-10,640	144,701	0.20947	1.50		2,825	117,778	0.20947	1.82		68,867	84,414	0.20947	2.44
S	A		0	0	0.20947	-		0	0	0.20947	-		0	0	0.20947	-
	P		4,397	41,443	0.20947	5.18		7,447	24,213	0.20947	8.74		-15,471	13,508	0.20947	15.90
P	A	00831	0	0	0.20947	-	00832	19,103	1,115	0.20947	NS	01670	865	25	0.20947	NS
	P		65,063	41,815	0.20947	4.95		11,682	3,943	0.20947	54.20		-26,100	5,614	0.20947	38.94
S	A		0	0	0.20947	-		1,397	326	0.20947	NS		5,923	192	0.20947	NS
	P		-2,029	14,822	0.20947	14.54		-9,840	1,601	0.20947	NS		-34,989	8,798	0.20947	24.98
P	A	01671	9,793	581	0.20947	NS	01672	11,682	486	0.20947	NS	01673	0	0	0.20947	-
	P		-68,696	19,037	0.20947	11.77		-73,105	16,441	0.20947	13.66		-21,464	6,503	0.20947	33.52
S	A		732	2,817	0.20947	76.37		179	2,860	0.20947	75.25		6,919	241	0.20947	NS
	P		-	108,255	0.20947	2.14		-	107,505	0.20947	2.16		-41,278	5,434	0.20947	40.59
			131,859					128,614								
P	A	01674	0	0	0.20947	-	01675	-15,887	32	0.20947	NS	01676	-47,635	639	0.20947	NS
	P		24,804	13,482	0.20947	15.73		-3,841	4,154	0.20947	51.93		6,514	335	0.20947	NS
S	A		0	0	0.20947	-		6,386	753	0.20947	NS		2,942	1,385	0.20947	NS
	P		-39,528	7,425	0.20947	29.67		-91,410	19,709	0.20947	11.52		-	39,264	0.20947	5.89
													125,570			
P	A	01677	-44,606	2,541	0.20947	86.96	01678	-54,802	655	0.20947	NS	01679	5,217	331	0.20947	NS
	P		7,423	10	0.20947	NS		6,513	134	0.20947	NS		-69,575	497	0.20947	NS
S	A		705	1,633	0.20947	NS		298	1,787	0.20947	NS		629	2,181	0.20947	98.65
	P		-	56,002	0.20947	4.17		-	64,388	0.20947	3.62		-	66,159	0.20947	3.50
			140,428					139,342					127,627			
P	A	01680	0	0	0.20947	-	01681	2,754	7,459	0.20947	28.81	01682	-6,707	21,128	0.20947	10.23
	P		12,976	21,070	0.20947	10.14		-50,488	345	0.20947	NS		0	0	0.20947	-
S	A		0	0	0.20947	-		680	134	0.20947	NS		272	516	0.20947	NS
	P		-59,697	3,133	0.20947	69.96		-10,024	477	0.20947	NS		-	3,516	0.20947	65.52
													117,766			
P	A	01683	-11,624	25,663	0.20947	8.45	01684	-13,198	24,675	0.20947	8.79	01685	0	0	0.20947	-
	P		0	0	0.20947	-		0	0	0.20947	-		-15,336	73,337	0.20947	2.96
S	A		-410	792	0.20947	NS		35	989	0.20947	NS		0	0	0.20947	-
	P		-	7,936	0.20947	29.16		-	11,479	0.20947	20.09		-31,940	12,657	0.20947	17.04
			125,816					119,754								
P	A	01686	0	0	0.20947	-	01687	4,234	27,307	0.20947	7.86	01688	5,144	44,473	0.20947	4.82
	P		2,881	7,927	0.20947	27.11		-49,961	404	0.20947	NS		-51,005	189	0.20947	NS
S	A		-66,765	6,353	0.20947	34.68		-94,301	17,111	0.20947	13.11		-	21,439	0.20947	10.69
	P		-497	706	0.20947	NS		1,300	392	0.20947	NS		108,986	833	0.20947	NS
P	A	01689	6,200	49,801	0.20947	4.31	01690	7,459	45,340	0.20947	4.73	01691	0	0	0.20947	-
	P		-40,654	219	0.20947	NS		-8,972	370	0.20947	NS		-21,678	54,559	0.20947	4.00
S	A		-	21,495	0.20947	10.68		-	18,524	0.20947	12.34		0	0	0.20947	-
	P		111,412	0	0.20947	-		103,808	0	0.20947	-		-43,465	4,425	0.20947	49.04
P	A	01692	-3,225	13,545	0.20947	15.92	01693	6,142	50,400	0.20947	4.25	01694	12,876	67,247	0.20947	3.18
	P		-58,346	817	0.20947	NS		-61,487	516	0.20947	NS		-51,901	481	0.20947	NS
S	A		-67,284	17,246	0.20947	12.80		-87,297	30,777	0.20947	7.36		-96,647	37,378	0.20947	6.09
	P		-2,236	665	0.20947	NS		40	581	0.20947	NS		964	526	0.20947	NS
P	A	01695	18,356	69,957	0.20947	3.04	01696	-28,2								



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
P	A	01701	27,182	83,501	0.20947	2.54	01702	-42,841	557	0.20947	NS	01703	-19,816	10,173	0.20947	21.41
P	P		-25,028	1,278	0.20947	NS		-44,544	84,745	0.20947	2.61		-3,224	673	0.20947	NS
S	A		-81,330	46,182	0.20947	4.89		-5,601	26	0.20947	NS		-45,960	15,632	0.20947	13.98
P	P		2,659	1,068	0.20947	NS		-31,663	9,922	0.20947	21.80		-6,832	564	0.20947	NS
P	A	01704	-1,214	65,810	0.20947	3.27	01705	13,821	93,970	0.20947	2.27	01706	26,620	101,091	0.20947	2.10
P	P		-67,555	840	0.20947	NS		-60,860	1,030	0.20947	NS		-33,124	1,381	0.20947	NS
S	A		-61,157	34,664	0.20947	6.44		-70,012	45,959	0.20947	4.88		-71,630	50,194	0.20947	4.47
P	P		-2,986	777	0.20947	NS		-476	957	0.20947	NS		1,945	1,171	0.20947	NS
P	A	01707	-45,398	1,185	0.20947	NS	01708	-42,636	588	0.20947	NS	01709	-15,045	43,024	0.20947	5.05
P	P		-67,841	165,227	0.41893	2.53		-36,761	37,382	0.20947	5.88		-56,148	777	0.20947	NS
S	A		-8,006	200	0.20947	NS		-31,956	610	0.20947	NS		-46,169	23,828	0.20947	9.28
P	P		-14,234	28,021	0.20947	7.75		-10,425	349	0.20947	NS		-5,981	630	0.20947	NS
P	A	01710	3,854	89,610	0.20947	2.40	01711	19,697	109,823	0.20947	1.94	01712	32,918	108,643	0.20947	1.94
P	P		-66,852	1,069	0.20947	NS		-60,990	1,453	0.20947	NS		-35,406	2,119	0.20947	NS
S	A		-56,643	40,006	0.20947	5.56		-61,704	48,404	0.20947	4.61		-61,953	49,446	0.20947	4.51
P	P		-2,690	898	0.20947	NS		-502	1,129	0.20947	NS		1,266	1,456	0.20947	NS
P	A	01713	-45,502	1,133	0.20947	NS	01714	-29,680	5,003	0.20947	43.78	01715	-8,374	72,645	0.20947	2.98
P	P		-53,590	104,860	0.20947	2.12		-7,574	1,335	0.20947	NS		-71,541	976	0.20947	NS
S	A		-8,482	136	0.20947	NS		-34,734	10,938	0.20947	20.09		-45,197	30,788	0.20947	7.18
P	P		-28,482	14,551	0.20947	15.04		-8,782	429	0.20947	NS		-5,152	735	0.20947	NS
P	A	01716	10,445	108,940	0.20947	1.96	01717	27,767	119,794	0.20947	1.77	01718	-49,560	1,789	0.20947	NS
P	P		-66,343	1,414	0.20947	NS		-40,747	1,982	0.20947	NS		-72,604	195,095	0.41893	2.15
S	A		-52,077	43,146	0.20947	5.14		-54,284	48,457	0.20947	4.59		-8,512	336	0.20947	NS
P	P		-2,458	1,027	0.20947	NS		346	1,309	0.20947	NS		-13,801	31,993	0.20947	6.78
P	A	01719	-45,278	903	0.20947	NS	01720	-21,252	43,109	0.20947	5.06	01721	-507	97,503	0.20947	2.21
P	P		-43,580	47,221	0.20947	4.68		-57,837	749	0.20947	NS		-70,618	1,267	0.20947	NS
S	A		-4,288	32	0.20947	NS		-36,088	19,359	0.20947	11.36		-43,652	35,634	0.20947	6.20
P	P		-31,588	3,856	0.20947	56.87		-7,458	541	0.20947	NS		-4,408	859	0.20947	NS
P	A	01722	18,125	122,583	0.20947	1.74	01723	34,574	123,067	0.20947	1.71	01724	-47,527	1,470	0.20947	NS
P	P		-65,638	1,839	0.20947	NS		-41,452	2,703	0.20947	81.60		-59,572	115,905	0.20947	1.92
S	A		-47,716	44,329	0.20947	4.99		-48,896	45,683	0.20947	4.85		-8,665	193	0.20947	NS
P	P		-973	1,172	0.20947	NS		-689	1,507	0.20947	NS		-21,539	17,463	0.20947	12.48
P	A	01725	-51,456	1,291	0.20947	NS	01726	-12,208	75,270	0.20947	2.88	01727	8,069	116,308	0.20947	1.84
P	P		-10,212	1,787	0.20947	NS		-74,105	1,025	0.20947	NS		-69,480	1,633	0.20947	NS
S	A		-29,116	7,344	0.20947	29.82		-36,819	26,728	0.20947	8.23		-42,091	38,913	0.20947	5.67
P	P		-9,653	349	0.20947	NS		-6,331	672	0.20947	NS		-3,928	985	0.20947	NS
P	A	01728	27,704	129,594	0.20947	1.63	01729	-50,002	2,047	0.20947	NS	01730	-46,692	1,068	0.20947	NS
P	P		-45,051	2,355	0.20947	93.86		-72,624	200,875	0.41893	2.08		-46,695	52,306	0.20947	4.23
S	A		-44,081	44,377	0.20947	4.98		-12,308	383	0.20947	NS		-6,403	60	0.20947	NS
P	P		-1,102	1,319	0.20947	NS		-14,872	33,898	0.20947	6.41		-26,874	6,172	0.20947	35.43
P	A	01731	-24,095	42,558	0.20947	5.13	01732	-2,698	100,797	0.20947	2.14	01733	17,120	128,426	0.20947	1.66
P	P		-58,798	720	0.20947	NS		-72,587	1,359	0.20947	NS		-67,946	2,039	0.20947	NS
S	A		-31,355	16,449	0.20947	13.33		-37,357	32,315	0.20947	6.81		-40,676	40,832	0.20947	5.40
P	P		-8,204	488	0.20947	NS		-5,430	810	0.20947	NS		-1,931	1,143	0.20947	NS
P	A	01734	35,300	129,860	0.20947	1.62	01735	-48,733	1,596	0.20947	NS	01736	-45,600	640	0.20947	NS
P	P		-44,518	3,006	0.20947	73.51		-62,186	137,276	0.20947	1.63		-11,166	1,980	0.20947	NS
S	A		-42,179	42,213	0.20947	5.23		-8,227	227	0.20947	NS		-26,897	5,767	0.20947	37.92
P	P		-1,905	1,479	0.20947	NS		-16,753	18,624	0.20947	11.67		-10,032	317	0.20947	NS
P	A	01737	-13,752	76,029	0.20947	2.85	01738	7,018	118,955	0.20947	1.80	01739	27,524	133,307	0.20947	1.59
P	P		-75,140	1,041	0.20947	NS		-70,679	1,721	0.20947	NS		-46,637	2,509	0.20947	88.18
S	A		-33,563	24,767	0.20947	8.86		-38,153	36,705	0.20947	6.00		-39,949	42,097	0.20947	5.23
P	P		-6,868	638	0.20947	NS		-2,719	945	0.20947	NS		-1,868	1,291	0.20947	NS
P	A	01740	-49,205	2,081	0.20947	NS	01741	-46,997	1,097	0.20947	NS	01742	-24,743	42,391	0.20947	5.15
P	P		-74,666	205,549	0.41893	2.04		-47,436	53,247	0.20947	4.16		-58,957	716	0.20947	NS
S	A		-12,737	385	0.20947	NS		-6,465	68	0.20947	NS		-30,442	15,861	0.20947	13.82
P	P		-16,061	34,318	0.20947	6.33		-26,408	6,712	0.20947	32.57		-8,375	475	0.20947	NS
P	A	01743	-3,273	101,357	0.20947	2.13	01744	16,694	129,471	0.20947	1.65	01745	35,292	131,082	0.20947	1.61
P	P		-72,875	1,378	0.20947	NS		-68,234	2,078	0.20947	NS		-44,779	3,056	0.20947	72.32
S	A		-36,131	31,591	0.20947	6.96		-39,282	40,068	0.20947	5.50		-40,915	41,526	0.20947	5.31
P	P		-5,668	794	0.20947	NS		-2,262	1,126	0.20947	NS		-2,323	1,462	0.20947	NS
P	A	01746	-48,518	1,547	0.20947	NS	01747	-45,184	617	0.20947	NS	01748	-13,463	75,770	0.20947	2.86
P	P		-63,410	133,183	0.20947	1.68		-10,419	1,917	0.20947	NS		-74,670	1,039	0.20947	NS
S	A		-7,561	228	0.20947	NS		-27,547	6,343	0.20947	34.49		-34,561	25,426	0.20947	8.64
P	P		-16,027	18,563	0.20947	11.71		-9,930	326	0.20947	NS		-6,732	645	0.20947	NS
P	A	01749	7,038	118,098	0.20947	1.81	01750	27,192	132,233	0.20947	1.60	01751	-46,434	1,903	0.20947	NS
P	P		-70,091	1,694	0.20947	NS		-45,668	2,460	0.20947	89.88		-76,461	190,532	0.41893	2.20
S	A		-39,353	37,432	0.20947	5.89		-41,177	42,809	0.20947	5.15		-9,604	337	0.20947	NS
P	P		-4,500	953	0.20947	NS		-1,702	1,293	0.20947	NS		-17,809	33,563	0.20947	6.48
P	A	01752	-46,038	996	0.20947	NS	01753	-23,322	42,753	0.20947	5.10	01754	-2,341	99,539	0.20947	2.17
P	P		-45,737	50,329	0.20947	4.39		-58,285	737	0.20947	NS		-71,552	1,328	0.20947	NS
S	A		-6,286	47	0.20947	NS		-33,137	17,630	0.20947	12.45		-39,676	33,631	0.20947	6.55
P	P		-30,178	5,430	0.20947	40.35		-7,961	505	0.20947	NS		-5,128			



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
P	A	01761	26,972	125,812	0.20947	1.68	01762	-45,260	1,523	0.20947	NS	01763	-43,928	752	0.20947	NS
	P		-42,339	2,190	0.20947	NS		-66,034	180,758	0.41893	2.31		-42,113	42,990	0.20947	5.13
S	A	01764	-48,011	46,352	0.20947	4.78	01765	-9,182	274	0.20947	NS	01766	0	0	0.20947	-
	P		-715	1,338	0.20947	NS		-19,648	32,798	0.20947	6.64		-35,497	2,490	0.20947	88.27
P	A	01767	-19,649	43,187	0.20947	5.04	01768	455	94,290	0.20947	2.28	01769	17,886	117,290	0.20947	1.82
	P		-56,870	772	0.20947	NS		-68,630	1,190	0.20947	NS		-63,160	1,673	0.20947	NS
S	A	01770	-40,126	21,370	0.20947	10.31	01771	-48,902	37,765	0.20947	5.87	01772	-53,425	46,399	0.20947	4.79
	P		-6,897	576	0.20947	NS		-3,738	873	0.20947	NS		-464	1,124	0.20947	NS
P	A	01773	33,369	116,790	0.20947	1.81	01774	-45,020	849	0.20947	NS	01775	-26,752	7,497	0.20947	29.17
	P		-38,778	2,433	0.20947	90.52		-48,779	96,576	0.20947	2.29		-5,728	1,022	0.20947	NS
S	A	01776	-54,144	47,484	0.20947	4.68	01777	-8,821	64	0.20947	NS	01778	-39,166	13,050	0.20947	16.88
	P		-1	1,426	0.20947	NS		-27,027	12,417	0.20947	17.61		-8,123	486	0.20947	NS
P	A	01779	-6,238	69,939	0.20947	3.09	01780	11,113	102,626	0.20947	2.08	01781	26,319	111,406	0.20947	1.90
	P		-69,463	933	0.20947	NS		-63,553	1,246	0.20947	NS		-36,823	1,691	0.20947	NS
S	A	01782	-51,759	32,908	0.20947	6.74	01783	-59,649	45,054	0.20947	4.95	01784	-61,812	49,541	0.20947	4.51
	P		-4,253	758	0.20947	NS		-1,574	996	0.20947	NS		1,062	1,261	0.20947	NS
P	A	01785	-46,040	757	0.20947	NS	01786	-41,027	368	0.20947	NS	01787	-11,003	41,947	0.20947	5.16
	P		-40,561	150,581	0.41893	2.77		-31,201	30,793	0.20947	7.12		-55,033	775	0.20947	NS
S	A	01788	-8,097	102	0.20947	NS	01789	-37,026	3,474	0.20947	62.53	01790	-54,103	25,807	0.20947	8.61
	P		-12,167	24,264	0.20947	8.81		-9,283	456	0.20947	NS		-4,768	671	0.20947	NS
P	A	01791	5,776	82,856	0.20947	2.59	01792	19,186	99,868	0.20947	2.13	01793	28,829	98,914	0.20947	2.14
	P		-63,922	919	0.20947	NS		-57,127	1,187	0.20947	NS		-30,721	1,741	0.20947	NS
S	A	01794	-66,168	41,179	0.20947	5.43	01795	-71,407	48,542	0.20947	4.62	01796	-69,664	48,325	0.20947	4.64
	P		-1,617	857	0.20947	NS		424	1,045	0.20947	NS		1,938	1,277	0.20947	NS
P	A	01797	-28,663	195	0.20947	NS	01798	-12,899	12,473	0.20947	17.39	01799	2,289	59,492	0.20947	3.61
	P		-30,882	70,227	0.20947	3.12		-57,999	856	0.20947	NS		-64,726	716	0.20947	NS
S	A	01800	0	0	0.20947	-	01801	-55,040	17,359	0.20947	12.63	01802	-72,770	34,564	0.20947	6.50
	P		-36,516	6,290	0.20947	34.43		-4,994	637	0.20947	NS		-1,524	726	0.20947	NS
P	A	01803	13,784	82,314	0.20947	2.59	01804	23,116	86,997	0.20947	2.44	01805	0	0	0.20947	-
	P		-56,619	774	0.20947	NS		-27,385	1,002	0.20947	NS		-18,639	105,641	0.20947	2.06
S	A	01806	-82,112	44,143	0.20947	5.11	01807	-82,711	46,583	0.20947	4.85	01808	0	0	0.20947	-
	P		433	816	0.20947	NS		2,095	921	0.20947	NS		-19,012	15,626	0.20947	13.69
P	A	01809	-24,525	32	0.20947	NS	01810	1,283	35,002	0.20947	6.14	01811	9,154	60,862	0.20947	3.52
	P		-10,103	15,008	0.20947	14.43		-66,319	645	0.20947	NS		-56,384	471	0.20947	NS
S	A	01812	-53,379	7,837	0.20947	27.90	01813	-78,565	24,775	0.20947	8.97	01814	-93,141	34,865	0.20947	6.52
	P		-4,408	699	0.20947	NS		-765	631	0.20947	NS		575	547	0.20947	NS
P	A	01815	14,920	70,132	0.20947	3.04	01816	18,896	67,615	0.20947	3.15	01817	0	0	0.20947	-
	P		-47,117	547	0.20947	NS		-18,082	839	0.20947	NS		1,881	36,405	0.20947	5.91
S	A	01818	-97,183	38,325	0.20947	5.94	01819	-91,276	36,394	0.20947	6.24	01820	0	0	0.20947	-
	P		1,477	515	0.20947	NS		2,374	581	0.20947	NS		-4,747	816	0.20947	NS
P	A	01791	3,424	12,533	0.20947	17.14	01792	4,318	37,569	0.20947	5.71	01793	5,226	48,367	0.20947	4.44
	P		-68,560	705	0.20947	NS		-44,361	253	0.20947	NS		-45,547	184	0.20947	NS
S	A	01794	-82,139	12,848	0.20947	17.32	01795	-	20,011	0.20947	11.42	01796	-	21,865	0.20947	10.50
	P		992	552	0.20947	NS		103,115					111,310			
P	A	01797	7,051	49,339	0.20947	4.34	01798	1,272	236	0.20947	NS	01799	721	31	0.20947	NS
	P		-34,910	301	0.20947	NS		0	0	0.20947	-		0	0	0.20947	-
S	A	01799	-	20,051	0.20947	11.42	01800	29,552	43,796	0.20947	4.83	01801	-15,124	3,997	0.20947	54.34
	P		107,524	0	0.20947	-		0	0	0.20947	-		-80,672	65	0.20947	NS
P	A	01797	-2,998	15,470	0.20947	13.94	01798	-32,260	5,663	0.20947	38.09	01799	3,826	399	0.20947	NS
	P		-44,553	112	0.20947	NS		-9,827	24,043	0.20947	9.00		-12,936	26,124	0.20947	8.30
S	A	01800	888	330	0.20947	NS	01801	0	0	0.20947	-	01802	0	0	0.20947	-
	P		-	1,646	0.20947	NS		-88	673	0.20947	NS		-252	888	0.20947	NS
P	A	01803	108,831				01804	-	5,863	0.20947	39.41	01805	-	10,067	0.20947	22.96
	P		-11,006	23,815	0.20947	9.10		123,479					124,147			
S	A	01806	-19,157	21	0.20947	NS	01807	0	0	0.20947	-	01808	-31,226	159	0.20947	NS
	P		-148	1,030	0.20947	NS		10,330	10,485	0.20947	20.40		8,762	455	0.20947	NS
P	A	01809	-	13,401	0.20947	17.15	01810	3,398	167	0.20947	NS	01811	4,768	1,129	0.20947	NS
	P		113,437					-59,786	12,205	0.20947	18.03		-	30,042	0.20947	7.66
P	A	01803	-55,844	728	0.20947	NS	01804	-59,109	804	0.20947	NS	01805	115,880			
	P		7,493	269	0.20947	NS		5,929	198	0.20947	NS		-454	347	0.20947	NS
S	A	01806	1,765	1,514	0.20947	NS	01807	714	1,678	0.20947	NS	01808	-49,218	703	0.20947	NS
	P		-	47,182	0.20947	4.92		-	59,573	0.20947	3.91		-165	1,956	0.20947	NS
			132,815					138,756					-	64,759	0.20947	3.57
													126,041			
Piano Fondo Vasca			PareteP2-P5								Parete P2-P5					
P	A	00001	136,616	8,459	0.13407	14.30	00047	157,265	8,817	0.13407	13.41	00049	-8,082	5,666	0.13407	24.65
	P		0	0	0.13407	-		0	0	0.13407	-		-31,365	2,503	0.13407	57.01
S	A	00050	70,357	45,975	0.13407	2.75	00474	100,970	47,752	0.13407	2.55	00475	-25,294	1,496	0.13407	94.86
	P		-78,627	5,643	0.13407	25.81		-58,876	3,821	0.13407	37.34		-5,036	220	0.13407	NS
P	A	00476	-7,618	5,482	0.13407	25.47	00477	25,441	5,474	0.13407	24.73	00478	6,040	4,682	0.13407	29.45
	P		-27,125	2,564	0.13407	55.44		21,132	107	0.13407	NS		10,109	910	0.13407	NS
S	A	00479	-24,369	1,576	0.13407	89.97	00480	42,122	33,424	0.13407	3.90	00481	-8,818	23,133	0.13407	6.04
	P		-5,066	103	0.13407	NS		-18,404	1,368	0.13407	NS		-6,568	2,567	0.13407	54.34
P	A	00476	-6,407	3,855	0.13407	36.18	00477	-40,156	1,811	0.13407	79.42	00478	-53,628	605	0.13407	NS
	P		-6,159	1,111	0.13407	NS		-9,622	1,694	0.13407	82.58		-10,769	2,542	0.13	



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																	
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]		
S	A		9,468	66	0.13407	NS		9,894	246	0.13407	NS		8,477	409	0.13407	NS	
	P		3,298	3,922	0.13407	35.24		-31,071	5,130	0.13407	27.81		-34,316	6,716	0.13407	21.30	
P	A	00482	-91,269	1,125	0.13407	NS	00483	-	1,273	0.13407	NS	00484	-	1,388	0.13407	NS	
	P		-34,521	11,121	0.13407	12.87		103,169	-37,984	12,157	0.13407	11.81	105,617	-39,869	14,233	0.13407	10.10
S	A		6,148	537	0.13407	NS		4,612	688	0.13407	NS		3,009	791	0.13407	NS	
	P		-29,995	7,233	0.13407	19.70		-29,914	8,549	0.13407	16.67		-29,849	8,772	0.13407	16.24	
P	A	00485	-	1,526	0.13407	99.95	00486	-	1,609	0.13407	94.95	00487	-	1,704	0.13407	89.75	
	P		107,714	-42,488	15,964	0.13407	9.03	109,739	-44,124	15,911	0.13407	9.07	111,010	-45,540	17,576	0.13407	8.22
S	A		6,069	1,838	0.13407	75.00		6,299	2,454	0.13407	56.17		6,014	3,300	0.13407	41.78	
	P		-26,958	8,293	0.13407	17.14		-27,011	8,738	0.13407	16.27		-26,561	8,629	0.13407	16.46	
P	A	00488	-	1,789	0.13407	85.54	00489	-	1,823	0.13407	83.98	00490	-	1,866	0.13407	82.08	
	P		111,693	-46,972	18,647	0.13407	7.76	112,178	-47,304	17,751	0.13407	8.15	112,679	-47,937	18,954	0.13407	7.64
S	A		5,854	4,468	0.13407	30.86		6,252	4,689	0.13407	29.40		6,088	5,144	0.13407	26.80	
	P		-25,189	8,130	0.13407	17.45		-25,385	8,332	0.13407	17.03		-24,850	8,200	0.13407	17.30	
P	A	00491	-	1,891	0.13407	81.00	00492	-	1,883	0.13407	81.33	00493	-	1,863	0.13407	82.17	
	P		112,793	-48,401	19,554	0.13407	7.41	112,534	-47,613	18,013	0.13407	8.04	112,116	-47,360	18,683	0.13407	7.75
S	A		5,758	5,328	0.13407	25.88		6,266	4,960	0.13407	27.79		5,512	4,940	0.13407	27.92	
	P		-24,950	8,017	0.13407	17.70		-25,199	8,289	0.13407	17.12		-24,636	8,140	0.13407	17.42	
P	A	00494	-	1,823	0.13407	83.95	00495	-	1,769	0.13407	86.46	00496	-	1,710	0.13407	89.32	
	P		111,726	-46,911	18,876	0.13407	7.67	111,027	-45,105	16,814	0.13407	8.59	109,371	-43,827	17,191	0.13407	8.39
S	A		5,128	4,202	0.13407	32.84		5,726	3,268	0.13407	42.20		5,892	2,847	0.13407	48.43	
	P		-26,090	8,241	0.13407	17.23		-26,741	8,718	0.13407	16.30		-25,932	8,362	0.13407	16.98	
P	A	00557	-31,190	3,201	0.13407	44.57	00558	-14,436	7,339	0.13407	19.15	00559	-34,788	10,407	0.13407	13.75	
	P		-17,978	297	0.13407	NS		-35,375	648	0.13407	NS		-29,341	704	0.13407	NS	
S	A		-49,355	12,063	0.13407	12.02		-69,394	36,610	0.13407	4.03		-	49,673	0.13407	3.06	
	P		24,043	3,737	0.13407	36.27		6,670	3,823	0.13407	36.04		104,774	7,991	3,776	0.13407	36.44
P	A	00560	-29,740	13,418	0.13407	10.62	00561	-19,243	14,469	0.13407	9.75	00562	-14,357	16,177	0.13407	8.69	
	P		-36,939	790	0.13407	NS		-25,474	612	0.13407	NS		4,176	665	0.13407	NS	
S	A		-	52,544	0.13407	2.91		-	72,806	0.13407	2.11		-	59,580	0.13407	2.57	
	P		112,174	2,794	2,812	0.13407	49.18	117,719	3,778	2,927	0.13407	47.20	114,016	4,877	2,197	0.13407	62.82
P	A	00563	13,091	17,634	0.13407	7.77	00564	53,270	14,910	0.13407	8.84	00565	105,015	16,452	0.13407	7.60	
	P		21,414	582	0.13407	NS		40,276	1,252	0.13407	NS		97,813	3,159	0.13407	39.88	
S	A		-	65,137	0.13407	2.36		-78,809	70,985	0.13407	2.10		-39,732	55,330	0.13407	2.60	
	P		115,106	-6,160	2,101	0.13407	66.37	654	2,040	0.13407	67.92		22,615	2,447	0.13407	55.46	
P	A	00566	32,790	4,608	0.13407	29.17	00567	3,116	4,826	0.13407	28.64	00568	-5,775	4,142	0.13407	33.65	
	P		8,982	489	0.13407	NS		8,635	1,007	0.13407	NS		-4,141	914	0.13407	NS	
S	A		32,192	33,112	0.13407	3.98		-28,906	21,777	0.13407	6.54		-30,947	14,117	0.13407	10.10	
	P		-38,817	1,732	0.13407	81.44		-7,354	2,847	0.13407	49.03		-7,458	3,484	0.13407	40.07	
P	A	00569	-19,377	1,371	0.13407	NS	00570	-49,968	548	0.13407	NS	00571	-65,160	739	0.13407	NS	
	P		-3,889	1,947	0.13407	71.47		-6,772	2,791	0.13407	49.99		-19,869	3,478	0.13407	40.60	
S	A		-37,817	7,064	0.13407	20.32		-37,998	1,753	0.13407	81.89		8,816	203	0.13407	NS	
	P		-4,627	4,218	0.13407	33.01		109	4,136	0.13407	33.52		1,139	3,843	0.13407	36.04	
P	A	00572	-73,447	842	0.13407	NS	00573	-82,707	980	0.13407	NS	00574	-90,879	1,153	0.13407	NS	
	P		-22,367	5,807	0.13407	24.37		-26,176	8,751	0.13407	16.23		-31,675	9,846	0.13407	14.50	
S	A		8,631	448	0.13407	NS		6,669	588	0.13407	NS		5,601	693	0.13407	NS	
	P		-38,021	4,929	0.13407	29.12		-34,182	6,246	0.13407	22.90		-32,325	7,220	0.13407	19.78	
P	A	00575	-95,308	1,263	0.13407	NS	00576	-	1,437	0.13407	NS	00577	-	1,576	0.13407	96.78	
	P		-33,584	12,046	0.13407	11.87		105,731	-37,095	14,801	0.13407	9.69	107,741	-42,407	15,825	0.13407	9.11
S	A		5,122	838	0.13407	NS		998	862	0.13407	NS		5,025	1,428	0.13407	96.63	
	P		-31,911	8,525	0.13407	16.75		-28,760	8,261	0.13407	17.23		-29,807	8,550	0.13407	16.67	
P	A	00578	146,848	17,210	0.13407	6.95	00579	44,062	17,616	0.13407	7.55	00580	11,782	17,433	0.13407	7.87	
	P		105,458	3,011	0.13407	41.51		44,820	964	0.13407	NS		20,134	655	0.13407	NS	
S	A		-15,775	58,088	0.13407	2.37		-82,089	60,503	0.13407	2.47		-	64,010	0.13407	2.37	
	P		19,187	2,080	0.13407	63.96		-5,539	1,913	0.13407	72.85		101,116	6,035	2,024	0.13407	68.11
P	A	00581	-9,879	13,971	0.13407	10.02	00582	-7,762	16,934	0.13407	8.25	00583	-40,616	12,013	0.13407	11.98	
	P		18,734	681	0.13407	NS		-29,425	660	0.13407	NS		-27,141	752	0.13407	NS	
S	A		-	65,671	0.13407	2.32		-	61,705	0.13407	2.48		-	56,613	0.13407	2.68	
	P		108,776	3,751	2,208	0.13407	62.57	113,962	2,860	2,516	0.13407	54.96	103,160	5,039	2,972	0.13407	46.43
P	A	00584	-24,135	10,720	0.13407	13.22	00585	-7,963	9,093	0.13407	15.36	00586	-36,446	3,881	0.13407	36.94	
	P		-34,764	712	0.13407	NS		-37,017	947	0.13407	NS		-8,601	816	0.13407	NS	
S	A		-	45,002	0.13407	3.37		-56,192	27,540	0.13407	5.30		-49,606	11,113	0.13407	13.05	
	P		101,732	4,490	3,223	0.13407	42.84	14,635	3,791	0.13407	36.07		23,114	3,775	0.13407	35.93	
P	A	00855	-81,463	6,429	0.13407	23.20	00856	-	6,206	0.13407	24.52	00857	-62,377	17,659	0.13407	8.31	
	P		28,985	9,541	0.13407	14.14		105,006	10,056	787	0.13407	NS	0	0	0.13407	-	
S	A		-13,261	2,088	0.13407	67.22		-11,276	1,449	0.13407	96.69		-11,617	3,719	0.13407	37.68	
	P		-8,455	2,590	0.13407	53.95		-4,599	1,055	0.13407	NS		0	0	0.13407	-	
P	A	00858	-25,232	21,139	0.13407	6.71	00859	-24,617	33,995	0.13407	4.17	00860	-40,159	47,437	0.13407	3.03	



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-17,795	8,041	0.13407	17.53		-18,792	8,821	0.13407	15.99		-17,213	10,194	0.13407	13.82
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	00861	-58,472	49,083	0.13407	2.98	00862	-48,275	56,205	0.13407	2.58	00863	-58,062	65,809	0.13407	2.22
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-12,722	13,001	0.13407	10.79		-12,328	14,533	0.13407	9.65		-15,531	13,698	0.13407	10.27
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	00864	-71,361	64,405	0.13407	2.30	00865	-60,709	66,738	0.13407	2.19	00866	-70,958	70,613	0.13407	2.09
	P		0	0	0.13407	-		0	0	0.13407	-		-12,266	731	0.13407	NS
S	A		-16,463	15,143	0.13407	9.30		-12,994	17,714	0.13407	7.92		-15,987	19,347	0.13407	7.27
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	00867	-67,377	73,707	0.13407	2.00	00868	-71,156	78,512	0.13407	1.88	00869	-76,055	76,516	0.13407	1.94
	P		-11,570	1,481	0.13407	94.62		-9,456	1,630	0.13407	85.81		-10,907	2,390	0.13407	58.60
S	A		-20,326	15,781	0.13407	8.95		-13,656	16,169	0.13407	8.68		-15,032	20,402	0.13407	6.89
	P		-2,380	101	0.13407	NS		-2,168	291	0.13407	NS		-1,432	184	0.13407	NS
P	A	00870	-70,217	76,978	0.13407	1.92	00871	-73,579	82,416	0.13407	1.80	00872	-78,257	77,521	0.13407	1.92
	P		-9,631	2,880	0.13407	48.57		-10,174	2,749	0.13407	50.91		-10,559	3,114	0.13407	44.96
S	A		-15,891	16,951	0.13407	8.30		-15,269	16,948	0.13407	8.30		-14,164	19,992	0.13407	7.03
	P		-2,098	433	0.13407	NS		-2,355	516	0.13407	NS		-1,823	329	0.13407	NS
P	A	00873	-69,572	77,003	0.13407	1.92	00874	-73,272	82,955	0.13407	1.79	00875	-76,846	75,977	0.13407	1.96
	P		-11,362	3,043	0.13407	46.04		-10,192	2,488	0.13407	56.25		-10,369	2,435	0.13407	57.49
S	A		-15,028	17,681	0.13407	7.95		-15,552	17,041	0.13407	8.25		-14,309	18,861	0.13407	7.45
	P		-1,932	519	0.13407	NS		-2,247	464	0.13407	NS		-1,309	139	0.13407	NS
P	A	00876	-66,053	74,289	0.13407	1.98	00877	-68,200	79,723	0.13407	1.85	00878	-72,913	71,593	0.13407	2.07
	P		-9,689	1,787	0.13407	78.29		-10,291	841	0.13407	NS		-11,522	664	0.13407	NS
S	A		-12,728	17,878	0.13407	7.85		-18,275	16,416	0.13407	8.59		-12,012	17,099	0.13407	8.20
	P		-1,763	282	0.13407	NS		-2,492	143	0.13407	NS		0	0	0.13407	-
P	A	00879	-59,170	68,062	0.13407	2.15	00880	-63,586	71,855	0.13407	2.04	00881	-63,791	62,275	0.13407	2.36
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-11,470	17,419	0.13407	8.04		-16,138	14,865	0.13407	9.47		-15,743	14,255	0.13407	9.87
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	00882	-49,699	56,238	0.13407	2.58	00883	-53,768	55,819	0.13407	2.61	00884	-44,088	44,654	0.13407	3.23
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-13,177	15,730	0.13407	8.92		-16,363	11,915	0.13407	11.81		-21,596	9,739	0.13407	14.52
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
P	A	00885	-28,182	34,847	0.13407	4.08	00886	-21,522	25,956	0.13407	5.45	00887	-16,424	16,142	0.13407	8.72
	P		0	0	0.13407	-		0	0	0.13407	-		0	0	0.13407	-
S	A		-14,975	11,615	0.13407	12.10		-15,108	6,279	0.13407	22.39		-14,453	2,430	0.13407	57.82
	P		0	0	0.13407	-		0	0	0.13407	-		628	16	0.13407	NS
P	A	00888	-	6,038	0.13407	25.18	00889	-79,617	6,620	0.13407	22.49	02247	-45,039	2,592	0.13407	55.73
	P		104,053													
	P		11,602	837	0.13407	NS		38,216	11,800	0.13407	11.33		-1,344	2,187	0.13407	63.47
S	A		-12,513	2,213	0.13407	63.38		-12,955	2,034	0.13407	68.99		-32,226	2,906	0.13407	49.14
	P		615	164	0.13407	NS		-1,964	3,503	0.13407	39.65		4,047	33	0.13407	NS
P	A	02248	65,752	12,179	0.13407	10.68	02249	83,808	12,357	0.13407	10.34	02250	-42,462	2,538	0.13407	56.79
	P		0	0	0.13407	-		0	0	0.13407	-		-1,108	1,152	0.13407	NS
S	A		-5,255	43,672	0.13407	3.13		31,310	43,845	0.13407	3.00		-34,928	2,131	0.13407	67.18
	P		-31,499	2,723	0.13407	51.42		-24,324	2,293	0.13407	60.48		7,755	191	0.13407	NS
P	A	02251	-73,701	3,133	0.13407	47.29	02252	-38,783	753	0.13407	NS	02253	2,673	2,744	0.13407	50.40
	P		12,097	2,664	0.13407	51.46		1,069	380	0.13407	NS		4,154	358	0.13407	NS
S	A		-29,445	3,126	0.13407	45.57		-74,237	13,015	0.13407	11.39		-98,734	24,765	0.13407	6.11
	P		0	0	0.13407	-		7,608	605	0.13407	NS		4,736	1,179	0.13407	NS
P	A	02254	13,508	5,044	0.13407	27.14	02255	27,578	7,981	0.13407	16.92	02256	17,983	7,905	0.13407	17.24
	P		9,476	329	0.13407	NS		15,471	213	0.13407	NS		1,357	50	0.13407	NS
S	A		-	32,889	0.13407	4.62		-83,404	34,923	0.13407	4.28		-26,796	32,204	0.13407	4.33
	P		102,623													
	P		2,500	1,264	0.13407	NS		3,558	1,221	0.13407	NS		2,549	1,350	0.13407	NS
P	A	02257	-89,522	2,676	0.13407	56.12	02258	-72,435	954	0.13407	NS	02259	-58,478	350	0.13407	NS
	P		2,693	1,162	0.13407	NS		6,549	4,153	0.13407	33.18		9,680	3,037	0.13407	45.24
S	A		3,569	1,030	0.13407	NS		-69,095	3,293	0.13407	44.81		-80,836	8,210	0.13407	18.16
	P		-3,900	435	0.13407	NS		-5,476	679	0.13407	NS		-5,546	946	0.13407	NS
P	A	02260	-8,542	243	0.13407	NS	02261	1,194	3,424	0.13407	40.45	02262	-62,582	13,974	0.13407	10.50
	P		5,439	1,600	0.13407	86.21		5,522	1,165	0.13407	NS		-3,956	17	0.13407	NS
S	A		-73,992	12,490	0.13407	11.86		-42,519	14,843	0.13407	9.71		-23,195	2,178	0.13407	65.03
	P		-4,976	1,514	0.13407	92.00		-2,210	2,485	0.13407	55.91		-1,210	176	0.13407	NS
P	A	02263	-92,701	2,224	0.13407	67.71	02264	-80,204	1,135	0.13407	NS	02265	-69,924	640	0.13407	NS
	P		-7,629	5,033	0.13407	27.74		-1,332	9,765	0.13407	14.22		55	8,563	0.13407	16.19
S	A		885	1,046	0.13407	NS		4,925	653	0.13407	NS		6,831	260	0.13407	NS
	P		-46,271	3,085	0.13407	46.88		-61,318	3,424	0.13407	42.80		-1,738	2,563	0.13407	54.18
P	A	02266	-43,213	467	0.13407	NS	02267	-39,009	596	0.13407	NS	02268	-86,481	7,874	0.13407	19.02
	P		-4,362	4,778	0.13407	29.14		-8,096	2,279	0.13407	61.29		-6,291	1,548	0.13407	90.09
S	A		-48,859	1,680	0.13407	86.28		-33,896	4,550	0.13407	31.43		-9,975	964	0.13407	NS
	P		-997	3,230	0.13407	42.96		319	3,893	0.13407	35.60		-24,942	1,226	0.13407	NS
P	A	02269	-94,779	1,984	0.13407	76.04	02270	-86,964	1,242	0.13407	NS	02271	-80,497	862	0.13407	NS
	P		-17,981	10,559	0.13407	13.35		-12,935	14,861	0.13407	9.44		-13,436	12,782	0.13407	10.98
S	A		357	922	0.13407	NS		5,208	700	0.13407	NS		8,221	434	0.13407	NS
	P		-41,775	6,153	0.13407	23.41		-48,890	7,545	0.13407	19.21		-46,544	6,421	0.13407	22.53
P	A	02272	-61,531	733	0.13407	NS	02273	-48,160	28,708	0.13407	5.05	02274	-	2,631	0.13407	57.72
	P												102,610			
	P		-18,163	7,896	0.13407	17.86		-8,048	48	0.13407	NS		-8,362	3,466	0.13407	40.31



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D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
S	A		8,943	193	0.13407	NS		-22,239	4,738	0.13407	29.87		-6,993	891	0.13407	NS
	P		1,744	3,951	0.13407	35.03		-803	218	0.13407	NS		-27,033	3,800	0.13407	37.40
P	A	02275	-98,190	1,832	0.13407	82.59	02276	-93,573	1,321	0.13407	NS	02277	-89,497	1,038	0.13407	NS
	P		-27,515	16,314	0.13407	8.72		-24,118	18,823	0.13407	7.53		-24,601	15,349	0.13407	9.24
S	A		673	837	0.13407	NS		5,554	702	0.13407	NS		8,774	531	0.13407	NS
	P		-35,908	8,406	0.13407	17.05		-38,868	9,837	0.13407	14.60		-37,085	8,907	0.13407	16.10
P	A	02278	-77,387	928	0.13407	NS	02279	-65,089	15,000	0.13407	9.80	02280	-	2,283	0.13407	66.65
	P		-26,567	9,539	0.13407	14.89		-9,594	2,637	0.13407	53.05		104,923	-	0.13407	
S	A		10,459	355	0.13407	NS		-28,582	832	0.13407	NS		-41,400	11,368	0.13407	12.67
	P		-31,453	6,700	0.13407	21.30		-860	842	0.13407	NS		-5,241	795	0.13407	NS
P	A	02281	-	1,750	0.13407	86.76	02282	-99,583	1,391	0.13407	NS	02283	-25,877	6,276	0.13407	22.62
	P		102,317	-	0.13407			-	-	0.13407			-96,759	1,188	0.13407	NS
S	A		-35,477	21,078	0.13407	6.79		-32,755	21,268	0.13407	6.72		-32,036	16,210	0.13407	8.81
	P		1,204	785	0.13407	NS		5,365	716	0.13407	NS		7,939	610	0.13407	NS
P	A	02284	-30,741	10,007	0.13407	14.25	02285	-32,379	10,880	0.13407	13.13	02286	-31,758	9,769	0.13407	14.61
	P		-62,388	39,955	0.13407	3.67		-	2,538	0.13407	60.17		-	2,081	0.13407	73.31
S	A		-9,944	1,336	0.13407	NS		109,214	-	0.13407			108,010	-	0.13407	
	P		-22,961	6,614	0.13407	21.41		-11,445	5,019	0.13407	27.92		-46,158	18,470	0.13407	7.83
P	A	02287	-1,176	429	0.13407	NS	02288	-19,630	2,407	0.13407	58.65	02289	-3,819	761	0.13407	NS
	P		-	1,712	0.13407	88.98		-	1,459	0.13407	NS		-24,096	8,042	0.13407	17.63
S	A		106,292	-	0.13407			104,395	-	0.13407			-	1,319	0.13407	NS
	P		-41,402	24,367	0.13407	5.91		-38,630	22,137	0.13407	6.49		102,681	-	0.13407	
P	A	02290	-	1,712	0.13407	88.98	02291	-	1,459	0.13407	NS	02292	-37,279	15,962	0.13407	8.99
	P		1,373	779	0.13407	NS		4,535	759	0.13407	NS		5,461	719	0.13407	NS
S	A		-27,123	10,774	0.13407	13.19		-28,619	11,029	0.13407	12.91		-29,157	9,737	0.13407	14.63
	P		-61,897	20,170	0.13407	7.27		-	2,291	0.13407	66.81		-	1,965	0.13407	77.82
P	A	02293	-	1,706	0.13407	89.53	02294	-	1,533	0.13407	99.46	02295	110,872	-	0.13407	
	P		109,452	-	0.13407			107,306	-	0.13407			-49,581	23,719	0.13407	6.12
S	A		-45,290	25,957	0.13407	5.57		-41,998	21,432	0.13407	6.72		-2,872	769	0.13407	NS
	P		897	811	0.13407	NS		2,805	827	0.13407	NS		-22,608	9,355	0.13407	15.13
P	A	02296	-24,963	10,967	0.13407	12.94	02297	-26,570	10,631	0.13407	13.36	02298	-71,968	46,342	0.13407	3.19
	P		-94,290	4,342	0.13407	34.73		-	2,140	0.13407	71.65		-11,090	3,090	0.13407	45.33
S	A		-12,750	6,508	0.13407	21.56		114,025	-	0.13407			-16,790	7,585	0.13407	18.56
	P		-13,170	634	0.13407	NS		-56,722	18,843	0.13407	7.75		-1,326	725	0.13407	NS
P	A	02299	-	1,723	0.13407	88.80	02300	-	1,624	0.13407	94.06	02301	-51,565	26,987	0.13407	5.38
	P		111,454	-	0.13407			109,574	-	0.13407			-2,528	806	0.13407	NS
S	A		-47,402	25,921	0.13407	5.58		-44,344	19,932	0.13407	7.24		-21,728	9,991	0.13407	14.16
	P		-21	851	0.13407	NS		5,929	1,416	0.13407	97.37		-69,245	23,594	0.13407	6.25
P	A	02302	-23,875	10,670	0.13407	13.28	02303	-25,784	9,795	0.13407	14.49	02304	-11,514	5,553	0.13407	25.24
	P		-	2,249	0.13407	68.29		-	2,046	0.13407	75.03		-25,293	2,973	0.13407	47.73
S	A		116,082	-	0.13407			115,372	-	0.13407			-1,012	1,059	0.13407	NS
	P		-14,111	8,252	0.13407	17.02		-57,093	24,684	0.13407	5.92		114,156	-	0.13407	
P	A	02305	-10,822	674	0.13407	NS	02306	-5,811	772	0.13407	NS	02307	-52,232	28,239	0.13407	5.15
	P		-17,156	4,075	0.13407	34.57		-19,264	8,417	0.13407	16.77		-2,549	859	0.13407	NS
S	A		-	1,756	0.13407	87.16		-74,493	49,347	0.13407	3.00		-21,481	10,208	0.13407	13.85
	P		111,921	-	0.13407			-	1,624	0.13407	94.06		-98,485	5,836	0.13407	25.93
P	A	02308	-47,768	24,266	0.13407	5.97	02309	-10,443	4,359	0.13407	32.12	02310	-13,167	7,512	0.13407	18.68
	P		5,285	1,703	0.13407	81.01		-17,846	8,175	0.13407	17.24		-14,567	626	0.13407	NS
S	A		-23,612	10,167	0.13407	13.94		-1,698	933	0.13407	NS		118	1,067	0.13407	NS
	P		-	2,146	0.13407	71.62		-	1,985	0.13407	77.37		-	1,863	0.13407	82.33
P	A	02311	116,883	-	0.13407		02312	115,963	-	0.13407		02313	114,400	-	0.13407	
	P		-61,728	18,759	0.13407	7.82		-56,436	28,050	0.13407	5.20		-51,726	27,676	0.13407	5.25
S	A		-8,928	728	0.13407	NS		-5,014	827	0.13407	NS		4,578	1,373	0.13407	NS
	P		-17,577	6,197	0.13407	22.74		-19,583	9,265	0.13407	15.24		-21,739	10,050	0.13407	14.07
P	A	02314	-	1,809	0.13407	84.63	02315	-72,459	24,950	0.13407	5.93	02316	-	2,221	0.13407	69.25
	P		112,263	-	0.13407			-	1,939	0.13407	79.19		117,689	-	0.13407	
S	A		-47,866	21,902	0.13407	6.61		-11,773	6,245	0.13407	22.44		-14,467	8,841	0.13407	15.89
	P		5,826	3,286	0.13407	41.96		-24,202	3,393	0.13407	41.78		-11,892	675	0.13407	NS
P	A	02317	-23,994	9,330	0.13407	15.19	02318	-960	1,128	0.13407	NS	02319	-16,503	3,643	0.13407	38.64
	P		-	2,069	0.13407	74.29		-	1,939	0.13407	79.19		-	1,858	0.13407	82.48
S	A		117,034	-	0.13407			115,797	-	0.13407			113,424	-	0.13407	
	P		-59,894	24,954	0.13407	5.87		-54,810	29,058	0.13407	5.01		-49,882	25,366	0.13407	5.72
P	A	02320	-7,231	783	0.13407	NS	02321	3,896	878	0.13407	NS	02322	5,171	2,722	0.13407	50.69
	P		-18,260	7,942	0.13407	17.75		-20,335	9,749	0.13407	14.49		-22,480	9,774	0.13407	14.48
S	A		-74,706	49,858	0.13407	2.97		-99,338	6,113	0.13407	24.77		-	2,140	0.13407	71.85
	P		-9,843	4,595	0.13407	30.45		-13,412	7,707	0.13407	18.21		117,439	-	0.13407	
P	A	02321	-18,524	8,295	0.13407	17.00	02322	-14,898	626	0.13407	NS	02323	-62,539	18,721	0.13407	7.84
	P		-1,836	979	0.13407	NS		-70	1,058	0.13407	NS		-9,417	732	0.13407	NS
S	A		-	1,999	0.13407	76.86		-	1,894	0.13407	81.01		-17,438	6,045	0.13407	23.31
	P		116,476	-	0.13407			114,870	-	0.13407			-	1,855	0.13407	82.57
P	A	02322	-57,147	28,232	0.13407	5.17	02323	-52,304	27,996	0.13407	5.19	02324	112,713	-	0.13407	
	P		-5,619	838	0.13407	NS		3,888	1,631	0.13407	84.70		-48,193	22,265	0.13407	6.51
S	A		-	1,999	0.13407	76.86		-	1,894	0.13407	81.01		5,804	3,641	0.13407	37.87



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D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	P		-19,370	9,098	0.13407	15.51		-21,477	9,899	0.13407	14.29		-23,687	9,223	0.13407	15.36
P	A	02323	-71,911	24,489	0.13407	6.04	02324	-	2,216	0.13407	69.37	02325	-	2,055	0.13407	74.76
	P		-12,200	5,988	0.13407	23.42		117,190	8,614	0.13407	16.31		116,465	24,871	0.13407	5.88
S	A		-23,082	3,384	0.13407	41.85		-11,669	676	0.13407	NS		-6,908	788	0.13407	NS
	P		-776	1,114	0.13407	NS		-16,918	3,804	0.13407	37.02		-18,856	8,098	0.13407	17.42
P	A	02326	-	1,919	0.13407	79.98	02327	-	1,837	0.13407	83.38	02328	-70,892	47,957	0.13407	3.08
	P		115,196					112,820								
	P		-53,561	28,799	0.13407	5.05		-48,621	25,046	0.13407	5.79		-10,296	3,749	0.13407	37.34
S	A		-3,837	889	0.13407	NS		4,584	2,340	0.13407	59.00		-19,005	8,044	0.13407	17.54
	P		-20,974	9,894	0.13407	14.29		-22,991	9,875	0.13407	14.34		-2,017	849	0.13407	NS
P	A	02329	-96,730	5,233	0.13407	28.88	02330	-	2,126	0.13407	72.23	02331	-	1,947	0.13407	78.80
	P		-13,190	7,070	0.13407	19.85		115,791	18,803	0.13407	7.78		114,713	27,660	0.13407	5.26
S	A		-14,177	630	0.13407	NS		-59,336	737	0.13407	NS		-53,897	841	0.13407	NS
	P		-87	1,095	0.13407	NS		-8,410	6,498	0.13407	21.71		-4,310	9,543	0.13407	14.81
P	A	02332	-	1,815	0.13407	84.42	02333	-	1,757	0.13407	87.06	02334	-68,749	22,398	0.13407	6.59
	P		113,125					111,230								
	P		-49,260	27,005	0.13407	5.37		-45,348	21,158	0.13407	6.83		-12,058	4,894	0.13407	28.65
S	A		-2,009	929	0.13407	NS		5,307	2,434	0.13407	56.68		-21,436	2,930	0.13407	48.26
	P		-23,043	10,316	0.13407	13.73		-24,992	9,586	0.13407	14.80		-496	1,033	0.13407	NS
P	A	02335	-	2,235	0.13407	68.63	02336	-	1,996	0.13407	76.78	02337	-	1,800	0.13407	85.04
	P		114,451					113,448								
	P		-59,206	9,821	0.13407	14.89		-53,259	24,336	0.13407	5.98		-48,310	27,348	0.13407	5.30
S	A		-10,266	690	0.13407	NS		-5,006	796	0.13407	NS		-1,429	881	0.13407	NS
	P		-18,595	4,469	0.13407	31.56		-21,351	8,806	0.13407	16.06		-23,716	10,529	0.13407	13.46
P	A	02338	-	1,680	0.13407	90.93	02339	-64,450	44,929	0.13407	3.27	02340	-	3,419	0.13407	44.86
	P		109,588					-10,395	2,119	0.13407	66.06		114,401			
	P		-43,787	23,174	0.13407	6.23		-19,354	7,950	0.13407	17.75		-12,411	5,790	0.13407	24.22
S	A		84	952	0.13407	NS		-1,716	509	0.13407	NS		-12,572	664	0.13407	NS
	P		-25,452	10,385	0.13407	13.67		-					-18,486	1,564	0.13407	90.17
P	A	02341	-	2,088	0.13407	73.28	02342	-	1,805	0.13407	84.66	02343	-	1,608	0.13407	94.89
	P		111,483					109,982								
	P		-51,698	18,768	0.13407	7.74		-46,160	25,964	0.13407	5.57		-42,092	24,371	0.13407	5.91
S	A		-6,143	764	0.13407	NS		-1,445	844	0.13407	NS		1,418	878	0.13407	NS
	P		-22,114	7,425	0.13407	19.06		-25,086	10,374	0.13407	13.68		-27,067	10,903	0.13407	13.04
P	A	02344	-	1,512	0.13407	NS	02345	-58,596	17,718	0.13407	8.25	02346	-	2,258	0.13407	67.62
	P		107,506					-11,097	3,344	0.13407	41.89		109,054			
	P		-40,334	18,194	0.13407	7.91		-29,168	1,568	0.13407	90.82		-49,170	10,960	0.13407	13.23
S	A		2,089	914	0.13407	NS		-1,471	828	0.13407	NS		-7,917	755	0.13407	NS
	P		-28,166	9,876	0.13407	14.41		-					-22,976	5,588	0.13407	25.34
P	A	02347	-	1,848	0.13407	82.49	02348	-	1,548	0.13407	98.30	02349	-	1,373	0.13407	NS
	P		107,172					104,974								
	P		-42,632	22,727	0.13407	6.34		-38,286	24,040	0.13407	5.97		-35,634	19,165	0.13407	7.47
S	A		-1,852	824	0.13407	NS		2,087	852	0.13407	NS		4,467	840	0.13407	NS
	P		-27,254	9,746	0.13407	14.59		-29,755	11,094	0.13407	12.84		-30,589	10,278	0.13407	13.87
P	A	02350	-54,377	35,399	0.13407	4.11	02351	-	2,561	0.13407	59.49	02352	-	1,951	0.13407	77.93
	P		-10,531	651	0.13407	NS		106,434								
	P		-23,352	5,448	0.13407	26.00		-10,402	4,230	0.13407	33.09		-37,555	17,764	0.13407	8.08
S	A		-1,454	282	0.13407	NS		-9,787	788	0.13407	NS		-2,613	839	0.13407	NS
	P		-					-23,278	3,217	0.13407	44.03		-30,160	8,420	0.13407	16.93
P	A	02353	-	1,509	0.13407	NS	02354	-97,567	1,239	0.13407	NS	02355	-96,163	1,141	0.13407	NS
	P		100,815					-30,273	19,267	0.13407	7.40		-30,729	13,469	0.13407	10.59
	P		-32,568	22,123	0.13407	6.46		5,435	775	0.13407	NS		6,629	707	0.13407	NS
S	A		2,312	828	0.13407	NS		-34,701	10,378	0.13407	13.79		-33,402	8,547	0.13407	16.73
	P		-33,922	10,671	0.13407	13.40		-	2,154	0.13407	70.43	02358	-96,235	1,497	0.13407	NS
P	A	02356	-59,040	10,929	0.13407	13.38	02357	101,300								
	P		-9,207	2,005	0.13407	69.74		-31,199	11,400	0.13407	12.52		-24,755	18,606	0.13407	7.62
S	A		-15,670	892	0.13407	NS		-3,523	898	0.13407	NS		2,158	828	0.13407	NS
	P		-1,547	770	0.13407	NS		-33,341	6,598	0.13407	21.67		-40,085	9,497	0.13407	15.14
P	A	02359	-91,430	1,105	0.13407	NS	02360	-87,353	923	0.13407	NS	02361	-38,975	21,575	0.13407	6.66
	P		-22,597	17,659	0.13407	8.02		-23,212	12,585	0.13407	11.25		0	0	0.13407	-
S	A		5,522	705	0.13407	NS		7,984	563	0.13407	NS		-22,910	2,878	0.13407	49.20
	P		-41,133	9,541	0.13407	15.09		-38,446	7,607	0.13407	18.88		-1,155	215	0.13407	NS
P	A	02362	-99,912	2,517	0.13407	60.20	02363	-91,871	1,514	0.13407	99.40	02364	-84,210	962	0.13407	NS
	P		-23,647	4,519	0.13407	31.36		-15,206	13,837	0.13407	10.16		-12,283	14,424	0.13407	9.72
S	A		-3,739	1,025	0.13407	NS		2,230	856	0.13407	NS		5,276	615	0.13407	NS
	P		-35,233	4,225	0.13407	33.89		-48,094	7,171	0.13407	20.20		-51,258	7,199	0.13407	20.18
P	A	02365	-77,644	700	0.13407	NS	02366	-62,114	689	0.13407	NS	02367	-75,846	3,489	0.13407	42.54
	P		-14,025	10,646	0.13407	13.19		-18,306	5,865	0.13407	24.04		-4,781	1,201	0.13407	NS
S	A		7,329	392	0.13407	NS		8,628	224	0.13407	NS		-4,963	1,165	0.13407	NS
	P		-46,731	5,267	0.13407	27.47		242	3,888	0.13407	35.65		-31,468	2,012	0.13407	70.93
P	A	02368	-88,103	1,556	0.13407	96.40	02369	-76,490	791	0.13407	NS	02370	-66,522	463	0.13407	NS
	P		-5,264	8,439	0.13407	16.51		-1,107	9,684	0.13407	14.33		-1,762	6,898	0.13407	20.13
S	A		3,035	861	0.13407	NS		4,924	452	0.13407	NS		-63,313	185	0.13407	NS
	P		-56,249	3,692	0.13407	39.52		-3,585	2,233	0.13407	62.30		-3,544	2,903	0.13407	47.92
P	A	02371	-41,396	433	0.13407	NS	02372	-61,482	6,592	0.13407	22.24	02373	-83,202	1,579	0.13407	94.60
	P		-8,467	2,927	0.13407	47.74		5,951	337	0.13407	NS		2,348	3,529	0.13407	39.20
S	A		-44,979	3,176	0.13407	45.48		-5,334	1,192	0.13407	NS		-56,931	1,485	0.13407	98.31



Pareti - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	P		-2,782	3,639	0.13407	38.20		-23,220	561	0.13407	NS		-5,061	557	0.13407	NS
P	A	02374	-67,536	542	0.13407	NS	02375	-55,344	172	0.13407	NS	02376	7,857	1,618	0.13407	85.06
	P		5,587	4,107	0.13407	33.58		3,229	1,697	0.13407	81.45		4,979	1,550	0.13407	89.03
S	A	02377	-78,681	5,743	0.13407	25.91	02378	-82,089	10,537	0.13407	14.16	02379	-65,792	13,801	0.13407	10.66
	P		-6,093	785	0.13407	NS		-6,518	1,203	0.13407	NS		-5,904	1,929	0.13407	72.27
P	A	02377	-6,070	3,385	0.13407	41.19	02378	-43,078	1,645	0.13407	87.66	02379	280	1,905	0.13407	72.76
	P		-3,244	1,345	0.13407	NS		-1,097	256	0.13407	NS		902	331	0.13407	NS
S	A	02380	-37,481	15,024	0.13407	9.55	02381	-39,738	5,668	0.13407	25.37	02382	-89,314	18,104	0.13407	8.29
	P		-6,232	2,931	0.13407	47.58		0	0	0.13407	-		6,800	971	0.13407	NS
P	A	02380	4,047	4,671	0.13407	29.57	02381	14,584	6,958	0.13407	19.65	02382	20,463	8,982	0.13407	15.14
	P		4,810	271	0.13407	NS		9,554	244	0.13407	NS		23,456	226	0.13407	NS
S	A	02380	-	28,366	0.13407	5.35	02381	-94,226	33,738	0.13407	4.47	02382	-58,862	33,674	0.13407	4.34
	P		101,291	3,299	0.13407	NS		3,101	1,341	0.13407	NS		-1,721	1,449	0.13407	95.84

## LEGENDA Pareti - Verifiche pressoflessione retta allo stato limite ultimo

- D** Direzione [P] = principale - [S] = secondaria.  
**P** Posizione [A] = anteriore - [P] = posteriore.  
**N, M** Coppia N-M che dà origine alla massima armatura.  
**Af** Area delle armature per centimetro.  
**CS** Coefficienti di sicurezza: [NS] = Non Significativo - Per valori di CS maggiori o uguali a 100.

## Pareti - VERIFICHE A TAGLIO PER PRESSOFLESSIONE RETTA ALLO STATO LIMITE ULTIMO (Elevazione)

Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo											
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE	
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm <sup>2</sup> /cm]	
Piano Terra			Parete P1-P2-P3				Parete P1-P2				
00047	18,789	7.34	137,906	0	-52,152	0	0	0	0.00	0.1341	
00048	48,913	3.25	159,129	0	141,484	0	0	0	0.00	0.1341	
00054	113,678	1.25	141,754	0	25,653	0	0	0	2.50	0.1341	
00056	55,463	2.54	141,107	0	21,338	0	0	0	0.00	0.1341	
00057	42,944	3.33	143,109	0	34,686	0	0	0	0.00	0.1341	
00058	48,887	2.99	146,206	0	55,329	0	0	0	0.00	0.1341	
00059	62,670	2.47	154,588	0	111,213	0	0	0	0.00	0.1341	
00060	58,669	2.71	159,173	0	141,778	0	0	0	0.00	0.1341	
00061	50,421	2.98	150,037	0	80,873	0	0	0	0.00	0.1341	
00062	54,134	2.70	146,372	0	56,440	0	0	0	0.00	0.1341	
00063	49,227	3.11	153,125	0	101,455	0	0	0	0.00	0.1341	
00064	84,236	1.83	154,104	0	107,983	0	0	0	0.00	0.1341	
00137	46,183	2.99	137,906	0	-2,162	0	0	0	0.00	0.1341	
00379	49,409	2.83	139,979	0	13,818	0	0	0	0.00	0.1341	
00517	35,901	3.95	141,924	0	26,786	0	0	0	0.00	0.1341	
00518	21,669	6.65	144,026	0	40,797	0	0	0	0.00	0.1341	
00519	23,646	6.14	145,273	0	49,110	0	0	0	0.00	0.1341	
00520	11,649	11.99	139,673	0	11,776	0	0	0	0.00	0.1341	
00521	10,121	13.80	139,675	0	11,794	0	0	0	0.00	0.1341	
00522	12,068	11.60	139,972	0	13,768	0	0	0	0.00	0.1341	
00523	24,276	6.40	155,436	0	116,863	0	0	0	0.00	0.1341	
00524	37,571	4.25	159,686	0	145,198	0	0	0	0.00	0.1341	
00541	71,359	1.93	137,906	0	-139,268	0	0	0	0.00	0.1341	
00542	26,619	5.18	137,906	0	-45,727	0	0	0	0.00	0.1341	
00543	29,905	4.61	137,906	0	-28,004	0	0	0	0.00	0.1341	
00544	33,719	4.23	142,537	0	30,874	0	0	0	0.00	0.1341	
00545	33,202	4.45	147,686	0	65,198	0	0	0	0.00	0.1341	
00546	48,208	3.10	149,432	0	76,836	0	0	0	0.00	0.1341	
00547	40,585	3.74	151,869	0	93,086	0	0	0	0.00	0.1341	
00548	48,409	3.23	156,221	0	122,095	0	0	0	0.00	0.1341	
00587	64,221	2.50	160,547	0	150,935	0	0	0	0.00	0.1341	
00588	51,079	2.95	150,794	0	85,915	0	0	0	0.00	0.1341	
00589	45,494	3.34	152,164	0	95,050	0	0	0	0.00	0.1341	
00590	47,435	3.20	151,896	0	93,262	0	0	0	0.00	0.1341	
00591	49,214	3.11	152,837	0	99,537	0	0	0	0.00	0.1341	
00592	52,520	2.92	153,240	0	102,224	0	0	0	0.00	0.1341	
00593	56,450	2.74	154,449	0	110,281	0	0	0	0.00	0.1341	
00594	57,218	2.72	155,719	0	118,751	0	0	0	0.00	0.1341	
00595	59,839	2.61	155,903	0	119,979	0	0	0	0.00	0.1341	
00596	60,917	2.59	157,536	0	130,865	0	0	0	0.00	0.1341	
00597	57,817	2.74	158,435	0	136,858	0	0	0	0.00	0.1341	
01043	60,817	2.45	148,761	0	72,365	0	0	0	0.00	0.1341	
01044	56,356	2.72	153,323	0	102,780	0	0	0	0.00	0.1341	
01047	56,467	2.69	152,121	0	94,764	0	0	0	0.00	0.1341	
01048	53,624	2.86	153,423	0	103,446	0	0	0	0.00	0.1341	
01051	79,395	1.89	149,882	0	79,837	0	0	0	0.00	0.1341	
01052	63,955	2.58	165,196	0	181,932	0	0	0	0.00	0.1341	
01055	45,272	3.15	142,418	0	30,077	0	0	0	0.00	0.1341	
01056	43,598	3.36	146,419	0	56,754	0	0	0	0.00	0.1341	



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm <sup>2</sup> /cm]
02426	16,444	8.39	137,906	0	-17,152	0	0	0	0.00	0.1341
02427	40,824	3.46	141,288	0	22,542	0	0	0	0.00	0.1341
02428	44,634	3.09	137,906	0	-39,143	0	0	0	0.00	0.1341
02429	54,415	2.89	157,189	0	128,553	0	0	0	0.00	0.1341
02430	62,193	2.51	156,248	0	122,276	0	0	0	0.00	0.1341
02431	58,607	2.59	151,503	0	90,644	0	0	0	0.00	0.1341
02432	54,597	2.69	146,866	0	59,730	0	0	0	0.00	0.1341
02433	41,719	3.31	137,906	0	-22,593	0	0	0	0.00	0.1341
02434	22,120	6.46	142,926	0	33,467	0	0	0	0.00	0.1341
02435	66,389	2.31	153,276	0	102,465	0	0	0	0.00	0.1341
02436	66,166	2.26	149,659	0	78,349	0	0	0	0.00	0.1341
02437	54,903	2.67	146,583	0	57,845	0	0	0	0.00	0.1341
02438	29,440	4.98	146,723	0	58,780	0	0	0	0.00	0.1341
02439	61,229	2.52	154,162	0	108,373	0	0	0	0.00	0.1341
02440	65,370	2.32	151,431	0	90,164	0	0	0	0.00	0.1341
02441	63,058	2.36	148,914	0	73,381	0	0	0	0.00	0.1341
02442	55,210	2.68	148,165	0	68,388	0	0	0	0.00	0.1341
02443	39,263	3.84	150,743	0	85,575	0	0	0	0.00	0.1341
02444	57,899	2.63	152,347	0	96,273	0	0	0	0.00	0.1341
02445	59,047	2.55	150,377	0	83,139	0	0	0	0.00	0.1341
02446	57,519	2.59	148,905	0	73,325	0	0	0	0.00	0.1341
02447	58,464	2.59	151,175	0	88,460	0	0	0	0.00	0.1341
02448	50,490	3.02	152,562	0	97,702	0	0	0	0.00	0.1341
02449	50,541	3.00	151,508	0	90,680	0	0	0	0.00	0.1341
02450	49,246	3.04	149,644	0	78,250	0	0	0	0.00	0.1341
02451	52,120	2.85	148,678	0	71,811	0	0	0	0.00	0.1341
02452	58,978	2.56	150,958	0	87,010	0	0	0	0.00	0.1341
02453	42,945	3.56	152,690	0	98,555	0	0	0	0.00	0.1341
02454	39,278	3.83	150,628	0	84,814	0	0	0	0.00	0.1341
02455	40,047	3.71	148,684	0	71,848	0	0	0	0.00	0.1341
02456	51,756	2.85	147,727	0	65,469	0	0	0	0.00	0.1341
02457	36,130	3.82	137,906	0	-71,774	0	0	0	0.00	0.1341
02458	29,694	4.64	137,906	0	-23,012	0	0	0	0.00	0.1341
02459	33,897	4.39	148,878	0	73,141	0	0	0	0.00	0.1341
02460	43,937	3.36	147,794	0	65,917	0	0	0	0.00	0.1341
02461	53,899	2.71	146,124	0	54,782	0	0	0	0.00	0.1341
Piano Terra			Parete P1-P2-P3				Parete P2-P3			
00040	52,047	2.68	139,454	0	10,318	0	0	0	0.00	0.1341
00041	55,246	2.50	137,906	0	-5,164	0	0	0	0.00	0.1341
00042	61,230	2.25	137,906	0	-22,196	0	0	0	0.00	0.1341
00043	67,083	2.06	137,906	0	-15,887	0	0	0	0.00	0.1341
00044	69,926	2.02	141,234	0	22,187	0	0	0	0.00	0.1341
00045	73,376	2.08	152,270	0	95,756	0	0	0	0.00	0.1341
00046	74,230	2.06	152,946	0	100,262	0	0	0	0.00	0.1341
00047	290,312	2.83	821,056	2,107,350	-47,051	0	0	0	2.50	0.1341
00055	61,659	2.52	155,588	0	117,877	0	0	0	0.00	0.1341
00137	22,264	6.25	139,229	0	8,819	0	0	0	0.00	0.1341
00139	3,954	34.88	137,906	0	-4,835	0	0	0	0.00	0.1341
00182	161,955	1.12	181,882	0	293,169	0	0	0	0.00	0.1341
00416	45,782	3.31	151,731	0	92,162	0	0	0	0.00	0.1341
00517	17,483	7.90	138,193	0	1,914	0	0	0	0.00	0.1341
00518	26,135	5.33	139,186	0	8,528	0	0	0	0.00	0.1341
00519	39,620	3.49	138,183	0	1,842	0	0	0	0.00	0.1341
00520	36,500	3.78	137,906	0	-13,610	0	0	0	0.00	0.1341
00521	38,404	3.62	138,920	0	6,757	0	0	0	0.00	0.1341
00522	61,126	2.26	137,906	0	-21,517	0	0	0	0.00	0.1341
00523	51,812	2.66	137,906	0	-36,224	0	0	0	0.00	0.1341
00524	97,495	1.46	142,704	0	31,983	0	0	0	2.50	0.1341
00549	29,276	4.80	140,630	0	18,160	0	0	0	0.00	0.1341
00550	21,018	6.56	137,906	0	-14,369	0	0	0	0.00	0.1341
00551	8,424	16.69	140,611	0	18,028	0	0	0	0.00	0.1341
00552	9,564	14.81	141,604	0	24,648	0	0	0	0.00	0.1341
00553	7,224	19.09	137,906	0	-8,593	0	0	0	0.00	0.1341
00554	8,031	17.17	137,906	0	-6,451	0	0	0	0.00	0.1341
00555	11,528	11.96	137,906	0	-10,666	0	0	0	0.00	0.1341
00556	8,770	15.72	137,906	0	-18,273	0	0	0	0.00	0.1341
00963	59,886	2.30	137,906	0	-11,247	0	0	0	0.00	0.1341
00965	57,707	2.39	137,906	0	-16,723	0	0	0	0.00	0.1341
00966	35,018	3.97	139,181	0	8,498	0	0	0	0.00	0.1341
00968	48,194	2.86	137,906	0	-1,998	0	0	0	0.00	0.1341
00971	38,948	3.54	137,906	0	-1,623	0	0	0	0.00	0.1341
00973	55,154	2.61	143,743	0	38,914	0	0	0	0.00	0.1341
00975	42,705	3.32	141,664	0	25,051	0	0	0	0.00	0.1341
01011	4,626	30.13	139,361	0	9,698	0	0	0	0.00	0.1341
01012	9,798	14.44	141,455	0	23,655	0	0	0	0.00	0.1341
01013	21,812	6.66	145,269	0	49,086	0	0	0	0.00	0.1341
01014	24,104	6.07	146,418	0	56,744	0	0	0	0.00	0.1341



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm <sup>2</sup> /cm]
01015	28,180	5.21	146,868	0	59,746	0	0	0	0.00	0.1341
01016	38,805	3.84	148,952	0	73,640	0	0	0	0.00	0.1341
01017	36,504	4.07	148,447	0	70,270	0	0	0	0.00	0.1341
01018	42,340	3.44	145,655	0	51,656	0	0	0	0.00	0.1341
01019	55,802	2.54	141,832	0	26,170	0	0	0	0.00	0.1341
02173	9,690	14.50	140,503	0	17,309	0	0	0	0.00	0.1341
02174	25,751	5.55	142,897	0	33,269	0	0	0	0.00	0.1341
02175	21,551	6.45	138,952	0	6,972	0	0	0	0.00	0.1341
02176	167,143	5.05	844,018	2,076,975	147,975	0	0	0	2.50	0.1341
02177	94,991	1.54	145,855	0	52,991	0	0	0	2.50	0.1341
02178	83,398	1.65	137,906	0	-29,406	0	0	0	0.00	0.1341
02179	69,929	1.97	137,906	0	-10,809	0	0	0	0.00	0.1341
02180	57,505	2.42	138,891	0	6,561	0	0	0	0.00	0.1341
02181	41,721	3.35	139,583	0	11,177	0	0	0	0.00	0.1341
02182	72,836	2.00	145,672	0	51,773	0	0	0	0.00	0.1341
02183	55,665	2.60	144,452	0	43,637	0	0	0	0.00	0.1341
02184	45,896	3.00	137,906	0	-10,206	0	0	0	0.00	0.1341
02185	35,074	3.93	137,906	0	-2,916	0	0	0	0.00	0.1341
02186	55,022	2.65	145,874	0	53,120	0	0	0	0.00	0.1341
02187	47,807	3.01	143,746	0	38,930	0	0	0	0.00	0.1341
02188	37,209	3.83	142,455	0	30,326	0	0	0	0.00	0.1341
02189	29,443	4.80	141,215	0	22,056	0	0	0	0.00	0.1341
02190	30,482	4.52	137,906	0	-4,085	0	0	0	0.00	0.1341
02191	41,920	3.42	143,527	0	37,468	0	0	0	0.00	0.1341
02192	30,485	4.66	142,108	0	28,011	0	0	0	0.00	0.1341
02193	23,706	5.94	140,899	0	19,948	0	0	0	0.00	0.1341
02194	22,061	6.40	141,162	0	21,701	0	0	0	0.00	0.1341
02195	28,163	5.08	142,951	0	33,634	0	0	0	0.00	0.1341
02196	22,053	6.46	142,572	0	31,101	0	0	0	0.00	0.1341
02197	21,224	6.68	141,721	0	25,434	0	0	0	0.00	0.1341
02198	18,007	7.80	140,448	0	16,947	0	0	0	0.00	0.1341
02199	20,834	6.95	144,791	0	45,897	0	0	0	0.00	0.1341
02200	13,467	10.56	142,152	0	28,301	0	0	0	0.00	0.1341
02201	13,592	10.51	142,902	0	33,303	0	0	0	0.00	0.1341
02202	19,954	7.06	140,800	0	19,291	0	0	0	0.00	0.1341
02203	16,676	8.27	137,906	0	-12,471	0	0	0	0.00	0.1341
Piano Terra			PareteP4-P5-P6				Parete P4-P5			
00004	46,133	3.45	159,274	0	142,453	0	0	0	0.00	0.1341
00051	108,414	1.30	141,133	0	21,508	0	0	0	2.50	0.1341
00052	40,270	3.55	143,136	0	34,866	0	0	0	0.00	0.1341
00094	47,277	3.07	145,116	0	48,064	0	0	0	0.00	0.1341
00095	44,335	3.27	144,883	0	46,511	0	0	0	0.00	0.1341
00096	43,029	3.36	144,630	0	44,822	0	0	0	0.00	0.1341
00097	58,849	2.57	150,995	0	87,257	0	0	0	0.00	0.1341
00098	62,448	2.50	155,858	0	119,675	0	0	0	0.00	0.1341
00099	54,179	2.74	148,196	0	68,596	0	0	0	0.00	0.1341
00100	64,615	2.25	145,417	0	50,070	0	0	0	0.00	0.1341
00101	85,889	1.75	150,595	0	84,591	0	0	0	0.00	0.1341
00102	77,075	2.05	157,870	0	133,093	0	0	0	0.00	0.1341
00509	24,817	5.56	137,906	0	-90,158	0	0	0	0.00	0.1341
00510	13,758	10.02	137,906	0	-17,989	0	0	0	0.00	0.1341
00511	17,596	7.95	139,899	0	13,281	0	0	0	0.00	0.1341
00512	15,224	9.32	141,953	0	26,977	0	0	0	0.00	0.1341
00513	19,238	7.64	146,941	0	60,232	0	0	0	0.00	0.1341
00514	32,534	4.53	147,316	0	62,730	0	0	0	0.00	0.1341
00515	29,274	5.03	147,260	0	62,355	0	0	0	0.00	0.1341
00516	32,406	4.51	146,212	0	55,370	0	0	0	0.00	0.1341
00533	51,419	3.05	156,747	0	125,604	0	0	0	0.00	0.1341
00534	35,611	4.30	152,973	0	100,443	0	0	0	0.00	0.1341
00535	48,764	3.11	151,787	0	92,535	0	0	0	0.00	0.1341
00536	33,116	4.42	146,386	0	56,531	0	0	0	0.00	0.1341
00537	33,050	4.37	144,549	0	44,284	0	0	0	0.00	0.1341
00538	31,072	4.44	137,906	0	-31,262	0	0	0	0.00	0.1341
00539	30,342	4.55	137,906	0	-49,747	0	0	0	0.00	0.1341
00540	75,042	1.84	137,906	0	-127,811	0	0	0	0.00	0.1341
00598	59,115	2.68	158,557	0	137,674	0	0	0	0.00	0.1341
00599	62,947	2.50	157,510	0	130,688	0	0	0	0.00	0.1341
00600	62,354	2.50	155,913	0	120,043	0	0	0	0.00	0.1341
00601	60,277	2.58	155,668	0	118,411	0	0	0	0.00	0.1341
00602	59,762	2.58	154,317	0	109,401	0	0	0	0.00	0.1341
00603	56,597	2.71	153,124	0	101,451	0	0	0	0.00	0.1341
00604	53,737	2.84	152,608	0	98,014	0	0	0	0.00	0.1341
00605	52,033	2.91	151,377	0	89,805	0	0	0	0.00	0.1341
00606	50,577	2.99	151,444	0	90,248	0	0	0	0.00	0.1341
00607	54,570	2.75	149,965	0	80,390	0	0	0	0.00	0.1341
00608	66,076	2.39	158,171	0	135,096	0	0	0	0.00	0.1341
00947	30,347	5.05	153,367	0	103,072	0	0	0	0.00	0.1341



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm/cm]
00948	49,239	3.27	161,197	0	155,271	0	0	0	0.00	0.1341
00951	43,139	3.35	144,304	0	42,651	0	0	0	0.00	0.1341
00953	41,551	3.53	146,679	0	58,485	0	0	0	0.00	0.1341
00955	68,325	2.24	153,242	0	102,237	0	0	0	0.00	0.1341
00957	54,758	2.77	151,440	0	90,227	0	0	0	0.00	0.1341
00958	56,451	2.63	148,463	0	70,375	0	0	0	0.00	0.1341
00961	61,434	2.46	151,114	0	88,049	0	0	0	0.00	0.1341
02462	21,091	6.54	137,906	0	-35,723	0	0	0	0.00	0.1341
02463	37,663	3.89	146,326	0	56,128	0	0	0	0.00	0.1341
02464	50,116	2.75	137,906	0	-29,718	0	0	0	0.00	0.1341
02465	54,937	2.86	157,361	0	129,699	0	0	0	0.00	0.1341
02466	65,150	2.39	155,785	0	119,191	0	0	0	0.00	0.1341
02467	65,939	2.30	151,540	0	90,890	0	0	0	0.00	0.1341
02468	56,575	2.60	147,241	0	62,231	0	0	0	0.00	0.1341
02469	42,528	3.24	137,906	0	-23,607	0	0	0	0.00	0.1341
02470	19,728	6.99	137,906	0	-4,335	0	0	0	0.00	0.1341
02471	68,663	2.23	153,285	0	102,523	0	0	0	0.00	0.1341
02472	68,012	2.20	149,727	0	78,803	0	0	0	0.00	0.1341
02473	56,921	2.58	146,606	0	57,998	0	0	0	0.00	0.1341
02474	31,607	4.65	146,829	0	59,482	0	0	0	0.00	0.1341
02475	64,536	2.39	154,114	0	108,048	0	0	0	0.00	0.1341
02476	68,730	2.20	151,534	0	90,853	0	0	0	0.00	0.1341
02477	66,115	2.25	149,024	0	74,119	0	0	0	0.00	0.1341
02478	58,052	2.55	148,022	0	67,439	0	0	0	0.00	0.1341
02479	44,001	3.42	150,518	0	84,075	0	0	0	0.00	0.1341
02480	62,513	2.44	152,325	0	96,127	0	0	0	0.00	0.1341
02481	63,822	2.36	150,547	0	84,268	0	0	0	0.00	0.1341
02482	61,459	2.43	149,062	0	74,369	0	0	0	0.00	0.1341
02483	61,951	2.43	150,284	0	82,519	0	0	0	0.00	0.1341
02484	55,885	2.72	152,185	0	95,190	0	0	0	0.00	0.1341
02485	57,212	2.65	151,537	0	90,868	0	0	0	0.00	0.1341
02486	55,559	2.70	150,008	0	80,679	0	0	0	0.00	0.1341
02487	55,365	2.69	149,021	0	74,096	0	0	0	0.00	0.1341
02488	58,752	2.54	149,403	0	76,645	0	0	0	0.00	0.1341
02489	50,537	3.01	152,218	0	95,412	0	0	0	0.00	0.1341
02490	48,389	3.12	150,842	0	86,240	0	0	0	0.00	0.1341
02491	47,351	3.16	149,452	0	76,971	0	0	0	0.00	0.1341
02492	50,943	2.91	148,166	0	68,395	0	0	0	0.00	0.1341
02493	39,671	3.48	137,906	0	-75,639	0	0	0	0.00	0.1341
02494	34,004	4.06	137,906	0	-23,839	0	0	0	0.00	0.1341
02495	44,502	3.36	149,611	0	78,028	0	0	0	0.00	0.1341
02496	51,472	2.90	149,323	0	76,110	0	0	0	0.00	0.1341
02497	51,255	2.90	148,753	0	72,309	0	0	0	0.00	0.1341
02498	16,224	8.50	137,906	0	-63,770	0	0	0	0.00	0.1341
Piano Terra			PareteP4-P5-P6			Parete P5-P6				
00005	36,818	3.87	142,497	0	30,601	0	0	0	0.00	0.1341
00006	29,993	4.70	140,971	0	20,430	0	0	0	0.00	0.1341
00007	43,999	3.19	140,450	0	16,955	0	0	0	0.00	0.1341
00008	58,605	2.37	138,935	0	6,855	0	0	0	0.00	0.1341
00009	66,050	2.12	139,809	0	12,682	0	0	0	0.00	0.1341
00010	72,764	1.94	141,136	0	21,531	0	0	0	0.00	0.1341
00011	49,880	3.02	150,870	0	86,424	0	0	0	0.00	0.1341
00052	23,264	6.35	147,692	0	65,235	0	0	0	0.00	0.1341
00053	86,628	1.62	140,695	0	18,591	0	0	0	2.50	0.1341
00138	2,837	49.07	139,206	0	8,667	0	0	0	0.00	0.1341
00183	143,044	1.20	172,142	0	228,235	0	0	0	0.00	0.1341
00418	34,807	4.06	141,401	0	23,299	0	0	0	0.00	0.1341
00509	85,754	1.66	142,413	0	30,047	0	0	0	0.00	0.1341
00510	46,639	2.96	137,906	0	-39,454	0	0	0	0.00	0.1341
00511	55,602	2.48	137,906	0	-22,781	0	0	0	0.00	0.1341
00512	33,120	4.20	138,954	0	6,981	0	0	0	0.00	0.1341
00513	31,444	4.39	137,906	0	-9,702	0	0	0	0.00	0.1341
00514	35,630	3.91	139,198	0	8,614	0	0	0	0.00	0.1341
00515	25,775	5.45	140,544	0	17,586	0	0	0	0.00	0.1341
00516	24,440	5.71	139,462	0	10,373	0	0	0	0.00	0.1341
00525	5,750	24.86	142,973	0	33,777	0	0	0	0.00	0.1341
00526	6,750	20.43	137,906	0	-11,406	0	0	0	0.00	0.1341
00527	4,009	35.50	142,309	0	29,353	0	0	0	0.00	0.1341
00528	6,407	22.45	143,830	0	39,488	0	0	0	0.00	0.1341
00529	12,077	11.70	141,262	0	22,372	0	0	0	0.00	0.1341
00530	9,216	15.15	139,615	0	11,389	0	0	0	0.00	0.1341
00531	23,411	5.89	137,906	0	-15,235	0	0	0	0.00	0.1341
00532	34,902	3.95	137,906	0	-35,182	0	0	0	0.00	0.1341
01020	6,631	21.07	139,734	0	12,184	0	0	0	0.00	0.1341
01021	11,682	12.14	141,850	0	26,289	0	0	0	0.00	0.1341
01022	24,533	5.89	144,621	0	44,762	0	0	0	0.00	0.1341
01023	25,698	5.67	145,818	0	52,741	0	0	0	0.00	0.1341



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm/cm]
01024	29,157	5.01	145,998	0	53,947	0	0	0	0.00	0.1341
01025	38,351	3.86	148,135	0	68,192	0	0	0	0.00	0.1341
01026	34,459	4.28	147,649	0	64,951	0	0	0	0.00	0.1341
01027	39,886	3.64	145,104	0	47,984	0	0	0	0.00	0.1341
01028	49,375	2.89	142,573	0	31,113	0	0	0	0.00	0.1341
01030	42,276	3.30	139,449	0	10,284	0	0	0	0.00	0.1341
01032	30,981	4.53	140,233	0	15,512	0	0	0	0.00	0.1341
01033	66,037	2.17	143,072	0	34,436	0	0	0	0.00	0.1341
01036	43,572	3.22	140,362	0	16,373	0	0	0	0.00	0.1341
01037	75,939	1.91	145,289	0	49,219	0	0	0	0.00	0.1341
01040	65,580	2.22	145,540	0	50,890	0	0	0	0.00	0.1341
01918	11,670	12.03	140,394	0	16,582	0	0	0	0.00	0.1341
01919	42,121	3.32	139,774	0	12,448	0	0	0	0.00	0.1341
01920	32,079	4.37	140,063	0	14,379	0	0	0	0.00	0.1341
01921	146,802	1.07	156,638	0	124,877	0	0	0	2.50	0.1341
01922	87,140	1.67	145,234	0	48,852	0	0	0	0.00	0.1341
01923	77,381	1.78	137,906	0	-30,609	0	0	0	0.00	0.1341
01924	63,554	2.17	137,906	0	-8,956	0	0	0	0.00	0.1341
01925	52,591	2.66	139,928	0	13,477	0	0	0	0.00	0.1341
01926	43,383	3.28	142,197	0	28,602	0	0	0	0.00	0.1341
01927	68,466	2.12	145,264	0	49,048	0	0	0	0.00	0.1341
01928	51,631	2.80	144,654	0	44,981	0	0	0	0.00	0.1341
01929	39,576	3.48	137,906	0	-6,147	0	0	0	0.00	0.1341
01930	29,265	4.79	140,204	0	15,318	0	0	0	0.00	0.1341
01931	54,772	2.65	145,409	0	50,015	0	0	0	0.00	0.1341
01932	47,634	3.01	143,606	0	37,998	0	0	0	0.00	0.1341
01933	36,122	3.96	142,995	0	33,922	0	0	0	0.00	0.1341
01934	23,518	5.86	137,906	0	-6,310	0	0	0	0.00	0.1341
01935	23,532	5.98	140,792	0	19,237	0	0	0	0.00	0.1341
01936	44,773	3.20	143,237	0	35,539	0	0	0	0.00	0.1341
01937	33,756	4.21	142,248	0	28,942	0	0	0	0.00	0.1341
01938	25,375	5.58	141,536	0	24,198	0	0	0	0.00	0.1341
01939	17,423	8.16	142,106	0	27,998	0	0	0	0.00	0.1341
01940	32,702	4.36	142,576	0	31,130	0	0	0	0.00	0.1341
01941	26,727	5.32	142,281	0	29,162	0	0	0	0.00	0.1341
01942	26,182	5.40	141,493	0	23,911	0	0	0	0.00	0.1341
01943	19,963	7.01	139,943	0	13,579	0	0	0	0.00	0.1341
01944	17,666	8.01	141,462	0	23,704	0	0	0	0.00	0.1341
01945	16,731	8.50	142,269	0	29,083	0	0	0	0.00	0.1341
01946	15,694	9.06	142,224	0	28,783	0	0	0	0.00	0.1341
01947	23,833	5.90	140,586	0	17,867	0	0	0	0.00	0.1341
01948	16,792	8.21	137,906	0	-24,249	0	0	0	0.00	0.1341
02498	283,914	2.89	821,056	2,004,075	-73,729	0	0	0	2.50	0.1341
Piano Terra			PareteP1-P4			Parete P1-P4				
00004	35,883	4.42	158,633	0	138,177	0	0	0	0.00	0.1341
00048	33,739	4.69	158,369	0	136,420	0	0	0	0.00	0.1341
00051	185,588	4.42	821,056	1,818,788	-91,522	0	0	0	2.50	0.1341
00054	174,660	4.70	821,056	1,859,288	-108,951	0	0	0	2.50	0.1341
00103	162,300	5.17	839,465	2,107,350	118,639	0	0	0	2.50	0.1341
00104	195,962	4.19	821,056	2,107,350	-86,692	0	0	0	2.50	0.1341
00105	187,522	4.38	821,056	2,107,350	-82,510	0	0	0	2.50	0.1341
00106	164,975	5.03	829,874	2,107,350	56,825	0	0	0	2.50	0.1341
00107	210,250	3.93	825,555	2,107,350	28,992	0	0	0	2.50	0.1341
00108	155,057	5.34	827,453	2,107,350	41,224	0	0	0	2.50	0.1341
00109	170,614	4.81	821,056	2,107,350	-16,224	0	0	0	2.50	0.1341
00110	120,617	1.14	137,906	0	-25,386	0	0	0	2.50	0.1341
00111	144,243	5.69	821,056	2,100,263	-28,417	0	0	0	2.50	0.1341
00112	128,396	1.07	137,906	0	-63,551	0	0	0	2.50	0.1341
00113	105,404	1.31	138,513	0	4,046	0	0	0	2.50	0.1341
00114	78,178	1.76	137,906	0	-10,527	0	0	0	0.00	0.1341
00115	77,815	1.77	137,906	0	-15,159	0	0	0	0.00	0.1341
00116	40,906	3.37	137,906	0	-1,438	0	0	0	0.00	0.1341
00117	97,747	1.42	138,766	0	5,733	0	0	0	2.50	0.1341
00118	123,946	1.11	137,906	0	-66,155	0	0	0	2.50	0.1341
00119	140,609	5.84	821,056	2,076,975	-39,613	0	0	0	2.50	0.1341
00120	121,636	1.13	137,906	0	-68,850	0	0	0	2.50	0.1341
00121	152,949	5.37	821,056	2,107,350	-13,592	0	0	0	2.50	0.1341
00122	144,802	5.70	825,449	2,107,350	28,311	0	0	0	2.50	0.1341
00123	203,838	4.05	826,301	2,107,350	33,799	0	0	0	2.50	0.1341
00124	167,220	4.96	829,921	2,107,350	57,129	0	0	0	2.50	0.1341
00125	190,820	4.30	821,056	2,070,900	-84,817	0	0	0	2.50	0.1341
00126	214,798	3.82	821,056	2,107,350	-59,523	0	0	0	2.50	0.1341
00127	142,582	5.76	821,056	2,107,350	-91,154	0	0	0	2.50	0.1341
00128	163,916	5.01	821,056	2,107,350	-116,888	0	0	0	2.50	0.1341
00415	162,670	5.05	821,056	2,107,350	-73,135	0	0	0	2.50	0.1341
00430	46,001	3.38	155,563	0	117,713	0	0	0	0.00	0.1341
00431	41,743	3.69	154,059	0	107,683	0	0	0	0.00	0.1341



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm <sup>2</sup> /cm]
00432	43,571	3.53	153,937	0	106,873	0	0	0	0.00	0.1341
00433	46,384	3.29	152,822	0	99,438	0	0	0	0.00	0.1341
00434	46,897	3.22	151,148	0	88,279	0	0	0	0.00	0.1341
00435	47,853	3.15	150,654	0	84,982	0	0	0	0.00	0.1341
00436	48,239	3.10	149,766	0	79,062	0	0	0	0.00	0.1341
00437	47,804	3.10	148,034	0	67,518	0	0	0	0.00	0.1341
00438	45,994	3.21	147,477	0	63,807	0	0	0	0.00	0.1341
00439	43,054	3.41	146,810	0	59,360	0	0	0	0.00	0.1341
00440	40,591	3.59	145,629	0	51,486	0	0	0	0.00	0.1341
00441	36,383	3.99	145,080	0	47,825	0	0	0	0.00	0.1341
00442	30,825	4.69	144,689	0	45,218	0	0	0	0.00	0.1341
00443	24,831	5.81	144,299	0	42,616	0	0	0	0.00	0.1341
00444	19,010	7.58	144,086	0	41,199	0	0	0	0.00	0.1341
00445	13,549	10.59	143,446	0	36,934	0	0	0	0.00	0.1341
00446	6,666	21.53	143,499	0	37,283	0	0	0	0.00	0.1341
00447	4,985	28.29	141,022	0	20,774	0	0	0	0.00	0.1341
00448	5,467	26.25	143,490	0	37,227	0	0	0	0.00	0.1341
00449	12,668	11.34	143,627	0	38,137	0	0	0	0.00	0.1341
00450	19,414	7.41	143,860	0	39,689	0	0	0	0.00	0.1341
00451	23,966	6.02	144,334	0	42,853	0	0	0	0.00	0.1341
00452	29,841	4.85	144,678	0	45,145	0	0	0	0.00	0.1341
00453	35,158	4.12	144,981	0	47,162	0	0	0	0.00	0.1341
00454	38,660	3.78	146,114	0	54,717	0	0	0	0.00	0.1341
00455	42,192	3.48	146,741	0	58,898	0	0	0	0.00	0.1341
00456	44,964	3.27	147,124	0	61,449	0	0	0	0.00	0.1341
00457	47,109	3.16	148,744	0	72,251	0	0	0	0.00	0.1341
00458	47,746	3.14	149,709	0	78,684	0	0	0	0.00	0.1341
00459	47,185	3.18	150,156	0	81,666	0	0	0	0.00	0.1341
00460	47,533	3.19	151,716	0	92,061	0	0	0	0.00	0.1341
00461	46,040	3.32	152,880	0	99,825	0	0	0	0.00	0.1341
00462	43,354	3.53	153,226	0	102,134	0	0	0	0.00	0.1341
00463	42,649	3.62	154,290	0	109,227	0	0	0	0.00	0.1341
00464	44,349	3.50	155,421	0	116,766	0	0	0	0.00	0.1341
00533	37,540	4.07	152,931	0	100,161	0	0	0	0.00	0.1341
00534	39,502	3.83	151,306	0	89,333	0	0	0	0.00	0.1341
00535	40,302	3.70	149,023	0	74,113	0	0	0	0.00	0.1341
00536	33,456	4.41	147,635	0	64,860	0	0	0	0.00	0.1341
00537	32,299	4.48	144,816	0	46,067	0	0	0	0.00	0.1341
00538	26,569	5.27	140,053	0	14,314	0	0	0	0.00	0.1341
00539	37,217	3.80	141,594	0	24,587	0	0	0	0.00	0.1341
00540	37,478	3.68	137,906	0	-53,652	0	0	0	0.00	0.1341
00541	66,142	2.09	137,906	0	-135,069	0	0	0	0.00	0.1341
00542	23,606	5.98	141,098	0	21,278	0	0	0	0.00	0.1341
00543	31,004	4.61	142,957	0	33,671	0	0	0	0.00	0.1341
00544	27,301	5.18	141,410	0	23,356	0	0	0	0.00	0.1341
00545	34,524	4.30	148,409	0	70,016	0	0	0	0.00	0.1341
00546	34,696	4.28	148,437	0	70,205	0	0	0	0.00	0.1341
00547	36,746	4.08	149,959	0	80,348	0	0	0	0.00	0.1341
00548	33,115	4.63	153,363	0	103,044	0	0	0	0.00	0.1341
00891	159,074	5.24	833,914	2,107,350	82,863	0	0	0	2.50	0.1341
00892	156,637	5.24	821,056	2,009,138	-46,702	0	0	0	2.50	0.1341
00894	179,664	4.57	821,056	2,071,913	-47,258	0	0	0	2.50	0.1341
00896	111,341	1.25	139,503	0	10,647	0	0	0	2.50	0.1341
00898	64,046	2.23	143,071	0	34,432	0	0	0	0.00	0.1341
00901	157,332	5.29	831,648	2,107,350	68,257	0	0	0	2.50	0.1341
00902	127,936	1.13	144,767	0	45,739	0	0	0	2.50	0.1341
00904	146,350	5.61	821,056	2,107,350	-5,430	0	0	0	2.50	0.1341
00906	195,096	4.21	821,056	2,107,350	-40,688	0	0	0	2.50	0.1341
00909	167,966	4.89	821,056	2,046,600	-43,452	0	0	0	2.50	0.1341
00910	190,489	4.31	821,056	2,107,350	-18,748	0	0	0	2.50	0.1341
00912	150,156	5.49	823,831	2,107,350	17,883	0	0	0	2.50	0.1341
00914	202,414	4.06	821,056	2,107,350	-59,428	0	0	0	2.50	0.1341
00917	91,090	1.51	137,906	0	-20,043	0	0	0	2.50	0.1341
00918	98,947	1.40	138,531	0	4,167	0	0	0	2.50	0.1341
00921	31,410	4.41	138,369	0	3,083	0	0	0	0.00	0.1341
00922	26,685	5.18	138,289	0	2,548	0	0	0	0.00	0.1341
00923	64,729	2.17	140,415	0	16,722	0	0	0	0.00	0.1341
00924	38,078	3.62	137,906	0	-12,298	0	0	0	0.00	0.1341
00928	82,884	1.72	142,938	0	33,546	0	0	0	0.00	0.1341
00930	148,635	5.52	821,056	1,968,638	-52,465	0	0	0	2.50	0.1341
00932	190,716	4.31	821,056	2,107,350	-32,739	0	0	0	2.50	0.1341
00935	133,547	1.05	140,292	0	15,906	0	0	0	2.50	0.1341
00936	139,500	1.04	145,606	0	51,328	0	0	0	2.50	0.1341
00939	207,975	3.95	821,056	2,107,350	-973	0	0	0	2.50	0.1341
00940	146,222	5.63	823,189	2,107,350	13,749	0	0	0	2.50	0.1341
00943	175,544	4.72	827,909	2,107,350	44,161	0	0	0	2.50	0.1341
00944	188,499	4.36	821,056	2,107,350	-14,692	0	0	0	2.50	0.1341



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm <sup>2</sup> /cm]
01949	40,528	3.81	154,566	0	111,063	0	0	0	0.00	0.1341
01950	116,017	1.19	137,906	0	-25,539	0	0	0	2.50	0.1341
01951	109,930	1.31	143,775	0	39,121	0	0	0	2.50	0.1341
01952	36,494	4.25	155,149	0	114,954	0	0	0	0.00	0.1341
01953	39,808	3.84	152,788	0	99,209	0	0	0	0.00	0.1341
01954	40,622	3.67	148,927	0	73,470	0	0	0	0.00	0.1341
01955	34,652	4.20	145,693	0	51,908	0	0	0	0.00	0.1341
01956	45,723	3.12	142,556	0	30,995	0	0	0	0.00	0.1341
01957	70,367	1.99	140,106	0	14,663	0	0	0	0.00	0.1341
01958	36,607	4.12	150,687	0	85,205	0	0	0	0.00	0.1341
01959	33,255	4.42	146,946	0	60,261	0	0	0	0.00	0.1341
01960	34,612	4.15	143,784	0	39,187	0	0	0	0.00	0.1341
01961	33,558	4.20	140,945	0	20,255	0	0	0	0.00	0.1341
01962	41,530	3.64	151,292	0	89,235	0	0	0	0.00	0.1341
01963	34,210	4.33	148,101	0	67,967	0	0	0	0.00	0.1341
01964	27,880	5.20	144,938	0	46,878	0	0	0	0.00	0.1341
01965	18,427	7.70	141,866	0	26,398	0	0	0	0.00	0.1341
01966	83,632	1.65	137,906	0	-3,343	0	0	0	0.00	0.1341
01967	38,867	3.83	148,818	0	72,741	0	0	0	0.00	0.1341
01968	30,471	4.78	145,781	0	52,496	0	0	0	0.00	0.1341
01969	25,887	5.51	142,559	0	31,016	0	0	0	0.00	0.1341
01970	32,010	4.39	140,456	0	16,998	0	0	0	0.00	0.1341
01971	42,689	3.48	148,618	0	71,408	0	0	0	0.00	0.1341
01972	34,057	4.30	146,295	0	55,925	0	0	0	0.00	0.1341
01973	25,593	5.60	143,388	0	36,547	0	0	0	0.00	0.1341
01974	17,540	8.00	140,237	0	15,537	0	0	0	0.00	0.1341
01975	76,853	1.79	137,906	0	-12,770	0	0	0	0.00	0.1341
01976	37,909	3.86	146,501	0	57,298	0	0	0	0.00	0.1341
01977	29,482	4.88	143,986	0	40,531	0	0	0	0.00	0.1341
01978	24,552	5.74	140,939	0	20,215	0	0	0	0.00	0.1341
01979	27,285	5.23	142,579	0	31,154	0	0	0	0.00	0.1341
01980	38,202	3.82	146,052	0	54,301	0	0	0	0.00	0.1341
01981	31,288	4.61	144,346	0	42,930	0	0	0	0.00	0.1341
01982	24,739	5.73	141,805	0	25,994	0	0	0	0.00	0.1341
01983	18,643	7.44	138,760	0	5,692	0	0	0	0.00	0.1341
01984	73,123	1.89	137,906	0	-14,343	0	0	0	0.00	0.1341
01985	31,255	4.62	144,550	0	44,292	0	0	0	0.00	0.1341
01986	25,116	5.67	142,429	0	30,148	0	0	0	0.00	0.1341
01987	21,193	6.60	139,782	0	12,507	0	0	0	0.00	0.1341
01988	23,807	6.05	144,077	0	41,135	0	0	0	0.00	0.1341
01989	27,540	5.24	144,223	0	42,108	0	0	0	0.00	0.1341
01990	23,321	6.13	142,903	0	33,314	0	0	0	0.00	0.1341
01991	18,700	7.52	140,620	0	18,088	0	0	0	0.00	0.1341
01992	13,782	10.01	137,906	0	-1,306	0	0	0	0.00	0.1341
01993	33,653	4.10	137,906	0	-17,275	0	0	0	0.00	0.1341
01994	19,214	7.46	143,322	0	36,102	0	0	0	0.00	0.1341
01995	16,318	8.67	141,439	0	23,552	0	0	0	0.00	0.1341
01996	15,046	9.23	138,882	0	6,505	0	0	0	0.00	0.1341
01997	17,456	8.36	145,930	0	53,491	0	0	0	0.00	0.1341
01998	12,084	11.85	143,256	0	35,662	0	0	0	0.00	0.1341
01999	10,680	13.31	142,149	0	28,285	0	0	0	0.00	0.1341
02000	9,264	15.12	140,039	0	14,219	0	0	0	0.00	0.1341
02001	8,820	15.64	137,906	0	-4,829	0	0	0	0.00	0.1341
02002	12,024	11.47	137,906	0	-28,987	0	0	0	0.00	0.1341
02003	5,146	27.55	141,755	0	25,657	0	0	0	0.00	0.1341
02004	5,974	23.93	142,977	0	33,807	0	0	0	0.00	0.1341
02005	7,098	20.33	144,338	0	42,876	0	0	0	0.00	0.1341
02006	9,336	15.70	146,556	0	57,663	0	0	0	0.00	0.1341
02007	5,691	25.14	143,069	0	34,420	0	0	0	0.00	0.1341
02008	5,279	26.89	141,978	0	27,146	0	0	0	0.00	0.1341
02009	5,935	24.12	143,158	0	35,009	0	0	0	0.00	0.1341
02010	7,059	20.50	144,675	0	45,122	0	0	0	0.00	0.1341
02011	11,665	12.56	146,476	0	57,129	0	0	0	0.00	0.1341
02012	13,297	10.75	142,949	0	33,617	0	0	0	0.00	0.1341
02013	11,215	12.59	141,148	0	21,613	0	0	0	0.00	0.1341
02014	9,790	14.17	138,694	0	5,253	0	0	0	0.00	0.1341
02015	15,764	9.21	145,144	0	48,252	0	0	0	0.00	0.1341
02016	22,016	6.53	143,671	0	38,431	0	0	0	0.00	0.1341
02017	18,449	7.72	142,431	0	30,162	0	0	0	0.00	0.1341
02018	15,018	9.34	140,297	0	15,936	0	0	0	0.00	0.1341
02019	11,346	12.15	137,906	0	-1,494	0	0	0	0.00	0.1341
02020	28,155	4.90	137,906	0	-21,369	0	0	0	0.00	0.1341
02021	26,622	5.40	143,764	0	39,048	0	0	0	0.00	0.1341
02022	21,911	6.48	141,904	0	26,651	0	0	0	0.00	0.1341
02023	19,430	7.17	139,397	0	9,939	0	0	0	0.00	0.1341
02024	19,984	7.20	143,847	0	39,603	0	0	0	0.00	0.1341
02025	33,904	4.27	144,877	0	46,471	0	0	0	0.00	0.1341



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm <sup>2</sup> /cm]
02026	28,664	5.01	143,568	0	37,742	0	0	0	0.00	0.1341
02027	22,839	6.19	141,278	0	22,476	0	0	0	0.00	0.1341
02028	17,111	8.09	138,442	0	3,572	0	0	0	0.00	0.1341
02029	58,350	2.36	137,906	0	-15,848	0	0	0	0.00	0.1341
02030	35,993	4.04	145,467	0	50,407	0	0	0	0.00	0.1341
02031	28,830	4.97	143,215	0	35,393	0	0	0	0.00	0.1341
02032	25,328	5.55	140,535	0	17,524	0	0	0	0.00	0.1341
02033	23,672	5.89	139,393	0	9,911	0	0	0	0.00	0.1341
02034	41,908	3.51	147,058	0	61,013	0	0	0	0.00	0.1341
02035	33,994	4.27	145,277	0	49,135	0	0	0	0.00	0.1341
02036	26,530	5.38	142,611	0	31,363	0	0	0	0.00	0.1341
02037	19,536	7.15	139,609	0	11,354	0	0	0	0.00	0.1341
02038	76,084	1.81	137,906	0	-4,927	0	0	0	0.00	0.1341
02039	39,627	3.73	147,676	0	65,134	0	0	0	0.00	0.1341
02040	30,737	4.71	144,916	0	46,730	0	0	0	0.00	0.1341
02041	25,847	5.49	141,818	0	26,079	0	0	0	0.00	0.1341
02042	28,235	5.06	142,944	0	33,587	0	0	0	0.00	0.1341
02043	43,426	3.45	149,787	0	79,205	0	0	0	0.00	0.1341
02044	34,656	4.25	147,265	0	62,390	0	0	0	0.00	0.1341
02045	26,458	5.45	144,271	0	42,434	0	0	0	0.00	0.1341
02046	17,690	7.96	140,840	0	19,557	0	0	0	0.00	0.1341
02047	80,953	1.70	137,906	0	-8,035	0	0	0	0.00	0.1341
02048	38,560	3.89	149,889	0	79,883	0	0	0	0.00	0.1341
02049	31,857	4.60	146,506	0	57,332	0	0	0	0.00	0.1341
02050	28,655	5.00	143,361	0	36,363	0	0	0	0.00	0.1341
02051	35,101	3.93	137,906	0	-803	0	0	0	0.00	0.1341
02052	41,095	3.70	152,206	0	95,330	0	0	0	0.00	0.1341
02053	35,298	4.21	148,688	0	71,877	0	0	0	0.00	0.1341
02054	32,698	4.44	145,256	0	49,000	0	0	0	0.00	0.1341
02055	27,869	5.11	142,425	0	30,125	0	0	0	0.00	0.1341
02056	86,780	1.59	137,964	0	382	0	0	0	2.50	0.1341
02057	38,063	3.96	150,781	0	85,829	0	0	0	0.00	0.1341
02058	36,366	4.05	147,450	0	63,622	0	0	0	0.00	0.1341
02059	39,776	3.60	143,386	0	36,531	0	0	0	0.00	0.1341
02060	52,155	2.74	142,704	0	31,984	0	0	0	0.00	0.1341
Piano Terra			Parete P2-P5				Parete P2-P5			
00047	110,341	1.28	140,713	0	18,711	0	0	0	2.50	0.1341
00052	41,132	3.35	137,906	0	-149,152	0	0	0	0.00	0.1341
00137	24,528	5.62	137,906	0	-88,328	0	0	0	0.00	0.1341
00380	68,423	2.21	151,039	0	87,554	0	0	0	0.00	0.1341
00381	39,378	3.74	147,380	0	63,159	0	0	0	0.00	0.1341
00382	56,106	2.77	155,365	0	116,390	0	0	0	0.00	0.1341
00383	52,664	2.91	153,180	0	101,827	0	0	0	0.00	0.1341
00384	50,852	2.97	151,138	0	88,213	0	0	0	0.00	0.1341
00385	41,909	3.38	141,447	0	23,607	0	0	0	0.00	0.1341
00386	40,854	3.42	139,665	0	11,725	0	0	0	0.00	0.1341
00387	40,534	3.43	139,065	0	7,724	0	0	0	0.00	0.1341
00388	37,030	3.74	138,458	0	3,677	0	0	0	0.00	0.1341
00389	35,091	3.93	137,906	0	-6,614	0	0	0	0.00	0.1341
00390	34,195	4.03	137,906	0	-2,312	0	0	0	0.00	0.1341
00391	27,899	4.94	137,906	0	-8,489	0	0	0	0.00	0.1341
00392	29,022	4.75	137,906	0	-16,188	0	0	0	0.00	0.1341
00393	24,892	5.54	137,906	0	-7,503	0	0	0	0.00	0.1341
00394	22,596	6.10	137,906	0	-14,299	0	0	0	0.00	0.1341
00395	24,304	5.67	137,906	0	-19,542	0	0	0	0.00	0.1341
00396	19,993	6.90	137,906	0	-14,490	0	0	0	0.00	0.1341
00397	21,420	6.44	137,906	0	-17,302	0	0	0	0.00	0.1341
00398	20,873	6.61	137,906	0	-25,195	0	0	0	0.00	0.1341
00399	25,128	5.49	137,906	0	-19,511	0	0	0	0.00	0.1341
00400	27,130	5.08	137,906	0	-20,268	0	0	0	0.00	0.1341
00401	25,972	5.31	137,906	0	-20,628	0	0	0	0.00	0.1341
00402	28,312	4.87	137,906	0	-16,275	0	0	0	0.00	0.1341
00403	31,446	4.39	137,906	0	-18,551	0	0	0	0.00	0.1341
00404	29,323	4.70	137,906	0	-15,989	0	0	0	0.00	0.1341
00405	32,276	4.27	137,906	0	-13,590	0	0	0	0.00	0.1341
00406	36,558	3.77	137,906	0	-17,763	0	0	0	0.00	0.1341
00407	34,678	3.98	137,906	0	-15,477	0	0	0	0.00	0.1341
00408	37,803	3.65	137,906	0	-13,598	0	0	0	0.00	0.1341
00409	40,279	3.42	137,906	0	-17,824	0	0	0	0.00	0.1341
00410	40,880	3.37	137,906	0	-19,388	0	0	0	0.00	0.1341
00411	52,974	2.72	144,015	0	40,726	0	0	0	0.00	0.1341
00412	53,014	2.71	143,684	0	38,520	0	0	0	0.00	0.1341
00413	45,336	3.04	137,906	0	-27,301	0	0	0	0.00	0.1341
00414	49,929	2.85	142,278	0	29,144	0	0	0	0.00	0.1341
00474	93,788	1.51	141,359	0	23,018	0	0	0	2.50	0.1341
00475	74,227	1.86	137,906	0	-7,942	0	0	0	0.00	0.1341
00476	68,811	2.00	137,906	0	-16,511	0	0	0	0.00	0.1341



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm <sup>2</sup> /cm]
00477	62,131	2.22	137,906	0	-14,357	0	0	0	0.00	0.1341
00478	55,629	2.48	137,906	0	-18,234	0	0	0	0.00	0.1341
00479	50,472	2.73	137,906	0	-16,279	0	0	0	0.00	0.1341
00480	44,653	3.09	137,906	0	-14,112	0	0	0	0.00	0.1341
00481	38,987	3.54	137,906	0	-14,674	0	0	0	0.00	0.1341
00482	34,127	4.04	137,906	0	-9,316	0	0	0	0.00	0.1341
00483	29,358	4.70	137,906	0	-7,730	0	0	0	0.00	0.1341
00484	25,655	5.38	137,906	0	-2,373	0	0	0	0.00	0.1341
00485	24,760	5.57	137,906	0	-3,072	0	0	0	0.00	0.1341
00486	23,386	5.90	137,906	0	-2,851	0	0	0	0.00	0.1341
00487	22,003	6.27	137,906	0	-3,272	0	0	0	0.00	0.1341
00488	21,152	6.52	137,906	0	-3,978	0	0	0	0.00	0.1341
00489	19,848	6.95	137,906	0	-3,614	0	0	0	0.00	0.1341
00490	19,448	7.09	137,906	0	-7,696	0	0	0	0.00	0.1341
00491	20,258	6.81	137,906	0	-7,927	0	0	0	0.00	0.1341
00492	21,596	6.39	137,906	0	-6,967	0	0	0	0.00	0.1341
00493	23,176	5.95	137,906	0	-7,195	0	0	0	0.00	0.1341
00494	24,147	5.71	137,906	0	-7,088	0	0	0	0.00	0.1341
00495	25,524	5.40	137,906	0	-5,969	0	0	0	0.00	0.1341
00496	27,276	5.06	137,906	0	-6,376	0	0	0	0.00	0.1341
00497	28,945	4.76	137,906	0	-5,195	0	0	0	0.00	0.1341
00498	30,255	4.56	137,906	0	-5,819	0	0	0	0.00	0.1341
00499	31,598	4.36	137,906	0	-3,144	0	0	0	0.00	0.1341
00500	35,320	3.90	137,906	0	-9,549	0	0	0	0.00	0.1341
00501	40,655	3.39	137,906	0	-12,848	0	0	0	0.00	0.1341
00502	45,656	3.02	137,906	0	-13,566	0	0	0	0.00	0.1341
00503	51,327	2.69	137,906	0	-13,553	0	0	0	0.00	0.1341
00504	56,955	2.42	137,906	0	-17,296	0	0	0	0.00	0.1341
00505	61,546	2.24	137,906	0	-11,404	0	0	0	0.00	0.1341
00506	68,348	2.02	137,906	0	-7,020	0	0	0	0.00	0.1341
00507	76,017	1.81	137,906	0	-9,145	0	0	0	0.00	0.1341
00508	93,856	1.54	144,728	0	45,476	0	0	0	2.50	0.1341
00509	93,911	1.47	137,906	0	-26,736	0	0	0	2.50	0.1341
00510	80,640	1.71	137,906	0	-13,099	0	0	0	0.00	0.1341
00511	67,157	2.05	137,906	0	-18,712	0	0	0	0.00	0.1341
00512	76,781	1.80	137,906	0	-15,276	0	0	0	0.00	0.1341
00513	86,542	1.66	143,349	0	36,287	0	0	0	0.00	0.1341
00514	85,904	1.65	141,500	0	23,955	0	0	0	0.00	0.1341
00515	109,124	1.26	137,906	0	-37,700	0	0	0	2.50	0.1341
00516	143,239	5.73	821,056	2,107,350	-172,143	0	0	0	2.50	0.1341
00517	118,086	1.17	137,906	0	-122,684	0	0	0	2.50	0.1341
00518	85,611	1.61	137,906	0	-14,467	0	0	0	2.50	0.1341
00519	96,698	1.46	141,026	0	20,796	0	0	0	2.50	0.1341
00520	83,528	1.76	146,765	0	59,060	0	0	0	0.00	0.1341
00521	72,446	1.90	137,906	0	-23,842	0	0	0	0.00	0.1341
00522	77,391	1.78	137,906	0	-14,217	0	0	0	0.00	0.1341
00523	71,016	1.94	137,906	0	-19,680	0	0	0	0.00	0.1341
00524	96,270	1.43	137,906	0	-37,004	0	0	0	2.50	0.1341
01806	104,778	1.32	138,715	0	5,388	0	0	0	2.50	0.1341
01807	64,025	2.15	137,906	0	-106,438	0	0	0	0.00	0.1341
01808	43,677	3.16	137,906	0	-46,111	0	0	0	0.00	0.1341
01809	103,513	1.33	137,906	0	-802	0	0	0	2.50	0.1341
01810	96,286	1.43	137,906	0	-10,129	0	0	0	2.50	0.1341
01811	91,950	1.50	137,906	0	-10,388	0	0	0	2.50	0.1341
01812	106,267	1.38	146,255	0	55,660	0	0	0	2.50	0.1341
01813	108,864	1.30	141,318	0	22,741	0	0	0	2.50	0.1341
01814	70,806	1.95	137,906	0	-2,284	0	0	0	0.00	0.1341
01815	71,867	1.92	137,906	0	-16,028	0	0	0	0.00	0.1341
01816	73,984	1.86	137,906	0	-13,528	0	0	0	0.00	0.1341
01817	86,950	1.66	143,927	0	40,137	0	0	0	0.00	0.1341
01818	72,891	1.97	143,525	0	37,458	0	0	0	0.00	0.1341
01819	62,057	2.22	137,906	0	-16,325	0	0	0	0.00	0.1341
01820	58,969	2.34	137,906	0	-15,093	0	0	0	0.00	0.1341
01821	65,319	2.21	144,105	0	41,325	0	0	0	0.00	0.1341
01822	62,792	2.30	144,429	0	43,487	0	0	0	0.00	0.1341
01823	50,164	2.97	148,891	0	73,229	0	0	0	0.00	0.1341
01824	49,002	2.81	137,906	0	-15,106	0	0	0	0.00	0.1341
01825	50,128	2.86	143,461	0	37,031	0	0	0	0.00	0.1341
01826	49,436	2.92	144,393	0	43,241	0	0	0	0.00	0.1341
01827	47,241	3.10	146,453	0	56,976	0	0	0	0.00	0.1341
01828	42,284	3.26	137,906	0	-13,011	0	0	0	0.00	0.1341
01829	39,477	3.62	142,915	0	33,389	0	0	0	0.00	0.1341
01830	38,626	3.73	143,907	0	40,006	0	0	0	0.00	0.1341
01831	36,563	3.79	138,545	0	4,259	0	0	0	0.00	0.1341
01832	39,493	3.53	139,585	0	11,191	0	0	0	0.00	0.1341
01833	31,479	4.38	137,906	0	-7,294	0	0	0	0.00	0.1341
01834	30,996	4.45	137,906	0	-1,035	0	0	0	0.00	0.1341



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm <sup>2</sup> /cm]
01835	32,911	4.19	137,987	0	535	0	0	0	0.00	0.1341
01836	37,570	3.68	138,084	0	1,186	0	0	0	0.00	0.1341
01837	27,545	5.01	137,906	0	-1,949	0	0	0	0.00	0.1341
01838	28,176	4.89	137,906	0	-2,064	0	0	0	0.00	0.1341
01839	29,670	4.65	137,906	0	-1,915	0	0	0	0.00	0.1341
01840	32,586	4.23	137,906	0	-1,229	0	0	0	0.00	0.1341
01841	35,310	3.91	137,906	0	-923	0	0	0	0.00	0.1341
01842	25,734	5.36	137,906	0	-2,879	0	0	0	0.00	0.1341
01843	26,759	5.15	137,906	0	-3,453	0	0	0	0.00	0.1341
01844	28,842	4.78	137,906	0	-3,634	0	0	0	0.00	0.1341
01845	32,592	4.23	137,906	0	-6,905	0	0	0	0.00	0.1341
01846	23,683	5.82	137,906	0	-3,126	0	0	0	0.00	0.1341
01847	24,368	5.66	137,906	0	-3,586	0	0	0	0.00	0.1341
01848	25,751	5.36	137,906	0	-5,134	0	0	0	0.00	0.1341
01849	28,083	4.91	137,906	0	-6,454	0	0	0	0.00	0.1341
01850	32,376	4.26	137,906	0	-8,892	0	0	0	0.00	0.1341
01851	22,140	6.23	137,906	0	-4,052	0	0	0	0.00	0.1341
01852	23,092	5.97	137,906	0	-4,512	0	0	0	0.00	0.1341
01853	24,744	5.57	137,906	0	-7,404	0	0	0	0.00	0.1341
01854	27,301	5.05	137,906	0	-11,671	0	0	0	0.00	0.1341
01855	20,127	6.85	137,906	0	-4,039	0	0	0	0.00	0.1341
01856	20,772	6.64	137,906	0	-5,005	0	0	0	0.00	0.1341
01857	21,769	6.33	137,906	0	-5,805	0	0	0	0.00	0.1341
01858	23,381	5.90	137,906	0	-10,295	0	0	0	0.00	0.1341
01859	27,525	5.01	137,906	0	-14,105	0	0	0	0.00	0.1341
01860	19,762	6.98	137,906	0	-9,590	0	0	0	0.00	0.1341
01861	19,703	7.00	137,906	0	-12,159	0	0	0	0.00	0.1341
01862	20,234	6.82	137,906	0	-7,340	0	0	0	0.00	0.1341
01863	21,294	6.48	137,906	0	-10,322	0	0	0	0.00	0.1341
01864	21,668	6.36	137,906	0	-8,205	0	0	0	0.00	0.1341
01865	21,768	6.34	137,906	0	-10,841	0	0	0	0.00	0.1341
01866	21,946	6.28	137,906	0	-13,555	0	0	0	0.00	0.1341
01867	22,297	6.18	137,906	0	-16,923	0	0	0	0.00	0.1341
01868	21,899	6.30	137,906	0	-12,083	0	0	0	0.00	0.1341
01869	23,730	5.81	137,906	0	-9,217	0	0	0	0.00	0.1341
01870	24,080	5.73	137,906	0	-11,900	0	0	0	0.00	0.1341
01871	24,587	5.61	137,906	0	-14,762	0	0	0	0.00	0.1341
01872	26,180	5.27	137,906	0	-19,184	0	0	0	0.00	0.1341
01873	25,670	5.37	137,906	0	-7,351	0	0	0	0.00	0.1341
01874	26,104	5.28	137,906	0	-10,207	0	0	0	0.00	0.1341
01875	26,676	5.17	137,906	0	-12,897	0	0	0	0.00	0.1341
01876	27,339	5.04	137,906	0	-15,789	0	0	0	0.00	0.1341
01877	26,752	5.15	137,906	0	-17,968	0	0	0	0.00	0.1341
01878	27,987	4.93	137,906	0	-8,266	0	0	0	0.00	0.1341
01879	28,867	4.78	137,906	0	-10,937	0	0	0	0.00	0.1341
01880	29,688	4.65	137,906	0	-13,662	0	0	0	0.00	0.1341
01881	30,581	4.51	137,906	0	-15,774	0	0	0	0.00	0.1341
01882	29,811	4.63	137,906	0	-5,923	0	0	0	0.00	0.1341
01883	31,006	4.45	137,906	0	-8,742	0	0	0	0.00	0.1341
01884	32,040	4.30	137,906	0	-11,691	0	0	0	0.00	0.1341
01885	32,710	4.22	137,906	0	-14,488	0	0	0	0.00	0.1341
01886	35,816	3.85	137,906	0	-17,474	0	0	0	0.00	0.1341
01887	32,718	4.21	137,906	0	-5,660	0	0	0	0.00	0.1341
01888	34,495	4.00	137,906	0	-9,176	0	0	0	0.00	0.1341
01889	35,561	3.88	137,906	0	-12,448	0	0	0	0.00	0.1341
01890	36,091	3.82	137,906	0	-15,737	0	0	0	0.00	0.1341
01891	35,138	3.92	137,906	0	-8,450	0	0	0	0.00	0.1341
01892	36,867	3.74	137,906	0	-5,862	0	0	0	0.00	0.1341
01893	38,628	3.57	137,906	0	-9,952	0	0	0	0.00	0.1341
01894	39,298	3.51	137,906	0	-13,679	0	0	0	0.00	0.1341
01895	41,670	3.31	137,906	0	-16,464	0	0	0	0.00	0.1341
01896	45,076	3.17	142,887	0	33,203	0	0	0	0.00	0.1341
01897	46,146	3.10	142,886	0	33,199	0	0	0	0.00	0.1341
01898	43,222	3.19	137,906	0	-11,336	0	0	0	0.00	0.1341
01899	43,139	3.20	137,906	0	-16,305	0	0	0	0.00	0.1341
01900	52,391	2.63	137,906	0	-13,396	0	0	0	0.00	0.1341
01901	55,909	2.56	143,229	0	35,487	0	0	0	0.00	0.1341
01902	58,141	2.46	142,960	0	33,690	0	0	0	0.00	0.1341
01903	55,054	2.59	142,824	0	32,782	0	0	0	0.00	0.1341
01904	48,177	2.86	137,906	0	-18,308	0	0	0	0.00	0.1341
01905	61,111	2.26	137,906	0	-14,175	0	0	0	0.00	0.1341
01906	70,083	2.05	143,949	0	40,282	0	0	0	0.00	0.1341
01907	73,451	1.94	142,521	0	30,764	0	0	0	0.00	0.1341
01908	64,139	2.21	142,028	0	27,478	0	0	0	0.00	0.1341
01909	72,756	1.90	137,906	0	-10,014	0	0	0	0.00	0.1341
01910	74,204	1.86	137,906	0	-12,979	0	0	0	0.00	0.1341
01911	90,541	1.60	144,414	0	43,387	0	0	0	2.50	0.1341



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm/cm]
01912	89,569	1.57	140,414	0	16,717	0	0	0	2.50	0.1341
01913	71,645	1.95	139,993	0	13,908	0	0	0	0.00	0.1341
01914	91,889	1.50	137,906	0	-10,280	0	0	0	2.50	0.1341
01915	102,394	1.45	148,681	0	71,834	0	0	0	2.50	0.1341
01916	115,535	1.23	142,669	0	31,754	0	0	0	2.50	0.1341
01917	109,950	1.25	137,906	0	-24,770	0	0	0	2.50	0.1341
02498	111,844	1.29	143,749	0	38,952	0	0	0	2.50	0.1341
Piano Terra										
PareteP3-P6					Parete P3-P6					
00012	85,785	1.73	148,463	0	70,379	0	0	0	0.00	0.1341
00013	78,732	1.89	148,553	0	70,978	0	0	0	0.00	0.1341
00014	94,071	1.56	146,510	0	57,359	0	0	0	2.50	0.1341
00015	83,212	1.66	137,906	0	-6,095	0	0	0	0.00	0.1341
00016	59,809	2.31	137,906	0	-1,284	0	0	0	0.00	0.1341
00017	56,980	2.44	138,850	0	6,290	0	0	0	0.00	0.1341
00018	38,864	3.61	140,234	0	15,517	0	0	0	0.00	0.1341
00019	19,573	7.28	142,463	0	30,378	0	0	0	0.00	0.1341
00020	25,785	5.50	141,862	0	26,371	0	0	0	0.00	0.1341
00021	22,649	6.35	143,830	0	39,494	0	0	0	0.00	0.1341
00022	19,850	7.28	144,518	0	44,078	0	0	0	0.00	0.1341
00023	15,501	9.26	143,548	0	37,608	0	0	0	0.00	0.1341
00024	12,407	11.58	143,691	0	38,562	0	0	0	0.00	0.1341
00025	6,599	21.77	143,669	0	38,416	0	0	0	0.00	0.1341
00026	3,910	36.44	142,461	0	30,365	0	0	0	0.00	0.1341
00027	5,237	27.27	142,796	0	32,595	0	0	0	0.00	0.1341
00028	9,344	15.16	141,667	0	25,070	0	0	0	0.00	0.1341
00029	11,769	12.20	143,599	0	37,950	0	0	0	0.00	0.1341
00030	16,342	8.70	142,174	0	28,449	0	0	0	0.00	0.1341
00031	18,534	7.73	143,329	0	36,153	0	0	0	0.00	0.1341
00032	24,859	5.68	141,138	0	21,547	0	0	0	0.00	0.1341
00033	37,688	3.72	140,387	0	16,537	0	0	0	0.00	0.1341
00034	39,249	3.54	139,094	0	7,915	0	0	0	0.00	0.1341
00035	59,097	2.34	138,262	0	2,374	0	0	0	0.00	0.1341
00036	70,037	2.07	144,943	0	46,914	0	0	0	0.00	0.1341
00037	67,617	2.13	143,771	0	39,096	0	0	0	0.00	0.1341
00038	60,267	2.46	148,115	0	68,060	0	0	0	0.00	0.1341
00039	87,727	1.80	157,637	0	131,536	0	0	0	0.00	0.1341
00053	93,002	1.53	142,273	0	29,114	0	0	0	2.50	0.1341
00055	103,448	1.50	155,233	0	115,513	0	0	0	2.50	0.1341
00138	3,817	36.39	138,912	0	6,704	0	0	0	0.00	0.1341
00139	2,942	47.40	139,444	0	10,248	0	0	0	0.00	0.1341
00417	68,140	2.15	146,287	0	55,873	0	0	0	0.00	0.1341
00525	4,422	32.11	141,990	0	27,223	0	0	0	0.00	0.1341
00526	4,633	30.53	141,468	0	23,743	0	0	0	0.00	0.1341
00527	6,193	22.99	142,391	0	29,899	0	0	0	0.00	0.1341
00528	4,920	28.12	138,346	0	2,932	0	0	0	0.00	0.1341
00529	6,431	21.44	137,906	0	-10,447	0	0	0	0.00	0.1341
00530	6,889	20.06	138,162	0	1,704	0	0	0	0.00	0.1341
00531	20,020	6.89	137,906	0	-30,892	0	0	0	0.00	0.1341
00532	31,683	4.35	137,906	0	-40,268	0	0	0	0.00	0.1341
00549	29,398	4.69	137,906	0	-46,717	0	0	0	0.00	0.1341
00550	16,583	8.32	137,906	0	-6,752	0	0	0	0.00	0.1341
00551	19,420	7.12	138,315	0	2,724	0	0	0	0.00	0.1341
00552	8,382	16.45	137,906	0	-1,488	0	0	0	0.00	0.1341
00553	10,179	13.55	137,906	0	-8,311	0	0	0	0.00	0.1341
00554	7,851	17.57	137,906	0	-8,343	0	0	0	0.00	0.1341
00555	5,665	24.34	137,906	0	-9,895	0	0	0	0.00	0.1341
00556	4,874	28.96	141,171	0	21,767	0	0	0	0.00	0.1341
00763	8,384	16.76	140,533	0	17,509	0	0	0	0.00	0.1341
00764	16,273	8.77	142,659	0	31,681	0	0	0	0.00	0.1341
00765	20,006	7.22	144,394	0	43,248	0	0	0	0.00	0.1341
00766	25,671	5.72	146,863	0	59,714	0	0	0	0.00	0.1341
00767	25,535	5.76	147,050	0	60,957	0	0	0	0.00	0.1341
00768	23,376	6.33	147,905	0	66,660	0	0	0	0.00	0.1341
00769	26,912	5.58	150,055	0	80,991	0	0	0	0.00	0.1341
00770	20,603	7.26	149,547	0	77,602	0	0	0	0.00	0.1341
00771	18,815	7.99	150,266	0	82,399	0	0	0	0.00	0.1341
00772	23,142	6.57	152,087	0	94,539	0	0	0	0.00	0.1341
00773	14,180	10.69	151,533	0	90,842	0	0	0	0.00	0.1341
00774	13,859	10.96	151,891	0	93,230	0	0	0	0.00	0.1341
00775	16,951	9.06	153,610	0	104,693	0	0	0	0.00	0.1341
00776	8,251	18.51	152,745	0	98,921	0	0	0	0.00	0.1341
00777	8,628	17.75	153,135	0	101,527	0	0	0	0.00	0.1341
00778	8,803	17.50	154,085	0	107,857	0	0	0	0.00	0.1341
00779	4,402	31.65	139,344	0	9,581	0	0	0	0.00	0.1341
00780	4,387	31.74	139,255	0	8,994	0	0	0	0.00	0.1341
00781	5,343	26.05	139,191	0	8,562	0	0	0	0.00	0.1341
00782	4,170	33.41	139,329	0	9,487	0	0	0	0.00	0.1341



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo

Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm <sup>2</sup> /cm]
00783	4,121	33.77	139,184	0	8,516	0	0	0	0.00	0.1341
00784	8,243	18.60	153,351	0	102,961	0	0	0	0.00	0.1341
00785	9,293	16.43	152,703	0	98,642	0	0	0	0.00	0.1341
00786	12,774	11.97	152,961	0	100,364	0	0	0	0.00	0.1341
00787	14,701	10.29	151,322	0	89,438	0	0	0	0.00	0.1341
00788	15,504	9.75	151,133	0	88,179	0	0	0	0.00	0.1341
00789	19,411	7.81	151,515	0	90,724	0	0	0	0.00	0.1341
00790	21,547	6.94	149,643	0	78,243	0	0	0	0.00	0.1341
00791	20,809	7.16	149,096	0	74,597	0	0	0	0.00	0.1341
00792	25,385	5.87	149,030	0	74,159	0	0	0	0.00	0.1341
00793	24,791	5.95	147,457	0	63,670	0	0	0	0.00	0.1341
00794	21,377	6.84	146,281	0	55,828	0	0	0	0.00	0.1341
00795	20,641	7.05	145,417	0	50,071	0	0	0	0.00	0.1341
00796	11,028	12.98	143,146	0	34,931	0	0	0	0.00	0.1341
00797	6,481	21.65	140,306	0	15,997	0	0	0	0.00	0.1341
01059	3,676	38.76	142,488	0	30,542	0	0	0	0.00	0.1341
01061	8,942	15.95	142,646	0	31,596	0	0	0	0.00	0.1341
01062	8,474	16.83	142,585	0	31,193	0	0	0	0.00	0.1341
01064	5,582	25.53	142,517	0	30,738	0	0	0	0.00	0.1341
01067	6,625	21.69	143,692	0	38,571	0	0	0	0.00	0.1341
01069	12,477	11.20	139,724	0	12,115	0	0	0	0.00	0.1341
01071	23,215	6.00	139,268	0	9,080	0	0	0	0.00	0.1341
01072	15,213	9.49	144,339	0	42,883	0	0	0	0.00	0.1341
01075	15,849	9.07	143,738	0	38,880	0	0	0	0.00	0.1341
01077	35,665	3.88	138,361	0	3,032	0	0	0	0.00	0.1341
01079	38,632	3.62	139,872	0	13,106	0	0	0	0.00	0.1341
01080	89,003	1.55	137,906	0	-10,449	0	0	0	2.50	0.1341
01082	64,422	2.14	137,925	0	124	0	0	0	0.00	0.1341
01085	41,117	3.46	142,184	0	28,519	0	0	0	0.00	0.1341
01087	20,750	6.75	140,073	0	14,445	0	0	0	0.00	0.1341
01089	13,993	9.99	139,858	0	13,009	0	0	0	0.00	0.1341
01090	25,335	5.59	141,524	0	24,115	0	0	0	0.00	0.1341
01093	30,527	4.54	138,570	0	4,424	0	0	0	0.00	0.1341
01095	40,556	3.49	141,708	0	25,347	0	0	0	0.00	0.1341
01097	62,218	2.30	142,860	0	33,026	0	0	0	0.00	0.1341
01098	35,198	3.96	139,271	0	9,095	0	0	0	0.00	0.1341
01101	43,868	3.23	141,480	0	23,824	0	0	0	0.00	0.1341
01103	57,517	2.44	140,516	0	17,400	0	0	0	0.00	0.1341
01105	83,874	1.66	139,269	0	9,087	0	0	0	0.00	0.1341
01106	46,888	2.97	139,400	0	9,958	0	0	0	0.00	0.1341
01109	70,348	2.01	141,720	0	25,421	0	0	0	0.00	0.1341
01111	113,717	1.34	152,134	0	94,848	0	0	0	2.50	0.1341
01113	128,140	1.15	147,739	0	65,548	0	0	0	2.50	0.1341
02061	2,529	55.72	140,923	0	20,114	0	0	0	0.00	0.1341
02062	43,231	3.22	139,246	0	8,933	0	0	0	0.00	0.1341
02063	41,382	3.37	139,461	0	10,361	0	0	0	0.00	0.1341
02064	7,304	19.22	140,404	0	16,654	0	0	0	0.00	0.1341
02065	14,329	9.88	141,621	0	24,761	0	0	0	0.00	0.1341
02066	12,542	11.00	137,906	0	-7,059	0	0	0	0.00	0.1341
02067	18,418	7.49	137,906	0	-8,874	0	0	0	0.00	0.1341
02068	27,825	4.99	138,969	0	7,085	0	0	0	0.00	0.1341
02069	22,426	6.15	137,906	0	-20,474	0	0	0	0.00	0.1341
02070	26,755	5.33	142,598	0	31,279	0	0	0	0.00	0.1341
02071	21,082	6.74	142,170	0	28,427	0	0	0	0.00	0.1341
02072	20,909	6.72	140,415	0	16,723	0	0	0	0.00	0.1341
02073	10,625	12.98	137,906	0	-5,032	0	0	0	0.00	0.1341
02074	36,309	3.98	144,621	0	44,761	0	0	0	0.00	0.1341
02075	26,947	5.32	143,232	0	35,501	0	0	0	0.00	0.1341
02076	17,646	8.04	141,827	0	26,139	0	0	0	0.00	0.1341
02077	6,343	21.82	138,427	0	3,472	0	0	0	0.00	0.1341
02078	16,320	8.49	138,558	0	4,345	0	0	0	0.00	0.1341
02079	36,677	3.97	145,689	0	51,885	0	0	0	0.00	0.1341
02080	21,837	6.58	143,627	0	38,135	0	0	0	0.00	0.1341
02081	10,506	13.55	142,364	0	29,715	0	0	0	0.00	0.1341
02082	19,570	7.11	139,071	0	7,766	0	0	0	0.00	0.1341
02083	35,392	4.18	148,078	0	67,810	0	0	0	0.00	0.1341
02084	26,988	5.40	145,869	0	53,085	0	0	0	0.00	0.1341
02085	15,423	9.35	144,224	0	42,115	0	0	0	0.00	0.1341
02086	9,086	15.38	139,744	0	12,254	0	0	0	0.00	0.1341
02087	14,490	9.79	141,796	0	25,931	0	0	0	0.00	0.1341
02088	31,456	4.72	148,511	0	70,696	0	0	0	0.00	0.1341
02089	19,688	7.43	146,259	0	55,687	0	0	0	0.00	0.1341
02090	10,389	13.96	145,054	0	47,648	0	0	0	0.00	0.1341
02091	13,270	10.67	141,618	0	24,742	0	0	0	0.00	0.1341
02092	31,773	4.74	150,460	0	83,689	0	0	0	0.00	0.1341
02093	22,274	6.66	148,253	0	68,979	0	0	0	0.00	0.1341
02094	14,094	10.40	146,634	0	58,185	0	0	0	0.00	0.1341



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm/cm]
02095	6,975	20.24	141,166	0	21,729	0	0	0	0.00	0.1341
02096	8,261	17.32	143,050	0	34,293	0	0	0	0.00	0.1341
02097	22,956	6.56	150,477	0	83,805	0	0	0	0.00	0.1341
02098	15,679	9.45	148,234	0	68,850	0	0	0	0.00	0.1341
02099	9,528	15.42	146,902	0	59,973	0	0	0	0.00	0.1341
02100	8,234	17.28	142,324	0	29,452	0	0	0	0.00	0.1341
02101	22,360	6.80	152,060	0	94,359	0	0	0	0.00	0.1341
02102	15,580	9.62	149,822	0	79,436	0	0	0	0.00	0.1341
02103	10,652	13.91	148,176	0	68,463	0	0	0	0.00	0.1341
02104	5,705	24.84	141,687	0	25,206	0	0	0	0.00	0.1341
02105	6,435	22.14	142,441	0	30,230	0	0	0	0.00	0.1341
02106	13,970	10.84	151,497	0	90,607	0	0	0	0.00	0.1341
02107	10,149	14.72	149,436	0	76,867	0	0	0	0.00	0.1341
02108	6,382	22.18	141,538	0	24,213	0	0	0	0.00	0.1341
02109	6,945	20.44	141,972	0	27,101	0	0	0	0.00	0.1341
02110	11,735	13.03	152,918	0	100,076	0	0	0	0.00	0.1341
02111	7,444	18.85	140,292	0	15,901	0	0	0	0.00	0.1341
02112	7,083	19.92	141,125	0	21,455	0	0	0	0.00	0.1341
02113	6,831	20.79	142,033	0	27,508	0	0	0	0.00	0.1341
02114	7,146	19.86	141,951	0	26,965	0	0	0	0.00	0.1341
02115	7,929	17.65	139,912	0	13,373	0	0	0	0.00	0.1341
02116	7,586	18.55	140,721	0	18,765	0	0	0	0.00	0.1341
02117	7,513	18.85	141,598	0	24,608	0	0	0	0.00	0.1341
02118	7,730	18.44	142,552	0	30,972	0	0	0	0.00	0.1341
02119	8,051	17.34	139,626	0	11,466	0	0	0	0.00	0.1341
02120	7,814	17.96	140,309	0	16,018	0	0	0	0.00	0.1341
02121	7,921	17.82	141,148	0	21,608	0	0	0	0.00	0.1341
02122	7,771	18.28	142,066	0	27,734	0	0	0	0.00	0.1341
02123	6,754	21.16	142,927	0	33,469	0	0	0	0.00	0.1341
02124	7,737	18.07	139,842	0	12,905	0	0	0	0.00	0.1341
02125	7,971	17.65	140,674	0	18,452	0	0	0	0.00	0.1341
02126	8,264	17.13	141,586	0	24,534	0	0	0	0.00	0.1341
02127	9,024	15.81	142,665	0	31,724	0	0	0	0.00	0.1341
02128	9,169	16.64	152,616	0	98,067	0	0	0	0.00	0.1341
02129	7,528	18.62	140,182	0	15,172	0	0	0	0.00	0.1341
02130	8,333	16.93	141,037	0	20,871	0	0	0	0.00	0.1341
02131	8,655	16.41	142,055	0	27,656	0	0	0	0.00	0.1341
02132	7,038	20.36	143,302	0	35,973	0	0	0	0.00	0.1341
02133	14,540	10.38	150,989	0	87,220	0	0	0	0.00	0.1341
02134	9,037	16.50	149,077	0	74,469	0	0	0	0.00	0.1341
02135	8,799	16.07	141,413	0	23,375	0	0	0	0.00	0.1341
02136	11,388	12.53	142,724	0	32,120	0	0	0	0.00	0.1341
02137	16,947	8.95	151,690	0	91,894	0	0	0	0.00	0.1341
02138	14,712	10.15	149,299	0	75,950	0	0	0	0.00	0.1341
02139	8,850	16.69	147,674	0	65,117	0	0	0	0.00	0.1341
02140	9,933	14.28	141,811	0	26,029	0	0	0	0.00	0.1341
02141	9,053	15.83	143,323	0	36,114	0	0	0	0.00	0.1341
02142	24,425	6.14	149,985	0	80,527	0	0	0	0.00	0.1341
02143	14,489	10.19	147,578	0	64,479	0	0	0	0.00	0.1341
02144	8,551	16.47	140,839	0	19,553	0	0	0	0.00	0.1341
02145	14,272	9.99	142,554	0	30,981	0	0	0	0.00	0.1341
02146	25,941	5.78	149,984	0	80,515	0	0	0	0.00	0.1341
02147	21,359	6.90	147,410	0	63,357	0	0	0	0.00	0.1341
02148	12,110	12.04	145,817	0	52,738	0	0	0	0.00	0.1341
02149	10,008	14.09	140,975	0	20,458	0	0	0	0.00	0.1341
02150	11,556	12.35	142,715	0	32,058	0	0	0	0.00	0.1341
02151	31,783	4.64	147,560	0	64,358	0	0	0	0.00	0.1341
02152	18,350	7.92	145,300	0	49,291	0	0	0	0.00	0.1341
02153	8,201	17.58	144,133	0	41,512	0	0	0	0.00	0.1341
02154	16,569	8.52	141,149	0	21,618	0	0	0	0.00	0.1341
02155	32,905	4.48	147,458	0	63,677	0	0	0	0.00	0.1341
02156	24,724	5.86	144,853	0	46,308	0	0	0	0.00	0.1341
02157	13,509	10.61	143,323	0	36,114	0	0	0	0.00	0.1341
02158	8,570	16.24	139,161	0	8,366	0	0	0	0.00	0.1341
02159	14,865	9.49	141,073	0	21,110	0	0	0	0.00	0.1341
02160	31,534	4.58	144,449	0	43,617	0	0	0	0.00	0.1341
02161	18,420	7.76	142,963	0	33,709	0	0	0	0.00	0.1341
02162	10,030	14.12	141,653	0	24,975	0	0	0	0.00	0.1341
02163	18,360	7.52	138,066	0	1,063	0	0	0	0.00	0.1341
02164	24,692	5.82	143,616	0	38,063	0	0	0	0.00	0.1341
02165	17,279	8.27	142,918	0	33,408	0	0	0	0.00	0.1341
02166	14,558	9.74	141,789	0	25,881	0	0	0	0.00	0.1341
02167	7,606	18.13	137,906	0	-11,040	0	0	0	0.00	0.1341
02168	18,148	7.60	137,906	0	-12,969	0	0	0	0.00	0.1341
02169	9,334	15.21	141,959	0	27,019	0	0	0	0.00	0.1341
02170	8,913	15.47	137,906	0	-6,613	0	0	0	0.00	0.1341
02171	16,006	8.62	137,906	0	-10,985	0	0	0	0.00	0.1341



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm <sup>2</sup> /cm]
02172	12,391	11.13	137,906	0	-25,791	0	0	0	0.00	0.1341
Piano Fondo Vasca			PareteP1-P2			Parete P1-P2				
00003	40,319	3.64	146,697	0	58,606	0	0	0	0.00	0.1341
00047	73,815	2.20	162,673	0	165,114	0	0	0	0.00	0.1341
00048	53,064	3.06	162,224	0	162,118	0	0	0	0.00	0.1341
00049	20,632	6.74	139,118	0	8,077	0	0	0	0.00	0.1341
00465	46,711	3.43	160,431	0	150,167	0	0	0	0.00	0.1341
00466	57,797	2.79	161,061	0	154,362	0	0	0	0.00	0.1341
00467	27,973	5.77	161,387	0	156,539	0	0	0	0.00	0.1341
00468	43,434	3.71	161,046	0	154,267	0	0	0	0.00	0.1341
00469	28,240	5.65	159,552	0	144,307	0	0	0	0.00	0.1341
00470	34,008	4.58	155,708	0	118,675	0	0	0	0.00	0.1341
00471	40,338	3.83	154,529	0	110,819	0	0	0	0.00	0.1341
00472	38,861	3.73	145,144	0	48,249	0	0	0	0.00	0.1341
00473	66,937	2.22	148,268	0	69,080	0	0	0	0.00	0.1341
00578	51,064	2.89	147,376	0	63,134	0	0	0	0.00	0.1341
00579	32,125	4.48	143,956	0	40,332	0	0	0	0.00	0.1341
00580	32,484	4.49	145,907	0	53,337	0	0	0	0.00	0.1341
00581	26,063	5.29	137,906	0	-3,191	0	0	0	0.00	0.1341
00582	28,909	4.77	137,906	0	-2,346	0	0	0	0.00	0.1341
00583	30,538	4.52	137,906	0	-4,024	0	0	0	0.00	0.1341
00584	32,895	4.19	137,906	0	-6,618	0	0	0	0.00	0.1341
00585	32,796	4.20	137,906	0	-8,154	0	0	0	0.00	0.1341
00586	37,568	3.67	137,906	0	-26,873	0	0	0	0.00	0.1341
00587	71,684	2.23	159,667	0	145,071	0	0	0	0.00	0.1341
00588	52,256	2.94	153,715	0	105,392	0	0	0	0.00	0.1341
00589	46,785	3.31	154,936	0	113,530	0	0	0	0.00	0.1341
00590	47,405	3.21	152,264	0	95,715	0	0	0	0.00	0.1341
00591	48,403	3.15	152,380	0	96,494	0	0	0	0.00	0.1341
00592	48,186	3.18	153,188	0	101,878	0	0	0	0.00	0.1341
00593	53,443	2.91	155,438	0	116,878	0	0	0	0.00	0.1341
00594	57,055	2.73	155,661	0	118,364	0	0	0	0.00	0.1341
00595	55,986	2.79	156,127	0	121,472	0	0	0	0.00	0.1341
00596	57,979	2.73	158,216	0	135,395	0	0	0	0.00	0.1341
00597	57,018	2.79	158,909	0	140,018	0	0	0	0.00	0.1341
00844	19,713	7.02	138,403	0	3,311	0	0	0	0.00	0.1341
00845	8,187	16.98	139,030	0	7,493	0	0	0	0.00	0.1341
00846	22,076	6.25	137,906	0	-3,774	0	0	0	0.00	0.1341
00847	22,960	6.04	138,609	0	4,682	0	0	0	0.00	0.1341
00848	15,657	8.85	138,625	0	4,790	0	0	0	0.00	0.1341
00849	16,800	8.21	137,944	0	253	0	0	0	0.00	0.1341
00850	9,184	15.24	139,927	0	13,474	0	0	0	0.00	0.1341
00851	9,361	14.77	138,306	0	2,667	0	0	0	0.00	0.1341
00852	12,618	10.93	137,906	0	-1,350	0	0	0	0.00	0.1341
00853	13,322	10.46	139,381	0	9,834	0	0	0	0.00	0.1341
00854	21,202	6.56	138,990	0	7,222	0	0	0	0.00	0.1341
02383	29,307	4.71	137,906	0	-2,750	0	0	0	0.00	0.1341
02384	68,697	2.25	154,239	0	108,882	0	0	0	0.00	0.1341
02385	51,245	3.13	160,251	0	148,965	0	0	0	0.00	0.1341
02386	45,703	3.15	143,769	0	39,082	0	0	0	0.00	0.1341
02387	37,157	3.87	143,646	0	38,261	0	0	0	0.00	0.1341
02388	18,934	7.28	137,906	0	-8,111	0	0	0	0.00	0.1341
02389	30,371	5.14	156,019	0	120,749	0	0	0	0.00	0.1341
02390	38,842	4.13	160,429	0	150,154	0	0	0	0.00	0.1341
02391	46,144	3.51	161,745	0	158,927	0	0	0	0.00	0.1341
02392	50,562	3.15	159,243	0	142,243	0	0	0	0.00	0.1341
02393	25,930	5.61	145,554	0	50,987	0	0	0	0.00	0.1341
02394	13,021	10.59	137,906	0	-7,251	0	0	0	0.00	0.1341
02395	12,394	11.26	139,507	0	10,674	0	0	0	0.00	0.1341
02396	29,407	5.40	158,806	0	139,329	0	0	0	0.00	0.1341
02397	46,964	3.37	158,121	0	134,762	0	0	0	0.00	0.1341
02398	25,129	5.63	141,578	0	24,480	0	0	0	0.00	0.1341
02399	22,846	6.43	146,984	0	60,520	0	0	0	0.00	0.1341
02400	13,481	10.31	139,007	0	7,337	0	0	0	0.00	0.1341
02401	13,986	9.97	139,471	0	10,432	0	0	0	0.00	0.1341
02402	31,852	4.90	156,078	0	121,143	0	0	0	0.00	0.1341
02403	46,666	3.34	155,791	0	119,231	0	0	0	0.00	0.1341
02404	22,476	6.33	142,232	0	28,838	0	0	0	0.00	0.1341
02405	14,346	9.67	138,716	0	5,400	0	0	0	0.00	0.1341
02406	13,852	10.05	139,164	0	8,386	0	0	0	0.00	0.1341
02407	21,681	7.08	153,568	0	104,414	0	0	0	0.00	0.1341
02408	38,456	4.00	153,719	0	105,419	0	0	0	0.00	0.1341
02409	13,740	10.05	138,090	0	1,224	0	0	0	0.00	0.1341
02410	14,562	9.52	138,585	0	4,522	0	0	0	0.00	0.1341
02411	14,241	9.76	138,955	0	6,989	0	0	0	0.00	0.1341
02412	14,516	9.59	139,165	0	8,390	0	0	0	0.00	0.1341
02413	29,916	5.09	152,124	0	94,785	0	0	0	0.00	0.1341



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm/cm]
02414	40,866	3.76	153,510	0	104,021	0	0	0	0.00	0.1341
02415	17,355	7.97	138,395	0	3,260	0	0	0	0.00	0.1341
02416	19,641	7.02	137,906	0	-10,251	0	0	0	0.00	0.1341
02417	16,837	8.19	137,906	0	-11,158	0	0	0	0.00	0.1341
02418	23,611	6.33	149,397	0	76,603	0	0	0	0.00	0.1341
02419	40,580	3.72	151,152	0	88,304	0	0	0	0.00	0.1341
02420	32,561	4.24	137,906	0	-10,373	0	0	0	0.00	0.1341
02421	34,227	4.03	137,906	0	-10,234	0	0	0	0.00	0.1341
02422	29,939	4.61	137,906	0	-6,979	0	0	0	0.00	0.1341
02423	23,375	5.90	137,906	0	-6,842	0	0	0	0.00	0.1341
02424	33,825	4.37	147,823	0	66,111	0	0	0	0.00	0.1341
02425	61,354	2.45	150,018	0	80,744	0	0	0	0.00	0.1341
Piano Fondo Vasca			Parete P4-P5				Parete P4-P5			
00001	72,206	2.22	160,581	0	151,167	0	0	0	0.00	0.1341
00002	47,458	3.08	146,217	0	55,404	0	0	0	0.00	0.1341
00004	51,971	3.11	161,642	0	158,239	0	0	0	0.00	0.1341
00050	19,511	7.07	137,906	0	-18,061	0	0	0	0.00	0.1341
00421	65,836	2.23	146,916	0	60,062	0	0	0	0.00	0.1341
00422	32,519	4.46	145,052	0	47,640	0	0	0	0.00	0.1341
00423	40,116	3.80	152,362	0	96,369	0	0	0	0.00	0.1341
00424	35,071	4.51	158,111	0	134,696	0	0	0	0.00	0.1341
00425	42,026	3.81	160,220	0	148,759	0	0	0	0.00	0.1341
00426	38,788	4.17	161,691	0	158,563	0	0	0	0.00	0.1341
00427	44,165	3.69	162,810	0	166,027	0	0	0	0.00	0.1341
00428	57,047	2.82	160,876	0	153,128	0	0	0	0.00	0.1341
00429	47,015	3.43	161,069	0	154,419	0	0	0	0.00	0.1341
00557	38,381	3.59	137,906	0	-27,522	0	0	0	0.00	0.1341
00558	33,581	4.11	137,906	0	-8,342	0	0	0	0.00	0.1341
00559	32,664	4.22	137,906	0	-6,973	0	0	0	0.00	0.1341
00560	30,736	4.49	137,906	0	-4,148	0	0	0	0.00	0.1341
00561	28,372	4.86	137,906	0	-2,412	0	0	0	0.00	0.1341
00562	26,106	5.28	137,906	0	-3,525	0	0	0	0.00	0.1341
00563	30,765	4.75	146,069	0	54,419	0	0	0	0.00	0.1341
00564	30,430	4.73	144,013	0	40,710	0	0	0	0.00	0.1341
00565	48,753	3.02	147,041	0	60,895	0	0	0	0.00	0.1341
00598	58,039	2.73	158,598	0	137,944	0	0	0	0.00	0.1341
00599	60,135	2.63	158,278	0	135,812	0	0	0	0.00	0.1341
00600	58,303	2.68	156,187	0	121,872	0	0	0	0.00	0.1341
00601	59,816	2.60	155,566	0	117,730	0	0	0	0.00	0.1341
00602	56,780	2.74	155,382	0	116,504	0	0	0	0.00	0.1341
00603	51,720	2.96	153,110	0	101,356	0	0	0	0.00	0.1341
00604	52,412	2.90	152,043	0	94,243	0	0	0	0.00	0.1341
00605	51,414	2.96	151,995	0	93,927	0	0	0	0.00	0.1341
00606	50,202	3.07	154,166	0	108,399	0	0	0	0.00	0.1341
00607	55,317	2.76	152,588	0	97,879	0	0	0	0.00	0.1341
00608	71,829	2.19	157,544	0	130,918	0	0	0	0.00	0.1341
00833	21,921	6.30	138,117	0	1,402	0	0	0	0.00	0.1341
00834	7,624	18.24	139,061	0	7,696	0	0	0	0.00	0.1341
00835	20,330	6.78	137,906	0	-3,174	0	0	0	0.00	0.1341
00836	21,921	6.32	138,607	0	4,668	0	0	0	0.00	0.1341
00837	14,811	9.36	138,703	0	5,311	0	0	0	0.00	0.1341
00838	15,801	8.73	138,010	0	692	0	0	0	0.00	0.1341
00839	9,193	15.00	137,906	0	-1,539	0	0	0	0.00	0.1341
00840	10,254	13.50	138,401	0	3,298	0	0	0	0.00	0.1341
00841	13,782	10.01	137,906	0	-692	0	0	0	0.00	0.1341
00842	13,481	10.34	139,402	0	9,974	0	0	0	0.00	0.1341
00843	21,459	6.48	139,032	0	7,504	0	0	0	0.00	0.1341
02204	29,698	4.64	137,906	0	-2,862	0	0	0	0.00	0.1341
02205	66,559	2.30	152,893	0	99,909	0	0	0	0.00	0.1341
02206	52,917	3.03	160,225	0	148,794	0	0	0	0.00	0.1341
02207	48,842	2.93	143,211	0	35,367	0	0	0	0.00	0.1341
02208	36,181	3.99	144,258	0	42,344	0	0	0	0.00	0.1341
02209	22,180	6.72	149,123	0	74,775	0	0	0	0.00	0.1341
02210	25,708	6.09	156,482	0	123,837	0	0	0	0.00	0.1341
02211	37,117	4.31	159,997	0	147,272	0	0	0	0.00	0.1341
02212	47,047	3.42	161,008	0	154,008	0	0	0	0.00	0.1341
02213	53,931	2.95	159,221	0	142,098	0	0	0	0.00	0.1341
02214	23,603	6.17	145,538	0	50,878	0	0	0	0.00	0.1341
02215	13,093	10.62	139,042	0	7,573	0	0	0	0.00	0.1341
02216	14,587	9.56	139,490	0	10,555	0	0	0	0.00	0.1341
02217	31,486	5.05	158,989	0	140,553	0	0	0	0.00	0.1341
02218	49,304	3.20	157,993	0	133,909	0	0	0	0.00	0.1341
02219	23,480	6.03	141,468	0	23,747	0	0	0	0.00	0.1341
02220	20,863	7.05	147,172	0	61,773	0	0	0	0.00	0.1341
02221	14,727	9.45	139,110	0	8,022	0	0	0	0.00	0.1341
02222	16,378	8.51	139,421	0	10,095	0	0	0	0.00	0.1341
02223	34,599	4.51	155,982	0	120,502	0	0	0	0.00	0.1341



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm/cm]
02224	49,334	3.15	155,634	0	118,182	0	0	0	0.00	0.1341
02225	20,976	6.78	142,257	0	29,001	0	0	0	0.00	0.1341
02226	15,236	9.11	138,778	0	5,809	0	0	0	0.00	0.1341
02227	16,126	8.63	139,108	0	8,010	0	0	0	0.00	0.1341
02228	24,566	6.25	153,492	0	103,905	0	0	0	0.00	0.1341
02229	41,522	3.70	153,576	0	104,467	0	0	0	0.00	0.1341
02230	15,511	8.90	138,122	0	1,438	0	0	0	0.00	0.1341
02231	16,532	8.38	138,559	0	4,353	0	0	0	0.00	0.1341
02232	16,307	8.52	138,902	0	6,636	0	0	0	0.00	0.1341
02233	16,647	8.35	139,077	0	7,802	0	0	0	0.00	0.1341
02234	32,732	4.64	151,972	0	93,774	0	0	0	0.00	0.1341
02235	43,910	3.49	153,218	0	102,076	0	0	0	0.00	0.1341
02236	19,124	7.24	138,390	0	3,223	0	0	0	0.00	0.1341
02237	20,439	6.75	137,906	0	-10,302	0	0	0	0.00	0.1341
02238	17,680	7.80	137,906	0	-11,296	0	0	0	0.00	0.1341
02239	25,865	5.77	149,321	0	76,096	0	0	0	0.00	0.1341
02240	42,834	3.52	150,778	0	85,812	0	0	0	0.00	0.1341
02241	32,961	4.18	137,906	0	-10,339	0	0	0	0.00	0.1341
02242	34,713	3.97	137,906	0	-10,051	0	0	0	0.00	0.1341
02243	30,533	4.52	137,906	0	-6,992	0	0	0	0.00	0.1341
02244	23,881	5.77	137,906	0	-7,205	0	0	0	0.00	0.1341
02245	34,714	4.25	147,559	0	64,351	0	0	0	0.00	0.1341
02246	59,875	2.50	149,535	0	77,527	0	0	0	0.00	0.1341
Piano Fondo Vasca			PareteP1-P4				Parete P1-P4			
00002	50,375	3.21	161,686	0	11,089	0	0	0	0.00	0.2095
00003	49,143	3.29	161,501	0	9,851	0	0	0	0.00	0.2095
00004	31,280	5.76	180,148	0	134,165	0	0	0	0.00	0.2095
00048	30,660	5.88	180,326	0	135,355	0	0	0	0.00	0.2095
00421	62,358	2.71	168,721	0	57,989	0	0	0	0.00	0.2095
00422	71,007	2.39	169,423	0	62,670	0	0	0	0.00	0.2095
00423	58,693	3.05	178,864	0	125,605	0	0	0	0.00	0.2095
00424	41,378	4.34	179,601	0	130,522	0	0	0	0.00	0.2095
00425	60,136	3.02	181,353	0	142,197	0	0	0	0.00	0.2095
00426	50,132	3.66	183,468	0	156,298	0	0	0	0.00	0.2095
00427	43,263	4.18	180,781	0	138,384	0	0	0	0.00	0.2095
00428	41,710	4.31	179,895	0	132,479	0	0	0	0.00	0.2095
00429	36,963	4.90	181,096	0	140,487	0	0	0	0.00	0.2095
00430	47,379	3.78	179,307	0	128,561	0	0	0	0.00	0.2095
00431	43,894	4.03	177,073	0	113,666	0	0	0	0.00	0.2095
00432	45,964	3.82	175,652	0	104,196	0	0	0	0.00	0.2095
00433	49,307	3.56	175,677	0	104,359	0	0	0	0.00	0.2095
00434	49,226	3.53	173,721	0	91,317	0	0	0	0.00	0.2095
00435	51,187	3.37	172,663	0	84,266	0	0	0	0.00	0.2095
00436	52,123	3.31	172,534	0	83,409	0	0	0	0.00	0.2095
00437	50,223	3.39	170,420	0	69,315	0	0	0	0.00	0.2095
00438	48,873	3.47	169,776	0	65,023	0	0	0	0.00	0.2095
00439	46,394	3.66	169,617	0	63,959	0	0	0	0.00	0.2095
00440	42,247	3.97	167,897	0	52,493	0	0	0	0.00	0.2095
00441	36,518	4.60	167,866	0	52,290	0	0	0	0.00	0.2095
00442	32,412	5.15	167,055	0	46,883	0	0	0	0.00	0.2095
00443	25,956	6.43	166,855	0	45,544	0	0	0	0.00	0.2095
00444	19,516	8.53	166,376	0	42,352	0	0	0	0.00	0.2095
00445	14,382	11.56	166,230	0	41,378	0	0	0	0.00	0.2095
00446	6,895	24.10	166,156	0	40,888	0	0	0	0.00	0.2095
00447	4,942	32.96	162,906	0	19,219	0	0	0	0.00	0.2095
00448	5,690	29.22	166,240	0	41,445	0	0	0	0.00	0.2095
00449	13,381	12.43	166,313	0	41,932	0	0	0	0.00	0.2095
00450	20,424	8.14	166,230	0	41,379	0	0	0	0.00	0.2095
00451	25,035	6.67	167,014	0	46,609	0	0	0	0.00	0.2095
00452	31,700	5.28	167,269	0	48,308	0	0	0	0.00	0.2095
00453	37,309	4.49	167,406	0	49,223	0	0	0	0.00	0.2095
00454	40,570	4.16	168,758	0	58,235	0	0	0	0.00	0.2095
00455	45,204	3.74	169,143	0	60,797	0	0	0	0.00	0.2095
00456	48,308	3.51	169,524	0	63,343	0	0	0	0.00	0.2095
00457	49,549	3.46	171,496	0	76,488	0	0	0	0.00	0.2095
00458	51,240	3.35	171,836	0	78,753	0	0	0	0.00	0.2095
00459	50,916	3.39	172,466	0	82,956	0	0	0	0.00	0.2095
00460	49,725	3.51	174,752	0	98,195	0	0	0	0.00	0.2095
00461	48,511	3.60	174,779	0	98,371	0	0	0	0.00	0.2095
00462	45,558	3.86	175,717	0	104,626	0	0	0	0.00	0.2095
00463	44,393	3.99	177,335	0	115,411	0	0	0	0.00	0.2095
00464	45,313	3.95	178,995	0	126,479	0	0	0	0.00	0.2095
00465	40,819	4.41	180,067	0	133,627	0	0	0	0.00	0.2095
00466	29,577	6.05	178,956	0	126,220	0	0	0	0.00	0.2095
00467	52,636	3.47	182,420	0	149,313	0	0	0	0.00	0.2095
00468	47,899	3.81	182,413	0	149,267	0	0	0	0.00	0.2095
00469	57,052	3.18	181,282	0	141,725	0	0	0	0.00	0.2095



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm <sup>2</sup> /cm]
00470	59,028	3.02	178,360	0	122,246	0	0	0	0.00	0.2095
00471	49,780	3.56	177,358	0	115,564	0	0	0	0.00	0.2095
00472	64,068	2.66	170,564	0	70,271	0	0	0	0.00	0.2095
00473	67,278	2.52	169,610	0	63,916	0	0	0	0.00	0.2095
00798	58,539	2.74	160,240	0	1,445	0	0	0	0.00	0.2095
00799	70,030	2.30	161,293	0	8,468	0	0	0	0.00	0.2095
00800	97,123	1.65	160,023	0	-7,022	0	0	0	2.50	0.2095
00801	80,906	1.98	160,023	0	-928	0	0	0	0.00	0.2095
00802	79,635	2.04	162,284	0	15,073	0	0	0	0.00	0.2095
00803	90,103	1.79	161,569	0	10,304	0	0	0	2.50	0.2095
00804	68,435	2.35	160,971	0	6,322	0	0	0	0.00	0.2095
00805	61,079	2.68	163,514	0	23,271	0	0	0	0.00	0.2095
00806	66,135	2.46	162,598	0	17,169	0	0	0	0.00	0.2095
00807	49,128	3.30	162,285	0	15,077	0	0	0	0.00	0.2095
00808	45,731	3.58	163,680	0	24,379	0	0	0	0.00	0.2095
00809	35,329	4.56	161,138	0	7,432	0	0	0	0.00	0.2095
00810	29,374	5.58	163,762	0	24,928	0	0	0	0.00	0.2095
00811	29,594	5.47	161,764	0	11,607	0	0	0	0.00	0.2095
00812	16,283	9.96	162,099	0	13,839	0	0	0	0.00	0.2095
00813	10,626	15.33	162,913	0	19,265	0	0	0	0.00	0.2095
00814	12,097	13.47	162,910	0	19,245	0	0	0	0.00	0.2095
00815	3,031	52.87	160,263	0	1,598	0	0	0	0.00	0.2095
00816	8,984	18.20	163,487	0	23,095	0	0	0	0.00	0.2095
00817	8,570	18.97	162,535	0	16,746	0	0	0	0.00	0.2095
00818	18,857	8.64	162,911	0	19,254	0	0	0	0.00	0.2095
00819	26,998	5.99	161,602	0	10,526	0	0	0	0.00	0.2095
00820	27,550	5.91	162,808	0	18,569	0	0	0	0.00	0.2095
00821	37,409	4.35	162,703	0	17,867	0	0	0	0.00	0.2095
00822	42,471	3.78	160,666	0	4,285	0	0	0	0.00	0.2095
00823	53,730	3.02	162,298	0	15,169	0	0	0	0.00	0.2095
00824	59,992	2.72	162,922	0	19,326	0	0	0	0.00	0.2095
00825	59,144	2.71	160,271	0	1,651	0	0	0	0.00	0.2095
00826	76,486	2.11	161,036	0	6,754	0	0	0	0.00	0.2095
00827	80,668	2.01	162,348	0	15,502	0	0	0	0.00	0.2095
00828	75,297	2.13	160,023	0	-4,397	0	0	0	0.00	0.2095
00829	88,548	1.81	160,023	0	-7,426	0	0	0	2.50	0.2095
00830	86,063	1.87	160,803	0	5,201	0	0	0	2.50	0.2095
00831	70,477	2.27	160,023	0	-5,139	0	0	0	0.00	0.2095
00832	55,927	2.87	160,385	0	2,412	0	0	0	0.00	0.2095
01670	64,704	2.56	165,441	0	36,120	0	0	0	0.00	0.2095
01671	44,118	4.08	179,800	0	131,845	0	0	0	0.00	0.2095
01672	42,564	4.21	179,312	0	128,593	0	0	0	0.00	0.2095
01673	71,716	2.32	166,212	0	41,259	0	0	0	0.00	0.2095
01674	86,191	1.93	166,174	0	41,005	0	0	0	0.00	0.2095
01675	90,514	1.92	173,728	0	91,367	0	0	0	0.00	0.2095
01676	75,284	2.37	178,629	0	124,038	0	0	0	0.00	0.2095
01677	64,496	2.81	180,945	0	139,481	0	0	0	0.00	0.2095
01678	55,422	3.26	180,924	0	139,342	0	0	0	0.00	0.2095
01679	53,058	3.38	179,167	0	127,627	0	0	0	0.00	0.2095
01680	128,801	1.31	169,120	0	60,646	0	0	0	2.50	0.2095
01681	105,666	1.65	174,352	0	95,524	0	0	0	2.50	0.2095
01682	88,027	2.02	177,681	0	117,722	0	0	0	0.00	0.2095
01683	70,679	2.53	178,888	0	125,766	0	0	0	0.00	0.2095
01684	55,257	3.22	177,978	0	119,699	0	0	0	0.00	0.2095
01685	129,162	1.27	164,092	0	27,125	0	0	0	2.50	0.2095
01686	121,820	1.40	170,031	0	66,721	0	0	0	2.50	0.2095
01687	104,434	1.67	173,979	0	93,037	0	0	0	2.50	0.2095
01688	85,942	2.05	176,258	0	108,233	0	0	0	0.00	0.2095
01689	68,332	2.59	176,711	0	111,252	0	0	0	0.00	0.2095
01690	53,740	3.27	175,652	0	104,191	0	0	0	0.00	0.2095
01691	132,567	1.25	165,741	0	38,117	0	0	0	2.50	0.2095
01692	111,274	1.53	170,118	0	67,301	0	0	0	2.50	0.2095
01693	95,594	1.81	173,043	0	86,800	0	0	0	0.00	0.2095
01694	78,620	2.22	174,453	0	96,203	0	0	0	0.00	0.2095
01695	62,172	2.80	174,331	0	95,385	0	0	0	0.00	0.2095
01696	107,444	1.51	162,624	0	17,338	0	0	0	2.50	0.2095
01697	108,571	1.53	166,532	0	43,394	0	0	0	2.50	0.2095
01698	97,445	1.74	169,857	0	65,563	0	0	0	2.50	0.2095
01699	83,597	2.06	171,856	0	78,884	0	0	0	0.00	0.2095
01700	69,062	2.50	172,615	0	83,944	0	0	0	0.00	0.2095
01701	56,774	3.03	172,279	0	81,710	0	0	0	0.00	0.2095
01702	105,583	1.56	164,302	0	28,526	0	0	0	2.50	0.2095
01703	91,578	1.83	167,185	0	47,748	0	0	0	2.50	0.2095
01704	82,263	2.06	169,344	0	62,143	0	0	0	0.00	0.2095
01705	70,622	2.42	170,617	0	70,624	0	0	0	0.00	0.2095
01706	58,334	2.93	170,849	0	72,171	0	0	0	0.00	0.2095
01707	75,698	2.14	162,158	0	14,234	0	0	0	0.00	0.2095



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm/cm]
01708	80,984	2.04	164,814	0	31,939	0	0	0	0.00	0.2095
01709	75,484	2.22	167,226	0	48,018	0	0	0	0.00	0.2095
01710	67,243	2.51	168,707	0	57,893	0	0	0	0.00	0.2095
01711	57,772	2.93	169,415	0	62,614	0	0	0	0.00	0.2095
01712	49,417	3.43	169,434	0	62,737	0	0	0	0.00	0.2095
01713	73,472	2.23	163,775	0	25,012	0	0	0	0.00	0.2095
01714	64,545	2.57	165,616	0	37,284	0	0	0	0.00	0.2095
01715	59,551	2.81	167,085	0	47,082	0	0	0	0.00	0.2095
01716	52,812	3.18	168,043	0	53,468	0	0	0	0.00	0.2095
01717	45,186	3.73	168,320	0	55,314	0	0	0	0.00	0.2095
01718	44,667	3.63	162,093	0	13,801	0	0	0	0.00	0.2095
01719	51,640	3.18	164,431	0	29,386	0	0	0	0.00	0.2095
01720	48,798	3.40	165,799	0	38,510	0	0	0	0.00	0.2095
01721	44,467	3.75	166,852	0	45,525	0	0	0	0.00	0.2095
01722	39,245	4.27	167,393	0	49,132	0	0	0	0.00	0.2095
01723	34,405	4.87	167,515	0	49,947	0	0	0	0.00	0.2095
01724	41,239	3.96	163,254	0	21,539	0	0	0	0.00	0.2095
01725	35,985	4.58	164,820	0	31,982	0	0	0	0.00	0.2095
01726	33,538	4.95	165,891	0	39,118	0	0	0	0.00	0.2095
01727	30,246	5.51	166,606	0	43,890	0	0	0	0.00	0.2095
01728	26,345	6.33	166,833	0	45,402	0	0	0	0.00	0.2095
01729	16,666	9.74	162,254	0	14,872	0	0	0	0.00	0.2095
01730	21,553	7.61	164,056	0	26,888	0	0	0	0.00	0.2095
01731	20,803	7.94	165,130	0	34,045	0	0	0	0.00	0.2095
01732	19,090	8.69	165,957	0	39,557	0	0	0	0.00	0.2095
01733	17,018	9.78	166,373	0	42,333	0	0	0	0.00	0.2095
01734	14,885	11.19	166,531	0	43,388	0	0	0	0.00	0.2095
01735	8,563	19.04	163,032	0	20,059	0	0	0	0.00	0.2095
01736	6,786	24.24	164,501	0	29,854	0	0	0	0.00	0.2095
01737	6,278	26.35	165,430	0	36,048	0	0	0	0.00	0.2095
01738	5,604	29.63	166,047	0	40,158	0	0	0	0.00	0.2095
01739	4,964	32.65	162,099	0	13,837	0	0	0	0.00	0.2095
01740	12,812	12.72	162,995	0	19,811	0	0	0	0.00	0.2095
01741	8,561	19.15	163,984	0	26,408	0	0	0	0.00	0.2095
01742	7,704	21.42	164,992	0	33,128	0	0	0	0.00	0.2095
01743	7,199	23.03	165,770	0	38,313	0	0	0	0.00	0.2095
01744	6,597	25.19	166,168	0	40,966	0	0	0	0.00	0.2095
01745	6,339	26.24	166,342	0	42,124	0	0	0	0.00	0.2095
01746	23,641	6.87	162,427	0	16,027	0	0	0	0.00	0.2095
01747	22,536	7.30	164,589	0	30,443	0	0	0	0.00	0.2095
01748	21,124	7.84	165,564	0	36,939	0	0	0	0.00	0.2095
01749	19,301	8.61	166,207	0	41,227	0	0	0	0.00	0.2095
01750	17,460	9.53	166,404	0	42,538	0	0	0	0.00	0.2095
01751	42,353	3.85	163,268	0	21,636	0	0	0	0.00	0.2095
01752	38,360	4.28	164,211	0	27,921	0	0	0	0.00	0.2095
01753	35,813	4.62	165,376	0	35,686	0	0	0	0.00	0.2095
01754	32,979	5.04	166,276	0	41,689	0	0	0	0.00	0.2095
01755	29,551	5.64	166,740	0	44,779	0	0	0	0.00	0.2095
01756	26,582	6.28	166,944	0	46,139	0	0	0	0.00	0.2095
01757	55,937	2.90	162,354	0	15,539	0	0	0	0.00	0.2095
01758	51,168	3.23	165,099	0	33,838	0	0	0	0.00	0.2095
01759	47,567	3.50	166,346	0	42,156	0	0	0	0.00	0.2095
01760	42,792	3.91	167,164	0	47,606	0	0	0	0.00	0.2095
01761	37,599	4.45	167,396	0	49,155	0	0	0	0.00	0.2095
01762	63,272	2.58	162,970	0	19,648	0	0	0	0.00	0.2095
01763	67,088	2.45	164,331	0	28,719	0	0	0	0.00	0.2095
01764	62,955	2.64	166,368	0	42,298	0	0	0	0.00	0.2095
01765	57,075	2.94	167,595	0	50,482	0	0	0	0.00	0.2095
01766	50,004	3.36	168,210	0	54,578	0	0	0	0.00	0.2095
01767	44,083	3.82	168,277	0	55,026	0	0	0	0.00	0.2095
01768	84,359	1.94	163,578	0	23,699	0	0	0	0.00	0.2095
01769	79,427	2.09	165,898	0	39,166	0	0	0	0.00	0.2095
01770	72,346	2.32	168,009	0	53,242	0	0	0	0.00	0.2095
01771	63,277	2.67	169,122	0	60,662	0	0	0	0.00	0.2095
01772	52,977	3.20	169,410	0	62,577	0	0	0	0.00	0.2095
01773	103,745	1.56	161,848	0	12,167	0	0	0	2.50	0.2095
01774	96,281	1.72	165,574	0	37,007	0	0	0	2.50	0.2095
01775	88,191	1.91	168,334	0	55,405	0	0	0	0.00	0.2095
01776	77,336	2.20	170,056	0	66,886	0	0	0	0.00	0.2095
01777	65,348	2.61	170,809	0	71,909	0	0	0	0.00	0.2095
01778	54,787	3.11	170,559	0	70,239	0	0	0	0.00	0.2095
01779	115,761	1.42	164,375	0	29,014	0	0	0	2.50	0.2095
01780	103,905	1.62	168,279	0	55,040	0	0	0	2.50	0.2095
01781	91,460	1.87	170,978	0	73,035	0	0	0	0.00	0.2095
01782	76,932	2.24	172,348	0	82,165	0	0	0	0.00	0.2095
01783	62,074	2.78	172,458	0	82,898	0	0	0	0.00	0.2095
01784	129,649	1.25	162,374	0	15,675	0	0	0	2.50	0.2095



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm <sup>2</sup> /cm]
01785	119,414	1.41	168,024	0	53,341	0	0	0	2.50	0.2095
01786	104,587	1.64	171,752	0	78,193	0	0	0	2.50	0.2095
01787	87,786	1.98	173,913	0	92,601	0	0	0	0.00	0.2095
01788	71,108	2.45	174,548	0	96,834	0	0	0	0.00	0.2095
01789	57,553	3.02	173,735	0	91,411	0	0	0	0.00	0.2095
01790	135,242	1.23	166,626	0	44,020	0	0	0	2.50	0.2095
01791	114,089	1.51	172,161	0	80,917	0	0	0	2.50	0.2095
01792	95,925	1.83	175,356	0	102,220	0	0	0	0.00	0.2095
01793	77,515	2.28	176,662	0	110,925	0	0	0	0.00	0.2095
01794	60,547	2.91	176,188	0	107,768	0	0	0	0.00	0.2095
01795	128,549	1.28	164,598	0	30,502	0	0	0	2.50	0.2095
01796	115,673	1.48	171,766	0	78,289	0	0	0	2.50	0.2095
01797	97,816	1.80	176,342	0	108,791	0	0	0	0.00	0.2095
01798	79,824	2.24	178,538	0	123,432	0	0	0	0.00	0.2095
01799	63,628	2.81	178,637	0	124,095	0	0	0	0.00	0.2095
01800	50,707	3.49	177,030	0	113,383	0	0	0	0.00	0.2095
01801	97,927	1.73	169,383	0	62,399	0	0	0	2.50	0.2095
01802	87,486	2.02	177,062	0	113,593	0	0	0	0.00	0.2095
01803	75,170	2.39	179,765	0	131,615	0	0	0	0.00	0.2095
01804	60,331	3.00	180,836	0	138,756	0	0	0	0.00	0.2095
01805	56,158	3.19	178,929	0	126,041	0	0	0	0.00	0.2095
Piano Fondo Vasca			Parete P2-P5			Parete P2-P5				
00001	108,918	1.27	137,906	0	-34,353	0	0	0	2.50	0.1341
00047	123,244	1.12	137,906	0	-74,725	0	0	0	2.50	0.1341
00049	17,917	7.78	139,408	0	10,013	0	0	0	0.00	0.1341
00050	19,143	7.27	139,174	0	8,449	0	0	0	0.00	0.1341
00474	95,605	1.44	137,906	0	-33,403	0	0	0	2.50	0.1341
00475	73,522	1.90	139,564	0	11,053	0	0	0	0.00	0.1341
00476	67,222	2.11	141,616	0	24,733	0	0	0	0.00	0.1341
00477	60,120	2.29	137,906	0	-15,406	0	0	0	0.00	0.1341
00478	55,186	2.50	137,906	0	-15,786	0	0	0	0.00	0.1341
00479	49,795	2.77	137,906	0	-17,571	0	0	0	0.00	0.1341
00480	44,952	3.07	137,906	0	-15,197	0	0	0	0.00	0.1341
00481	39,652	3.48	137,906	0	-13,246	0	0	0	0.00	0.1341
00482	35,036	3.94	137,906	0	-10,355	0	0	0	0.00	0.1341
00483	30,483	4.52	137,906	0	-8,401	0	0	0	0.00	0.1341
00484	25,856	5.33	137,906	0	-6,477	0	0	0	0.00	0.1341
00485	24,551	5.62	137,906	0	-3,170	0	0	0	0.00	0.1341
00486	23,195	5.95	137,906	0	-3,515	0	0	0	0.00	0.1341
00487	21,868	6.31	137,906	0	-3,483	0	0	0	0.00	0.1341
00488	21,032	6.56	137,906	0	-3,790	0	0	0	0.00	0.1341
00489	19,722	6.99	137,906	0	-4,288	0	0	0	0.00	0.1341
00490	19,390	7.11	137,906	0	-7,823	0	0	0	0.00	0.1341
00491	20,230	6.82	137,906	0	-7,261	0	0	0	0.00	0.1341
00492	21,508	6.41	137,906	0	-7,752	0	0	0	0.00	0.1341
00493	22,968	6.00	137,906	0	-7,296	0	0	0	0.00	0.1341
00494	24,063	5.73	137,906	0	-6,307	0	0	0	0.00	0.1341
00495	25,367	5.44	137,906	0	-6,700	0	0	0	0.00	0.1341
00496	26,815	5.14	137,906	0	-6,573	0	0	0	0.00	0.1341
00557	32,945	4.19	137,906	0	-11,686	0	0	0	0.00	0.1341
00558	27,783	4.96	137,906	0	-1,118	0	0	0	0.00	0.1341
00559	32,968	4.18	137,906	0	-5,951	0	0	0	0.00	0.1341
00560	27,849	4.95	137,906	0	-1,189	0	0	0	0.00	0.1341
00561	33,603	4.10	137,906	0	-3,443	0	0	0	0.00	0.1341
00562	29,587	4.66	137,906	0	-5,749	0	0	0	0.00	0.1341
00563	37,324	4.18	156,009	0	120,686	0	0	0	0.00	0.1341
00564	67,354	2.22	149,741	0	78,895	0	0	0	0.00	0.1341
00565	79,690	1.80	143,386	0	36,528	0	0	0	0.00	0.1341
00566	90,143	1.53	137,906	0	-13,555	0	0	0	2.50	0.1341
00567	74,429	1.91	142,328	0	29,477	0	0	0	0.00	0.1341
00568	66,729	2.14	142,649	0	31,620	0	0	0	0.00	0.1341
00569	59,350	2.32	137,906	0	-11,169	0	0	0	0.00	0.1341
00570	55,413	2.49	137,906	0	-15,499	0	0	0	0.00	0.1341
00571	50,333	2.74	137,906	0	-14,647	0	0	0	0.00	0.1341
00572	45,791	3.01	137,906	0	-14,168	0	0	0	0.00	0.1341
00573	40,902	3.37	137,906	0	-11,288	0	0	0	0.00	0.1341
00574	35,807	3.85	137,906	0	-9,916	0	0	0	0.00	0.1341
00575	31,987	4.31	137,906	0	-9,295	0	0	0	0.00	0.1341
00576	29,951	4.60	137,906	0	-5,030	0	0	0	0.00	0.1341
00577	28,204	4.89	137,906	0	-4,684	0	0	0	0.00	0.1341
00578	108,220	1.29	139,847	0	12,940	0	0	0	2.50	0.1341
00579	60,694	2.48	150,589	0	84,552	0	0	0	0.00	0.1341
00580	31,636	4.36	137,906	0	-7,814	0	0	0	0.00	0.1341
00581	34,180	4.03	137,906	0	-4,002	0	0	0	0.00	0.1341
00582	29,173	4.73	137,906	0	-2,390	0	0	0	0.00	0.1341
00583	33,650	4.10	137,906	0	-3,980	0	0	0	0.00	0.1341
00584	28,209	4.89	137,906	0	-1,207	0	0	0	0.00	0.1341



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm/cm]
00585	29,375	4.69	137,906	0	-11,106	0	0	0	0.00	0.1341
00586	32,173	4.29	137,906	0	-11,657	0	0	0	0.00	0.1341
00855	25,356	5.51	139,834	0	12,849	0	0	0	0.00	0.1341
00856	28,280	4.92	139,175	0	8,458	0	0	0	0.00	0.1341
00857	36,740	3.82	140,457	0	17,005	0	0	0	0.00	0.1341
00858	35,073	4.00	140,438	0	16,876	0	0	0	0.00	0.1341
00859	36,164	3.86	139,638	0	11,547	0	0	0	0.00	0.1341
00860	36,210	3.88	140,596	0	17,931	0	0	0	0.00	0.1341
00861	33,298	4.22	140,445	0	16,923	0	0	0	0.00	0.1341
00862	31,113	4.48	139,459	0	10,352	0	0	0	0.00	0.1341
00863	28,478	4.93	140,462	0	17,039	0	0	0	0.00	0.1341
00864	28,136	5.00	140,795	0	19,256	0	0	0	0.00	0.1341
00865	23,143	6.04	139,722	0	12,101	0	0	0	0.00	0.1341
00866	16,683	8.47	141,229	0	22,150	0	0	0	0.00	0.1341
00867	19,011	7.42	141,142	0	21,572	0	0	0	0.00	0.1341
00868	15,387	8.99	138,318	0	2,743	0	0	0	0.00	0.1341
00869	12,421	11.15	138,545	0	4,257	0	0	0	0.00	0.1341
00870	12,870	10.74	138,176	0	1,798	0	0	0	0.00	0.1341
00871	13,376	10.34	138,254	0	2,318	0	0	0	0.00	0.1341
00872	10,886	12.71	138,322	0	2,773	0	0	0	0.00	0.1341
00873	10,985	12.57	138,104	0	1,318	0	0	0	0.00	0.1341
00874	13,339	10.37	138,261	0	2,361	0	0	0	0.00	0.1341
00875	11,566	11.92	137,907	0	4	0	0	0	0.00	0.1341
00876	11,858	11.66	138,306	0	2,663	0	0	0	0.00	0.1341
00877	23,258	6.07	141,254	0	22,316	0	0	0	0.00	0.1341
00878	17,890	7.82	139,983	0	13,844	0	0	0	0.00	0.1341
00879	20,277	6.95	140,935	0	20,188	0	0	0	0.00	0.1341
00880	33,348	4.23	140,935	0	20,194	0	0	0	0.00	0.1341
00881	25,288	5.54	140,027	0	14,135	0	0	0	0.00	0.1341
00882	29,230	4.82	141,032	0	20,838	0	0	0	0.00	0.1341
00883	40,740	3.45	140,740	0	18,888	0	0	0	0.00	0.1341
00884	31,453	4.46	140,223	0	15,444	0	0	0	0.00	0.1341
00885	35,201	4.01	141,097	0	21,273	0	0	0	0.00	0.1341
00886	39,769	3.54	140,893	0	19,910	0	0	0	0.00	0.1341
00887	33,166	4.21	139,710	0	12,026	0	0	0	0.00	0.1341
00888	29,484	4.76	140,397	0	16,604	0	0	0	0.00	0.1341
00889	24,446	5.71	139,638	0	11,547	0	0	0	0.00	0.1341
02247	29,639	4.66	138,254	0	2,317	0	0	0	0.00	0.1341
02248	93,865	1.50	140,910	0	20,025	0	0	0	2.50	0.1341
02249	107,952	1.28	137,906	0	-20,201	0	0	0	2.50	0.1341
02250	33,660	4.10	137,906	0	-1,537	0	0	0	0.00	0.1341
02251	42,357	3.26	138,014	0	719	0	0	0	0.00	0.1341
02252	39,690	3.47	137,906	0	-5,002	0	0	0	0.00	0.1341
02253	41,981	3.28	137,906	0	-4,061	0	0	0	0.00	0.1341
02254	45,765	3.01	137,906	0	-2,794	0	0	0	0.00	0.1341
02255	73,734	2.04	150,229	0	82,153	0	0	0	0.00	0.1341
02256	94,463	1.50	141,867	0	26,407	0	0	0	2.50	0.1341
02257	53,688	2.57	137,906	0	-2,157	0	0	0	0.00	0.1341
02258	48,673	2.83	137,906	0	-4,367	0	0	0	0.00	0.1341
02259	50,655	2.72	137,906	0	-5,673	0	0	0	0.00	0.1341
02260	55,522	2.48	137,906	0	-7,910	0	0	0	0.00	0.1341
02261	72,787	1.98	143,949	0	40,282	0	0	0	0.00	0.1341
02262	58,986	2.35	138,877	0	6,474	0	0	0	0.00	0.1341
02263	55,011	2.51	137,906	0	-1,079	0	0	0	0.00	0.1341
02264	53,719	2.57	137,906	0	-5,913	0	0	0	0.00	0.1341
02265	54,746	2.52	137,906	0	-9,609	0	0	0	0.00	0.1341
02266	56,881	2.42	137,906	0	-13,541	0	0	0	0.00	0.1341
02267	57,260	2.41	137,906	0	-17,040	0	0	0	0.00	0.1341
02268	60,255	2.31	139,003	0	7,313	0	0	0	0.00	0.1341
02269	54,610	2.53	137,906	0	-2,285	0	0	0	0.00	0.1341
02270	53,770	2.56	137,906	0	-8,112	0	0	0	0.00	0.1341
02271	53,303	2.59	137,906	0	-12,678	0	0	0	0.00	0.1341
02272	52,591	2.62	137,906	0	-16,600	0	0	0	0.00	0.1341
02273	59,764	2.34	139,720	0	12,089	0	0	0	0.00	0.1341
02274	54,497	2.54	138,517	0	4,074	0	0	0	0.00	0.1341
02275	51,695	2.67	137,906	0	-3,944	0	0	0	0.00	0.1341
02276	49,738	2.77	137,906	0	-9,734	0	0	0	0.00	0.1341
02277	47,783	2.89	137,906	0	-13,675	0	0	0	0.00	0.1341
02278	45,087	3.06	137,906	0	-15,923	0	0	0	0.00	0.1341
02279	51,313	2.72	139,806	0	12,665	0	0	0	0.00	0.1341
02280	47,780	2.89	138,153	0	1,645	0	0	0	0.00	0.1341
02281	45,588	3.03	137,906	0	-5,318	0	0	0	0.00	0.1341
02282	43,061	3.20	137,906	0	-10,051	0	0	0	0.00	0.1341
02283	39,871	3.46	137,906	0	-12,703	0	0	0	0.00	0.1341
02284	48,144	2.91	140,219	0	15,416	0	0	0	0.00	0.1341
02285	42,456	3.28	139,055	0	7,658	0	0	0	0.00	0.1341
02286	40,386	3.41	137,906	0	-224	0	0	0	0.00	0.1341



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm/cm]
02287	38,027	3.63	137,906	0	-5,799	0	0	0	0.00	0.1341
02288	35,091	3.93	137,906	0	-8,916	0	0	0	0.00	0.1341
02289	31,781	4.34	137,906	0	-9,662	0	0	0	0.00	0.1341
02290	36,248	3.87	140,219	0	15,420	0	0	0	0.00	0.1341
02291	34,160	4.06	138,631	0	4,832	0	0	0	0.00	0.1341
02292	32,383	4.26	137,906	0	-1,336	0	0	0	0.00	0.1341
02293	29,897	4.61	137,906	0	-5,211	0	0	0	0.00	0.1341
02294	26,736	5.16	137,906	0	-6,654	0	0	0	0.00	0.1341
02295	32,560	4.32	140,529	0	17,487	0	0	0	0.00	0.1341
02296	27,829	5.01	139,361	0	9,700	0	0	0	0.00	0.1341
02297	26,130	5.30	138,361	0	3,031	0	0	0	0.00	0.1341
02298	24,249	5.69	137,906	0	-1,593	0	0	0	0.00	0.1341
02299	22,749	6.06	137,906	0	-2,410	0	0	0	0.00	0.1341
02300	23,006	5.99	137,906	0	-3,249	0	0	0	0.00	0.1341
02301	21,666	6.38	138,198	0	1,944	0	0	0	0.00	0.1341
02302	20,742	6.65	137,906	0	-88	0	0	0	0.00	0.1341
02303	20,865	6.61	137,906	0	-1,255	0	0	0	0.00	0.1341
02304	21,026	6.56	137,906	0	-2,239	0	0	0	0.00	0.1341
02305	21,251	6.49	137,906	0	-3,108	0	0	0	0.00	0.1341
02306	19,330	7.15	138,221	0	2,100	0	0	0	0.00	0.1341
02307	19,151	7.20	137,977	0	468	0	0	0	0.00	0.1341
02308	19,196	7.18	137,906	0	-793	0	0	0	0.00	0.1341
02309	19,309	7.14	137,906	0	-1,904	0	0	0	0.00	0.1341
02310	19,473	7.08	137,906	0	-2,844	0	0	0	0.00	0.1341
02311	19,638	7.02	137,906	0	-3,873	0	0	0	0.00	0.1341
02312	19,284	7.15	137,921	0	97	0	0	0	0.00	0.1341
02313	18,561	7.43	137,906	0	-1,292	0	0	0	0.00	0.1341
02314	18,856	7.31	137,906	0	-2,868	0	0	0	0.00	0.1341
02315	19,155	7.20	137,906	0	-4,435	0	0	0	0.00	0.1341
02316	19,464	7.09	137,906	0	-6,157	0	0	0	0.00	0.1341
02317	19,594	7.05	138,112	0	1,368	0	0	0	0.00	0.1341
02318	20,061	6.87	137,906	0	-140	0	0	0	0.00	0.1341
02319	20,296	6.79	137,906	0	-1,846	0	0	0	0.00	0.1341
02320	20,593	6.70	137,906	0	-3,456	0	0	0	0.00	0.1341
02321	20,906	6.60	137,906	0	-4,994	0	0	0	0.00	0.1341
02322	21,308	6.47	137,906	0	-6,838	0	0	0	0.00	0.1341
02323	22,619	6.10	137,949	0	282	0	0	0	0.00	0.1341
02324	21,760	6.34	137,906	0	-789	0	0	0	0.00	0.1341
02325	22,082	6.25	137,906	0	-2,371	0	0	0	0.00	0.1341
02326	22,464	6.14	137,906	0	-3,921	0	0	0	0.00	0.1341
02327	22,923	6.02	137,906	0	-5,589	0	0	0	0.00	0.1341
02328	22,527	6.13	138,138	0	1,547	0	0	0	0.00	0.1341
02329	23,157	5.96	137,947	0	268	0	0	0	0.00	0.1341
02330	23,389	5.90	137,906	0	-1,264	0	0	0	0.00	0.1341
02331	23,815	5.79	137,906	0	-2,746	0	0	0	0.00	0.1341
02332	24,338	5.67	137,906	0	-4,239	0	0	0	0.00	0.1341
02333	24,935	5.53	137,906	0	-6,014	0	0	0	0.00	0.1341
02334	30,480	4.58	139,645	0	11,590	0	0	0	0.00	0.1341
02335	26,848	5.17	138,883	0	6,514	0	0	0	0.00	0.1341
02336	25,466	5.42	138,042	0	903	0	0	0	0.00	0.1341
02337	25,566	5.39	137,906	0	-2,931	0	0	0	0.00	0.1341
02338	26,418	5.22	137,906	0	-4,579	0	0	0	0.00	0.1341
02339	32,920	4.27	140,628	0	18,147	0	0	0	0.00	0.1341
02340	34,426	4.05	139,255	0	8,988	0	0	0	0.00	0.1341
02341	33,388	4.14	138,218	0	2,075	0	0	0	0.00	0.1341
02342	31,406	4.39	137,906	0	-2,884	0	0	0	0.00	0.1341
02343	28,552	4.83	137,906	0	-5,511	0	0	0	0.00	0.1341
02344	28,074	4.91	137,906	0	-4,363	0	0	0	0.00	0.1341
02345	46,057	3.05	140,324	0	16,117	0	0	0	0.00	0.1341
02346	40,809	3.39	138,521	0	4,095	0	0	0	0.00	0.1341
02347	39,027	3.53	137,906	0	-2,413	0	0	0	0.00	0.1341
02348	36,717	3.76	137,906	0	-6,652	0	0	0	0.00	0.1341
02349	33,781	4.08	137,906	0	-8,805	0	0	0	0.00	0.1341
02350	44,459	3.16	140,302	0	15,970	0	0	0	0.00	0.1341
02351	47,776	2.91	138,874	0	6,451	0	0	0	0.00	0.1341
02352	46,105	2.99	137,906	0	-1,221	0	0	0	0.00	0.1341
02353	43,948	3.14	137,906	0	-6,725	0	0	0	0.00	0.1341
02354	41,589	3.32	137,906	0	-10,105	0	0	0	0.00	0.1341
02355	38,331	3.60	137,906	0	-11,398	0	0	0	0.00	0.1341
02356	50,485	2.78	140,242	0	15,570	0	0	0	0.00	0.1341
02357	51,791	2.66	137,983	0	512	0	0	0	0.00	0.1341
02358	49,735	2.77	137,906	0	-5,829	0	0	0	0.00	0.1341
02359	48,135	2.86	137,906	0	-10,191	0	0	0	0.00	0.1341
02360	46,431	2.97	137,906	0	-13,192	0	0	0	0.00	0.1341
02361	53,931	2.59	139,746	0	12,261	0	0	0	0.00	0.1341
02362	55,385	2.49	138,180	0	1,821	0	0	0	0.00	0.1341
02363	53,072	2.60	137,906	0	-4,507	0	0	0	0.00	0.1341



Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo										
Nodo	Ty	CS	Vcc	Vwd	N	Vwp	Vr1	Vfd	Ctgθ	AfTE
	[N]		[N]	[N]	[N]	[N]	[N]	[N]		[cm²/cm]
02364	52,118	2.65	137,906	0	-8,897	0	0	0	0.00	0.1341
02365	51,956	2.65	137,906	0	-12,239	0	0	0	0.00	0.1341
02366	50,459	2.73	137,906	0	-14,552	0	0	0	0.00	0.1341
02367	59,671	2.32	138,527	0	4,135	0	0	0	0.00	0.1341
02368	52,844	2.61	137,906	0	-3,407	0	0	0	0.00	0.1341
02369	52,295	2.64	137,906	0	-6,721	0	0	0	0.00	0.1341
02370	53,958	2.56	137,906	0	-9,470	0	0	0	0.00	0.1341
02371	56,220	2.45	137,906	0	-12,479	0	0	0	0.00	0.1341
02372	51,305	2.70	138,653	0	4,978	0	0	0	0.00	0.1341
02373	48,290	2.86	137,906	0	-3,373	0	0	0	0.00	0.1341
02374	47,702	2.89	137,906	0	-4,578	0	0	0	0.00	0.1341
02375	50,644	2.72	137,906	0	-5,599	0	0	0	0.00	0.1341
02376	62,104	2.38	147,655	0	64,991	0	0	0	0.00	0.1341
02377	68,202	2.11	143,596	0	37,929	0	0	0	0.00	0.1341
02378	42,291	3.26	137,906	0	-6,267	0	0	0	0.00	0.1341
02379	39,645	3.48	137,906	0	-5,493	0	0	0	0.00	0.1341
02380	42,611	3.24	137,906	0	-3,173	0	0	0	0.00	0.1341
02381	55,887	2.72	151,888	0	93,214	0	0	0	0.00	0.1341
02382	84,438	1.74	146,953	0	60,314	0	0	0	0.00	0.1341

## LEGENDA Pareti - Verifiche a taglio per pressoflessione retta allo stato limite ultimo

<b>Ty</b>	Valore della sollecitazione di taglio.
<b>CS</b>	Coefficienti di sicurezza relativi alle sollecitazioni "Ty": [NS] = Non Significativo - Per valori di CS maggiori o uguali a 100.
<b>Vcc</b>	Valori massimo e minimo del taglio ultimo, per conglomerato compresso.
<b>Vwd</b>	Contributi dell'acciaio al taglio ultimo dovuto alle staffe, relativi alle sollecitazioni "Ty".
<b>N</b>	Sforzo normale utilizzato per il calcolo di AlfaC.
<b>Vwp</b>	Contributi dell'acciaio al taglio ultimo dovuti ai ferri piegati, relativi alle sollecitazioni "Ty".
<b>Vr1</b>	Taglio Massimo in assenza di ARMATURA incrociata.
<b>Vfd</b>	Contributo acciaio al Taglio ultimo dovuto al rinforzo in FRP.
<b>Ctg θ</b>	Cotangente di θ utilizzata nel calcolo di Vcc, Vwd e Vwp, relativi alle sollecitazioni "Ty".
<b>AfTE</b>	Aree di ferro per il taglio in un centimetro, relativi alle sollecitazioni "Ty".

## SOLETTE - VERIFICHE PRESSOFLESSIONE RETTA ALLO STATO LIMITE ULTIMO (Elevazione)

Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
Piano Terra																
SolettaP1-P2-P5-P4																
P	S	00051	92,08 5	835	0.080 44	54.68	00052	0	0	0.080 44	-	00054	76,80 1	970	0.080 44	48.35
	I		118,6 31	1,315	0.080 44	33.09		-7,126	3,437	0.080 44	15.61		97,93 1	1,763	0.080 44	25.63
S	S		- 145,6 70	11,44 8	0.080 44	5.65		0	0	0.080 44	-		- 126,5 87	10,84 9	0.080 44	5.83
	I		143,8 45	15,26 5	0.080 44	2.72		- 70,49 2	12,00 9	0.080 44	4.89		94,92 5	14,60 2	0.080 44	3.11
P	S	00056	18,87 0	1,381	0.080 44	37.35	00057	- 34,37 1	2,795	0.080 44	19.98	00058	- 43,27 4	3,044	0.080 44	18.58
	I		- 47,18 7	719	0.080 44	79.11		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 35,40 4	3,331	0.080 44	16.79		- 10,34 1	10,19 8	0.080 44	5.29		19,87 9	18,87 3	0.080 44	2.73
	I		- 38,26 0	3,672	0.080 44	15.30		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00059	- 42,91 9	2,755	0.080 44	20.52	00060	- 64,87 9	3,692	0.080 44	15.79	00061	- 43,74 1	3,242	0.080 44	17.46
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 21,30 0	18,53 7	0.080 44	2.96		2,082	8,452	0.080 44	6.26		- 48,11 2	18,83 6	0.080 44	3.02
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00062	- 64,95 5	2,932	0.080 44	19.89	00063	23,30 6	793	0.080 44	64.59	00064	0	0	0.080 44	-
	I		0	0	0.080 44	-		30,50 3	219	0.080 44	NS		62,96 4	1,150	0.080 44	41.75
S	S		- 28,75 8	18,71 9	0.080 44	2.96		- 27,44 8	10,09 8	0.080 44	5.48		- 69,36 5	2,039	0.080 44	28.77
	I		0	0	0.080	-		-1.989	1.481	0.080	35.96		51.50	10.18	0.080	4.80



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
					44					44			7	7	44	
P	S	00094	-	440	0.080	NS	00095	-	1,990	0.080	28.29	00096	-	3,279	0.080	16.92
			31,075			39,841				29,655						
	I		-	1,004	0.080	56.61		-	26	0.080	NS		0	0	0.080	-
			46,620				24,342									
S	S		4,121	3,281	0.080	16.08		-	10,113	0.080	5.34		7,214	16,229	0.080	3.24
							10,770									
	I		-	5,584	0.080	10.21		0	0	0.080	-		0	0	0.080	-
			48,623													
P	S	00097	-	4,335	0.080	12.90	00098	-	3,475	0.080	16.32	00099	-	3,258	0.080	17.82
			35,143			45,093				61,978						
I	0		0	0.080	-	0		0	0.080	-	0		0	0.080	-	
S	S		-4,888	18,088	0.080	2.96		2,329	8,272	0.080	6.40		-	17,105	0.080	3.31
													43,602	0	0.080	-
	I		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-
P	S	00100	-	3,771	0.080	15.38	00101	-	1,110	0.080	48.57	00102	0	0	0.080	-
			61,261			10,213				77,263						
I	0		0	0.080	-	-		308	0.080	NS	910		0.080	51.49		
							12,829									
S	S		-	19,419	0.080	2.84		-	9,435	0.080	5.74		-	1,928	0.080	30.16
			24,631				13,466						62,949			
	I		0	0	0.080	-		-8,734	1,126	0.080	47.78		36,249	6,583	0.080	7.62
P	S	00103	-	10,089	0.080	5.48	00104	16,346	9,008	0.080	5.75	00105	39,946	21,131	0.080	2.36
			27,823			0		0	0.080	-	0		0	0.080	-	
I	-		2,031	0.080	27.63											
			37,728													
S	S		73,240	6,731	0.080	7.01		109,021	3,785	0.080	11.70		5,514	4,898	0.080	10.75
			0					0	0	0.080	-		0	0	0.080	-
	I		-	3,512	0.080	17.82										
			118,847													
P	S	00106	-	26,558	0.080	2.03	00107	26,552	28,705	0.080	1.78	00108	14,310	31,060	0.080	1.67
			11,164			0		0	0.080	-	0		0	0.080	-	
I	0		0	0.080	-											
S	S		79,311	6,520	0.080	7.16		8,492	6,726	0.080	7.79		7,053	5,917	0.080	8.88
	I		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-
P	S	00109	103,101	33,342	0.080	1.34	00110	1,149	35,592	0.080	1.49	00111	14,394	34,090	0.080	1.52
			0	0	0.080	-		0	0	0.080	-		0	0	0.080	-
I																
			984	7,612	0.080	6.96		-	7,480	0.080	7.25		55,102	9,224	0.080	5.27
								14,567								
	I		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-
P	S	00112	15,857	35,783	0.080	1.45	00113	9,484	34,622	0.080	1.51	00114	7,482	35,694	0.080	1.47
			0	0	0.080	-		0	0	0.080	-		0	0	0.080	-
I																
S	S		-	7,633	0.080	7.12		-	7,661	0.080	7.13		-7,880	8,900	0.080	6.04
			15,354					19,455								
	I		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-
P	S	00115	3,815	36,137	0.080	1.46	00116	3,675	36,747	0.080	1.44	00117	-2,575	35,182	0.080	1.52
			0	0	0.080	-		0	0	0.080	-		0	0	0.080	-
I																
S	S		-8,616	7,034	0.080	7.65		-3,759	8,067	0.080	6.62		30,771	9,818	0.080	5.16
	I		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-
P	S	00118	6,241	34,75	0.080	1.51	00119	8,447	34,31	0.080	1.53	00120	-7,118	36,19	0.080	1.48



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	I		0	8 0	44 0.080 44	-		0	7 0	44 0.080 44	-		0	4 0	44 0.080 44	-
S	S		- 11,75 6	7,300	0.080 44	7.40		47,08 7	8,983	0.080 44	5.49		- 10,09 5	7,321	0.080 44	7.36
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00121	-906	34,42 8	0.080 44	1.54	00122	8,954	34,02 7	0.080 44	1.54	00123	52,77 7	31,87 3	0.080 44	1.53
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 13,17 0	7,150	0.080 44	7.57		5,916	6,219	0.080 44	8.46		9,203	7,398	0.080 44	7.08
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00124	333	30,71 2	0.080 44	1.73	00125	57,40 6	26,62 3	0.080 44	1.82	00126	42,07 5	18,22 6	0.080 44	2.73
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		75,42 1	8,176	0.080 44	5.75		1,697	6,139	0.080 44	8.63		70,64 0	6,273	0.080 44	7.56
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00127	1,443	17,47 0	0.080 44	3.03	00128	- 93,88 7	11,85 5	0.080 44	5.11	00137	0	0	0.080 44	-
	I		0	0	0.080 44	-		- 693 10,48 6	0.080 44	77.83		54,06 1	3,749	0.080 44	13.00	
S	S		27,43 9	2,786	0.080 44	18.26		120,1 10	4,584	0.080 44	9.47		0	0	0.080 44	-
	I		0	0	0.080 44	-		- 1,380 111,4 49	0.080 44	44.94		33,30 6	2,760	0.080 44	18.26	
P	S	00379	1,251	465	0.080 44	NS	00380	18,09 4	90	0.080 44	NS	00381	- 37,26 0	11,22 6	0.080 44	5.00
	I		- 49,70 5	2,240	0.080 44	25.48		11,71 2	1,030	0.080 44	50.63		0	0	0.080 44	-
S	S		- 12,19 9	2,761	0.080 44	19.59		16,24 5	52	0.080 44	NS		- 41,46 6	1,546	0.080 44	36.50
	I		- 80,19 4	9,225	0.080 44	6.45		16,24 5	76	0.080 44	NS		0	0	0.080 44	-
P	S	00382	- 43,92 7	22,93 6	0.080 44	2.47	00383	-9,100	24,12 2	0.080 44	2.23	00384	-2,532	30,59 3	0.080 44	1.74
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 47,98 9	3,930	0.080 44	14.49		- 43,19 0	5,676	0.080 44	9.97		- 34,91 4	7,050	0.080 44	7.93
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00385	-164	35,75 3	0.080 44	1.49	00386	21,15 0	34,09 9	0.080 44	1.51	00387	7,633	37,22 7	0.080 44	1.41
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 35,58 2	7,226	0.080 44	7.74		- 30,31 0	7,405	0.080 44	7.50		- 27,72 0	9,086	0.080 44	6.09
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00388	-4,297	37,36 7	0.080 44	1.43	00389	3,569	40,87 8	0.080 44	1.29	00390	5,431	40,24 6	0.080 44	1.31
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 30,88 3	9,079	0.080 44	6.12		- 21,59 3	7,911	0.080 44	6.93		- 23,06 6	9,854	0.080 44	5.58
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00391	-1,604	40,37 6	0.080 44	1.32	00392	2,337	42,79 0	0.080 44	1.24	00393	1,187	40,83 6	0.080 44	1.30
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		-	9,657	0.080	5.74		-	8,434	0.080	6.48		-	10,02	0.080	5.46



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
			29,67		44			19,03		44			20,23	0	44	
	I		4	0	0.080	-		0	0	0.080	-		9	0	0.080	-
			0		44			0		44			0		44	
P	S	00394	-847	41,52	0.080	1.28	00395	-2,283	42,26	0.080	1.26	00396	-4,500	46,02	0.080	1.16
	I		0	2	44			0	3	44			0	5	44	
				0	0.080	-			0	0.080	-		0	0	0.080	-
					44					44					44	
S	S		-	9,769	0.080	5.64		-	8,730	0.080	6.25		-	9,295	0.080	5.91
			24,36		44			18,37		44			23,16		44	
	I		8	0	0.080	-		2	0	0.080	-		6	0	0.080	-
			0		44			0		44			0		44	
P	S	00397	363	42,49	0.080	1.25	00398	316	42,32	0.080	1.25	00399	-3,120	46,20	0.080	1.15
	I		0	7	44			0	7	44			0	1	44	
				0	0.080	-			0	0.080	-		0	0	0.080	-
					44					44					44	
S	S		-	9,846	0.080	5.56		-	8,893	0.080	6.14		-	9,200	0.080	5.97
			20,77		44			19,16		44			22,89		44	
	I		8	0	0.080	-		9	0	0.080	-		2	0	0.080	-
			0		44			0		44			0		44	
P	S	00400	-155	42,46	0.080	1.25	00401	2,459	41,95	0.080	1.26	00402	-4,854	46,17	0.080	1.16
	I		0	5	44			0	6	44			0	9	44	
				0	0.080	-			0	0.080	-		0	0	0.080	-
					44					44					44	
S	S		-	9,549	0.080	5.72		-	8,967	0.080	6.11		-	9,190	0.080	5.99
			18,95		44			21,28		44			24,34		44	
	I		8	0	0.080	-		5	0	0.080	-		6	0	0.080	-
			0		44			0		44			0		44	
P	S	00403	-2,118	41,67	0.080	1.28	00404	4,078	40,86	0.080	1.29	00405	-4,424	44,47	0.080	1.20
	I		0	9	44			0	6	44			0	0	44	
				0	0.080	-			0	0.080	-		0	0	0.080	-
					44					44					44	
S	S		-	8,999	0.080	6.07		-	8,994	0.080	6.12		-	8,792	0.080	6.27
			19,24		44			23,87		44			25,35		44	
	I		5	0	0.080	-		6	0	0.080	-		0	0	0.080	-
			0		44			0		44			0		44	
P	S	00406	-6,646	39,74	0.080	1.35	00407	3,214	37,28	0.080	1.42	00408	-5,341	39,33	0.080	1.36
	I		0	0	44			0	2	44			0	1	44	
				0	0.080	-			0	0.080	-		0	0	0.080	-
					44					44					44	
S	S		-	8,289	0.080	6.59		-	8,620	0.080	6.41		-	7,869	0.080	7.01
			19,04		44			26,72		44			25,75		44	
	I		6	0	0.080	-		2	0	0.080	-		2	0	0.080	-
			0		44			0		44			0		44	
P	S	00409	-6,529	33,19	0.080	1.62	00410	-2,252	27,60	0.080	1.93	00411	-3,589	21,90	0.080	2.44
	I		0	5	44			0	5	44			0	8	44	
				0	0.080	-			0	0.080	-		0	0	0.080	-
					44					44					44	
S	S		-	6,645	0.080	8.21		-	6,699	0.080	8.20		-	6,335	0.080	8.55
			18,51		44			23,15		44			13,41		44	
	I		7	0	0.080	-		4	0	0.080	-		5	0	0.080	-
			0		44			0		44			0		44	
P	S	00412	-9,409	18,18	0.080	2.96	00413	-	9,716	0.080	5.66	00414	-	6,677	0.080	8.25
	I		0	6	44			23,09		44			24,86		44	
				0	0.080	-		6	0	0.080	-		2	1,026	0.080	53.20
					44					44			18,46		44	
S	S		-8,591	3,232	0.080	16.64		-	2,006	0.080	27.50		7,827	488	0.080	NS
					44			25,77		44					44	
	I		0	0	0.080	-		5	0	0.080	-		0	0	0.080	-
					44			0		44					44	
P	S	00415	71,83	17,47	0.080	2.71	00609	-	770	0.080	74.11	00610	-1,928	1,289	0.080	41.31
	I		2	7	44			49,41		44					44	
					44			4		44					44	
				8,125	0.080	7.76			36	0.080	NS			271	0.080	NS
			124,4		44			108,4		44			16,18		44	
			78					62					3			
S	S		66,66	5,785	0.080	8.25		-	8,139	0.080	7.16		224	1,654	0.080	32.09
			8		44			64,36		44					44	
	I			4,829	0.080	12.89		1		44					44	
					44				525	0.080	NS			1,105	0.080	55.00
			114,3					336,7		44			-		44	
			10					71					95,94			
													6			



Solette - Verifiche pressoflessione retta allo stato limite ultimo																	
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]		
P	S	00611	4,232	192	0.080	NS	00612	0	0	0.080	-	00613	0	0	0.080	-	
	I		2,066	187	0.080	NS		2,986	1,201	0.080	44.01		3,484	452	0.080	NS	
S	S		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-	
	I	00614	5,600	1,670	0.080	31.52	00615	-7,992	3,481	0.080	15.44	00616	-3,756	4,564	0.080	11.70	
P	S		0	0	0.080	-		0	0	0.080	-		155	618	0.080	85.89	
	I		3,099	402	0.080	NS		7,973	1,202	0.080	43.64		0	0	0.080	-	
S	S	00617	0	0	0.080	-	00618	0	0	0.080	-	00619	0	0	0.080	-	
	I		-8,532	5,049	0.080	10.65		-	0	0	0.080		-	0	0	0.080	-
P	S		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-	
	I	00620	166	1,038	0.080	51.14	00621	2,041	541	0.080	97.84	00622	487	917	0.080	57.86	
S	S		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-	
	I		20,540	1,225	0.080	41.99		49,978	1,023	0.080	47.96		67,628	2,392	0.080	19.92	
P	S	00623	744	154	0.080	NS	00624	0	0	0.080	-	00625	0	0	0.080	-	
	I		4,175	29	0.080	NS		47	148	0.080	NS		304	714	0.080	74.33	
S	S		0	0	0.080	-		98,369	169	0.080	NS		88,322	112	0.080	NS	
	I	00626	66,138	1,741	0.080	27.43	00627	98,736	1,416	0.080	31.86	00628	87,897	1,304	0.080	35.27	
P	S		0	0	0.080	-		0	0	0.080	-		685	50	0.080	NS	
	I		6,992	690	0.080	76.13		5,595	579	0.080	90.92		3,189	84	0.080	NS	
S	S	00629	122,660	66	0.080	NS	00630	128,302	202	0.080	NS	00631	136,370	512	0.080	82.17	
	I		118,926	1,045	0.080	41.61		130,604	806	0.080	52.78		139,049	287	0.080	NS	
P	S		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-	
	I	00632	4,741	243	0.080	NS	00633	2,969	553	0.080	95.58	00634	10,696	775	0.080	67.40	
S	S		155,934	491	0.080	82.45		142,832	469	0.080	88.58		171,284	476	0.080	82.43	
	I		160,803	207	0.080	NS		146,198	268	0.080	NS		177,704	183	0.080	NS	
P	S	00635	0	0	0.080	-	00636	0	0	0.080	-	00637	0	0	0.080	-	
	I		7,783	331	0.080	NS		3,473	216	0.080	NS		969	446	0.080	NS	
S	S		167,014	462	0.080	85.68		194,515	702	0.080	53.20		170,776	607	0.080	64.71	
	I	00638	171,881	100	0.080	NS	00639	13,595	468	0.080	NS	00640	10,421	891	0.080	58.65	
P	S		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-	
	I		11,231	807	0.080	64.67		2,846	539	0.080	98.08		8,372	189	0.080	NS	
S	S	00639	195,702	607	0.080	61.37	00640	189,896	708	0.080	53.28	00641	207,250	532	0.080	68.26	
	I		15,361	893	0.080	58.07		14,464	847	0.080	61.31		16,455	657	0.080	78.80	
P	S		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-	
	I	00642	3,248	243	0.080	NS	00643	6,729	328	0.080	NS	00644	12,101	834	0.080	62.49	
S	S		213,928	855	0.080	41.84		188,129	746	0.080	50.76		206,516	664	0.080	54.78	
	I		19,239	455	0.080	NS		15,918	912	0.080	56.81		21,220	945	0.080	54.38	
P	S	00645	0	0	0.080	-	00646	0	0	0.080	-	00647	0	0	0.080	-	
	I		4,810	450	0.080	NS		5,185	231	0.080	NS		4,990	228	0.080	NS	
S	S		186,482	766	0.080	49.61		210,156	639	0.080	56.46		203,992	675	0.080	54.19	
	I	00648	17,055	994	0.080	52.03	00649	20,425	660	0.080	77.95	00650	18,021	652	0.080	79.21	
P	S		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-	
	I		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-	



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
P	S	00641	0	0	0.080	-	00642	0	0	0.080	-	00643	0	0	0.080	-
	I		5,264	459	0.080	NS		10,899	840	0.080	62.16		870	590	0.080	89.87
S	S		183,674	681	0.080	56.14		190,390	608	0.080	61.98		164,001	588	0.080	67.73
	I		15,011	1,025	0.080	50.62		15,798	1,033	0.080	50.17		169,929	24	0.080	NS
P	S	00644	0	0	0.080	-	00645	0	0	0.080	-	00646	0	0	0.080	-
	I		3,403	240	0.080	NS		5,942	172	0.080	NS		449	766	0.080	69.27
S	S		180,673	747	0.080	51.51		159,260	660	0.080	60.93		155,231	456	0.080	88.90
	I		12,784	763	0.080	68.24		8,530	1,039	0.080	50.44		159,873	344	0.080	NS
P	S	00647	0	0	0.080	-	00648	0	0	0.080	-	00649	417	21	0.080	NS
	I		7,489	846	0.080	62.05		182	704	0.080	75.40		3,063	111	0.080	NS
S	S		144,956	317	0.080	NS		117,975	181	0.080	NS		125,493	427	0.080	NS
	I		149,072	612	0.080	67.06		119,094	852	0.080	51.02		127,298	625	0.080	68.49
P	S	00650	0	0	0.080	-	00651	0	0	0.080	-	00652	0	0	0.080	-
	I		7,591	650	0.080	80.74		7,777	853	0.080	61.51		291	999	0.080	53.12
S	S		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-
	I		109,517	1,302	0.080	33.98		101,859	1,621	0.080	27.68		61,858	1,897	0.080	25.36
P	S	00653	0	0	0.080	-	00654	233	192	0.080	NS	00655	0	0	0.080	-
	I		3,942	365	0.080	NS		0	0	0.080	-		1,299	1,450	0.080	36.54
S	S		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-
	I		82,584	803	0.080	57.82		51,723	988	0.080	49.52		48,787	1,230	0.080	39.97
P	S	00656	0	0	0.080	-	00657	0	0	0.080	-	00658	1,511	54	0.080	NS
	I		2,674	767	0.080	68.94		757	1,525	0.080	34.78		189	48	0.080	NS
S	S		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-
	I		27,526	1,399	0.080	36.37		-10,404	4,739	0.080	11.38		-5,682	5,099	0.080	10.50
P	S	00659	0	0	0.080	-	00660	0	0	0.080	-	00661	0	0	0.080	-
	I		2,608	299	0.080	NS		1,880	1,130	0.080	46.85		-587	854	0.080	62.23
S	S		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-
	I		-1,467	4,597	0.080	11.58		-5,297	3,813	0.080	14.04		-1,137	1,765	0.080	30.13
P	S	00662	0	0	0.080	-	00663	-25,861	189	0.080	NS	00664	-137,096	558	0.080	NS
	I		6,017	1,223	0.080	43.02		0	0	0.080	-		0	0	0.080	-
S	S		-2,597	2,155	0.080	24.73		-69,265	9,349	0.080	6.27		-40,188	1,977	0.080	28.49
	I		-101,502	995	0.080	61.53		-294,978	306	0.080	NS		0	0	0.080	-
P	S	00665	-80,790	2,831	0.080	21.04	00666	-91,774	5,893	0.080	10.26	00667	-71,967	2,806	0.080	20.98
	I		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-
S	S		-9,156	2,688	0.080	20.03		0	0	0.080	-		1,502	2,296	0.080	23.07
	I		0	0	0.080	-		-4,963	1,711	0.080	31.26		0	0	0.080	-
P	S	00668	-90,917	243	0.080	NS	00669	5,140	307	0.080	NS	00670	7,080	1,307	0.080	40.19
	I		-28	0.080	NS	0		0	0.080	-	0		0	0.080	-	



Solette - Verifiche pressoflessione retta allo stato limite ultimo																	
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	
			[N] 78,74 8	[N-m]	[cm²/cm] 44			[N]	[N-m]	[cm²/cm] 44			[N]	[N-m]	[cm²/cm] 44		
S	S		- 19,21 0 0	1,907	0.080 44	28.65		27,44 6	8,765	0.080 44	5.81		76,24 3	1,283	0.080 44	36.59	
	I			0	0	0.080 44	-	0	0	0.080 44	-		64,93 5	717	0.080 44	66.74	
P	S		00671	0	0	0.080 44	-	00672	0	0	0.080 44	-	00673	0	0	0.080 44	-
	I		2,930	249	0.080 44	NS		6,817	1,159	0.080 44	45.34		7,873	452	0.080 44	NS	
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-	
	I			90,88 8	1,642	0.080 44	27.87		74,27 0	3,600	0.080 44	13.08		89,03 1	4,744	0.080 44	9.68
P	S		00674	0	0	0.080 44	-	00675	0	0	0.080 44	-	00676	1,333	590	0.080 44	89.81
	I		6,566	240	0.080 44	NS		3,684	1,280	0.080 44	41.25		0	0	0.080 44	-	
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-	
	I			81,85 3	5,288	0.080 44	8.79		65,94 8	5,023	0.080 44	9.51		79,35 2	2,628	0.080 44	17.77
P	S		00677	0	0	0.080 44	-	00678	0	0	0.080 44	-	00679	0	0	0.080 44	-
	I		4,847	986	0.080 44	53.45		5,385	383	0.080 44	NS		1,448	858	0.080 44	61.74	
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-	
	I			66,84 5	2,275	0.080 44	20.97		66,99 3	2,068	0.080 44	23.06		52,50 9	1,922	0.080 44	25.42
P	S		00680	797	152	0.080 44	NS	00681	0	0	0.080 44	-	00682	0	0	0.080 44	-
	I		0	0	0.080 44	-		1,747	72	0.080 44	NS		1,771	652	0.080 44	81.21	
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-	
	I			48,39 8	2,941	0.080 44	16.73		50,70 0	1,404	0.080 44	34.90		35,06 6	2,264	0.080 44	22.20
P	S		00683	0	0	0.080 44	-	00684	0	0	0.080 44	-	00685	196	52	0.080 44	NS
	I		2,784	570	0.080 44	92.75		1,032	661	0.080 44	80.20		0	0	0.080 44	-	
S	S		0	0	0.080 44	-		38,21 2	40	0.080 44	NS		41,93 5	392	0.080 44	NS	
	I			45,46 1	1,048	0.080 44	47.16		38,21 2	904	0.080 44	55.33		41,93 5	643	0.080 44	77.31
P	S		00686	0	0	0.080 44	-	00687	0	0	0.080 44	-	00688	0	0	0.080 44	-
	I		1,403	202	0.080 44	NS		95	521	0.080 44	NS		2,076	683	0.080 44	77.49	
S	S		38,47 5	455	0.080 44	NS		36,03 7	425	0.080 44	NS		36,90 5	479	0.080 44	NS	
	I			38,47 5	536	0.080 44	93.27		36,03 7	548	0.080 44	91.59		36,90 5	429	0.080 44	NS
P	S		00689	0	0	0.080 44	-	00690	0	0	0.080 44	-	00691	0	0	0.080 44	-
	I		106	441	0.080 44	NS		571	134	0.080 44	NS		265	436	0.080 44	NS	
S	S		32,26 7	200	0.080 44	NS		36,36 7	934	0.080 44	53.71		31,21 7	610	0.080 44	82.91	
	I			32,26 7	34	0.080 44	NS		0	0	0.080 44	-		31,21 7	193	0.080 44	NS
P	S		00692	0	0	0.080 44	-	00693	0	0	0.080 44	-	00694	0	0	0.080 44	-
	I		2,122	713	0.080 44	74.23		56	613	0.080 44	86.61		1,403	137	0.080 44	NS	
S	S		34,29 4	635	0.080 44	79.26		30,63 3	715	0.080 44	70.80		31,88 1	814	0.080 44	62.07	
	I			34,29 4	180	0.080 44	NS		30,63 3	136	0.080 44	NS		31,88 1	21	0.080 44	NS
P	S		00695	0	0	0.080 44	-	00696	0	0	0.080 44	-	00697	0	0	0.080 44	-
	I		395	173	0.080 44	NS		165	477	0.080 44	NS		1,918	740	0.080 44	71.54	
S	S		32,86 6 0	1,020	0.080 44	49.46		29,06 0	689	0.080 44	73.66		32,14 8	691	0.080 44	73.09	
	I			0	0	0.080 44	-		29,06 0	104	0.080 44	NS		32,14 8	103	0.080 44	NS
P	S		00698	0	0	0.080 44	-	00699	0	0	0.080 44	-	00700	0	0	0.080 44	-



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
	I		[N] 106	[N-m] 495	[cm²/cm] 0.080 44	NS		[N] 794	[N-m] 184	[cm²/cm] 0.080 44	NS		[N] 687	[N-m] 134	[cm²/cm] 0.080 44	NS
S	S		28,78 9	690	0.080 44	73.59		31,30 7	901	0.080 44	56.13		30,99 9	898	0.080 44	56.34
	I		28,78 9	133	0.080 44	NS		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00701	0	0	0.080 44	-	00702	0	0	0.080 44	-	00703	0	0	0.080 44	-
	I		128	579	0.080 44	91.68		1,993	748	0.080 44	70.77		232	573	0.080 44	92.63
S	S		28,25 7	614	0.080 44	82.76		31,23 7	552	0.080 44	91.62		27,92 8	190	0.080 44	NS
	I		28,25 7	213	0.080 44	NS		31,23 7	245	0.080 44	NS		16,09 1	492	0.080 44	NS
P	S	00704	0	0	0.080 44	-	00705	0	0	0.080 44	-	00706	0	0	0.080 44	-
	I		495	182	0.080 44	NS		225	119	0.080 44	NS		119	728	0.080 44	72.92
S	S		31,39 4	696	0.080 44	72.65		30,57 0	486	0.080 44	NS		28,57 7	282	0.080 44	NS
	I		31,39 4	170	0.080 44	NS		30,57 0	373	0.080 44	NS		28,57 7	602	0.080 44	84.37
P	S	00707	0	0	0.080 44	-	00708	0	0	0.080 44	-	00709	196	74	0.080 44	NS
	I		2,215	736	0.080 44	71.90		516	725	0.080 44	73.18		0	0	0.080 44	-
S	S		31,34 8	137	0.080 44	NS		0	0	0.080 44	-		32,08 0	98	0.080 44	NS
	I		31,34 8	740	0.080 44	68.33		27,42 9	868	0.080 44	58.62		32,08 0	934	0.080 44	54.08
P	S	00710	0	0	0.080 44	-	00711	0	0	0.080 44	-	00712	0	0	0.080 44	-
	I		1,203	822	0.080 44	64.47		2,359	768	0.080 44	68.88		207	933	0.080 44	56.89
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
	I		16,73 1	2,177	0.080 44	23.77		20,87 2	2,655	0.080 44	19.36		18,62 5	3,186	0.080 44	16.19
P	S	00713	0	0	0.080 44	-	00714	698	254	0.080 44	NS	00715	0	0	0.080 44	-
	I		1,350	375	0.080 44	NS		0	0	0.080 44	-		1,288	1,272	0.080 44	41.66
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
	I		21,04 2	3,436	0.080 44	14.96		22,57 9	4,123	0.080 44	12.44		19,00 3	4,488	0.080 44	11.49
P	S	00716	0	0	0.080 44	-	00717	0	0	0.080 44	-	00718	1,254	125	0.080 44	NS
	I		3,218	661	0.080 44	79.93		1,500	1,393	0.080 44	38.03		0	0	0.080 44	-
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
	I		24,03 5	4,851	0.080 44	10.55		21,01 8	5,071	0.080 44	10.14		24,42 8	5,405	0.080 44	9.46
P	S	00719	0	0	0.080 44	-	00720	0	0	0.080 44	-	00721	0	0	0.080 44	-
	I		1,504	310	0.080 44	NS		2,171	985	0.080 44	53.72		4,956	753	0.080 44	69.98
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
	I		33,30 5	2,559	0.080 44	19.70		24,82 8	4,025	0.080 44	12.69		41,14 6	1,409	0.080 44	35.33
P	S	00722	0	0	0.080 44	-	00723	8,349	186	0.080 44	NS	00724	- 70,43 1	292	0.080 44	NS
	I		4,209	1,251	0.080 44	42.17		0	0	0.080 44	-		- 33,80 5	54	0.080 44	NS
S	S		30,20 5	2,062	0.080 44	24.57		36,42 9	8,772	0.080 44	5.72		4,764	1,330	0.080 44	39.63
	I		29,25 9	516	0.080 44	98.33		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00725	- 61,00 2	2,769	0.080 44	20.94	00726	- 67,13 1	2,771	0.080 44	21.10	00727	- 73,67 9	1,415	0.080 44	41.70
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		-4,707 0	3,565	0.080 44	15.00		-701 0	3,562	0.080 44	14.92		251 0	3,363	0.080 44	15.78
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-



Solette - Verifiche pressoflessione retta allo stato limite ultimo																			
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS			
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]				
P	S	00728	- 168,6 17 0	2,271	0.080 44	29.30	00891	-4,722	14,00 9	0.080 44	3.82	00892	26,52 3	33,66 5	0.080 44	1.51			
	I			0	0	0.080 44		-		0	0		0.080 44	-		0	0	0.080 44	-
S	S			0	0	0.080 44		-		- 29,33 6	2,582		0.080 44	21.48		1,240	5,812	0.080 44	9.12
	I		- 50,17 3	2,880	0.080 44	19.83		- 18,82 0	445	0.080 44	NS		0	0	0.080 44	-			
P	S	00894	8,609	32,49 9	0.080 44	1.61	00896	45,09 5	35,71 4	0.080 44	1.38	00898	- 22,65 8	38,40 4	0.080 44	1.43			
	I			0	0	0.080 44		-		0	0		0.080 44	-		0	0	0.080 44	-
S	S			48,97 4	9,956	0.080 44		4.94		5,885	7,507		0.080 44	7.01		-8,286	6,874	0.080 44	7.82
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-			
P	S	00901	-6,212	34,63 5	0.080 44	1.55	00902	5,443	34,53 1	0.080 44	1.52	00904	- 19,00 2	26,52 1	0.080 44	2.06			
	I			0	0	0.080 44		-		0	0		0.080 44	-		0	0	0.080 44	-
S	S			13,41 3	8,006	0.080 44		6.50		- 10,39 7	6,778		0.080 44	7.96		-2,216	5,728	0.080 44	9.30
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-			
P	S	00906	54,24 6	18,32 2	0.080 44	2.66	00909	19,28 1	31,38 1	0.080 44	1.64	00910	-5,116	28,67 4	0.080 44	1.87			
	I			0	0	0.080 44		-		0	0		0.080 44	-		0	0	0.080 44	-
S	S			-8,594	2,449	0.080 44		21.96		5,732	5,031		0.080 44	10.46		-2,277	5,944	0.080 44	8.96
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-			
P	S	00912	- 41,12 3	13,57 5	0.080 44	4.15	00914	81,23 4	15,26 9	0.080 44	3.05	00917	-6,413	36,99 2	0.080 44	1.45			
	I			0	0	0.080 44		-		- 134,7 27	7,632		0.080 44	8.37		0	0	0.080 44	-
S	S			60,51 2	1,350	0.080 44		35.71		76,31 3	5,483		0.080 44	8.56		-6,738	6,534	0.080 44	8.21
	I		0	0	0.080 44	-		- 123,4 05	5,170	0.080 44	12.18		0	0	0.080 44	-			
P	S	00918	24,25 7	34,66 6	0.080 44	1.48	00921	- 12,72 2	39,23 5	0.080 44	1.38	00922	- 13,34 1	39,55 9	0.080 44	1.37			
	I			0	0	0.080 44		-		0	0		0.080 44	-		0	0	0.080 44	-
S	S			23,88 4	9,449	0.080 44		5.42		-8,015	6,839		0.080 44	7.86		-7,987	6,951	0.080 44	7.73
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-			
P	S	00923	8,298	37,40 1	0.080 44	1.40	00924	5,373	34,84 3	0.080 44	1.51	00928	- 19,91 4	38,42 2	0.080 44	1.42			
	I			0	0	0.080 44		-		0	0		0.080 44	-		0	0	0.080 44	-
S	S			-3,105	7,704	0.080 44		6.92		19,89 5	10,17 2		0.080 44	5.06		-6,892	6,851	0.080 44	7.83
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-			
P	S	00930	39,62 5	33,60 0	0.080 44	1.49	00932	14,07 4	31,10 0	0.080 44	1.67	00935	41,53 9	35,57 0	0.080 44	1.40			
	I			0	0	0.080 44		-		0	0		0.080 44	-		0	0	0.080 44	-
S	S			- 19,15 1	8,608	0.080 44		6.35		53,27 1	9,889		0.080 44	4.93		8,602	7,899	0.080 44	6.63
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-			
P	S	00936	12,17 8	34,26 0	0.080 44	1.52	00939	101,7 57	25,42 9	0.080 44	1.76	00940	- 15,57 8	32,19 4	0.080 44	1.69			
	I			0	0	0.080 44		-		0	0		0.080 44	-		0	0	0.080 44	-



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
S	S		-7,460	6,739	0.080	7.97		14,44	4,426	0.080	11.73		-9,770	6,819	0.080	7.90
	I		0	0	0.080	-		2	0	0.080	-		0	0	0.080	-
			44		44			0		44					44	
P	S	00943	21,89	16,29	0.080	3.15	00944	-1,686	32,27	0.080	1.65	00947	-	1,956	0.080	28.06
	I		0	0	0.080	-		0	0	0.080	-		22,21	4	0.080	-
			44		44					44			0	0	0.080	-
S	S		6,577	3,628	0.080	14.49		-6,427	6,594	0.080	8.13		-	15,63	0.080	3.48
	I		0	0	0.080	-		0	0	0.080	-		16,87	9	0.080	-
			44		44			0		44			0	0	0.080	-
P	S	00948	44,18	295	0.080	NS	00951	-	1,798	0.080	30.60	00953	-	3,259	0.080	17.11
	I		2		44			23,92		44			33,37	3	0.080	-
			49,97	491	0.080	99.93		-	429	0.080	NS		0	0	0.080	-
			7		44			32,39		44					44	
S	S		-	5,954	0.080	9.48		-	4,353	0.080	12.68		3,278	13,19	0.080	4.00
	I		41,84		44			26,18		44				3	0.080	-
			7		44			9		44			0	0	0.080	-
			21,63	3,581	0.080	14.34		-	1,688	0.080	31.97				44	
			3		44			10,74		44					44	
P	S	00955	-	3,234	0.080	17.65	00957	-	3,848	0.080	14.98	00958	-	1,922	0.080	29.10
	I		49,64		44			56,46		44			35,23	3	0.080	-
			0	0	0.080	-		7	0	0.080	-		0	0	0.080	-
			0		44			0		44					44	
S	S		-4,549	9,200	0.080	5.81		-	17,80	0.080	3.18		3,539	18,98	0.080	2.78
	I		0	0	0.080	-		43,99	5	44				2	0.080	-
					44			8		44			0	0	0.080	-
					44			0	0	0.080	-				44	
P	S	00961	-	4,524	0.080	12.51	01043	-	3,055	0.080	19.21	01044	-	3,787	0.080	15.07
	I		43,44		44			69,69		44			49,67	9	0.080	-
			0	0	0.080	-		5	0	0.080	-		0	0	0.080	-
			0		44			0		44					44	
S	S		-2,846	13,54	0.080	3.94		-7,035	11,59	0.080	4.63		-	20,40	0.080	2.74
	I		0	0	0.080	-			3	44			34,49	0	0.080	-
					44			0		44			4	0	0.080	-
					44				0	0.080	-		0	0	0.080	-
P	S	01047	-	3,139	0.080	17.72	01048	-	3,329	0.080	17.23	01051	-	2,695	0.080	21.20
	I		31,47		44			53,02		44			50,28	3	0.080	-
			9	0	0.080	-		1	0	0.080	-		0	0	0.080	-
			0		44			0		44					44	
S	S		2,325	18,02	0.080	2.94		-4,698	11,92	0.080	4.48		-	13,29	0.080	4.06
	I			3	44				5	44			11,22	0	0.080	-
			0	0	0.080	-		0		44			6	0	0.080	-
					44				0	0.080	-		0	0	0.080	-
P	S	01052	48,93	145	0.080	NS	01055	-	1,395	0.080	39.84	01056	-	2,490	0.080	22.07
	I		2		44			30,82		44			23,06	6	0.080	-
			75,02	341	0.080	NS		4	454	0.080	NS		0	0	0.080	-
			0		44			-		44					44	
S	S		-	4,937	0.080	11.24		25,83		44					44	
	I		29,93		44			1	6,989	0.080	7.85		12,22	15,10	0.080	3.45
			0		44			22,00		44			8	9	0.080	-
			69,18	4,514	0.080	10.53		6	384	0.080	NS		0	0	0.080	-
			2		44			-		44					44	
					44			27,97		44					44	
P	S	01437	17,71	142	0.080	NS	01438	-	368	0.080	NS	01439	135,2	2,697	0.080	15.63
	I		7		44			27,01		44			91		44	
			17,71	284	0.080	NS		4	264	0.080	NS		-	524	0.080	NS
			7		44			-		44			123,5		44	
S	S		10,91	864	0.080	60.43		20,75		44			41		44	
	I		4		44			6	167	0.080	NS		59,12	168	0.080	NS
			15,55	533	0.080	97.26		2	726	0.080	71.51		1	532	0.080	-
			8		44			4		44			46,06		44	
P	S	01440	114,4	1,865	0.080	23.51	01441	34,08	1,929	0.080	26.10	01442	0	0	0.080	-
	I		21		44			3		44					44	
			-	681	0.080	92.10		-	457	0.080	NS		-	1,590	0.080	36.21



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
			120,388		44			63,748		44			55,896		44	
S	S		44,073	153	0.08044	NS		16,952	570	0.08044	90.75		-28,788	4,489	0.08044	12.34
	I		33,856	153	0.08044	NS		-63,813	698	0.08044	83.40		-63,704	669	0.08044	87.00
P	S	01443	0	0	0.08044	-	01444	0	0	0.08044	-	01445	-9,961	1,203	0.08044	44.80
	I		1,745	592	0.08044	89.45		-4,136	417	0.08044	NS		-20,007	352	0.08044	NS
S	S		3,502	7,354	0.08044	7.18		7,568	586	0.08044	89.56		0	0	0.08044	-
	I		0	0	0.08044	-		4,060	452	0.08044	NS		-39,277	1,842	0.08044	30.54
P	S	01446	0	0	0.08044	-	01447	0	0	0.08044	-	01448	-7,614	6,514	0.08044	8.24
	I		1,304	1,219	0.08044	43.47		-3,722	1,556	0.08044	34.31		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-16,979	1,751	0.08044	31.10		14,146	1,371	0.08044	37.90		3,513	512	0.08044	NS
P	S	01449	6,310	8,801	0.08044	5.97	01450	-4,592	220	0.08044	NS	01451	0	0	0.08044	-
	I		0	0	0.08044	-		-461	1,155	0.08044	46.00		-280	1,507	0.08044	35.25
S	S		-4,419	1,019	0.08044	52.45		0	0	0.08044	-		0	0	0.08044	-
	I		-33,530	274	0.08044	NS		-22,225	3,465	0.08044	15.84		15,732	4,351	0.08044	11.91
P	S	01452	-1,252	2,938	0.08044	18.11	01453	-9,818	5,473	0.08044	9.85	01454	0	0	0.08044	-
	I		0	0	0.08044	-		0	0	0.08044	-		356	1,219	0.08044	43.53
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		7,796	1,044	0.08044	50.25		-21,722	2,103	0.08044	26.08		-13,872	4,468	0.08044	12.13
P	S	01455	1,447	238	0.08044	NS	01456	158	14,188	0.08044	3.74	01457	-7,931	17,408	0.08044	3.09
	I		1,447	315	0.08044	NS		0	0	0.08044	-		0	0	0.08044	-
S	S		0	0	0.08044	-		-10,879	1,101	0.08044	49.02		12,585	1,629	0.08044	31.97
	I		7,455	3,210	0.08044	16.35		0	0	0.08044	-		0	0	0.08044	-
P	S	01458	377	1,330	0.08044	39.90	01459	0	0	0.08044	-	01460	720	6,487	0.08044	8.18
	I		0	0	0.08044	-		-26	841	0.08044	63.13		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		7,084	166	0.08044	NS
	I		24,417	1,314	0.08044	38.91		14,525	3,249	0.08044	15.98		7,084	193	0.08044	NS
P	S	01461	7,592	28,004	0.08044	1.87	01462	1,321	7,156	0.08044	7.40	01463	0	0	0.08044	-
	I		0	0	0.08044	-		0	0	0.08044	-		2	581	0.08044	91.38
S	S		-17,862	5,475	0.08044	9.96		34,269	445	0.08044	NS		69,685	101	0.08044	NS
	I		0	0	0.08044	-		-15,961	435	0.08044	NS		68,045	1,360	0.08044	35.00
P	S	01464	329	1,770	0.08044	29.98	01465	1,054	17,846	0.08044	2.97	01466	1,981	18,681	0.08044	2.83
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		0	0	0.08044	-		-7,504	2,377	0.08044	22.59		22,857	2,589	0.08044	19.80
	I		17,383	805	0.08044	64.22		0	0	0.08044	-		0	0	0.08044	-
P	S	01467	-821	2,574	0.080	20.65	01468	0	0	0.080	-	01469	635	8,859	0.080	5.99



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	I		0	0	0.080 44	-		-5	356	0.080 44	NS		0	0	0.080 44	-
S	S		79,48 2	473	0.080 44	98.69		23,67 5	51	0.080 44	NS		8,102	743	0.080 44	70.58
	I		-8,243	915	0.080 44	58.75		23,67 5	808	0.080 44	63.35		0	0	0.080 44	-
P	S	01470	5,088	32,18 8	0.080 44	1.64	01471	-6,410	9,777	0.080 44	5.48	01472	-2,097	86	0.080 44	NS
	I		0	0	0.080 44	-		0	0	0.080 44	-		-442	213	0.080 44	NS
S	S		- 18,16 0	6,614	0.080 44	8.25		62,77 7	837	0.080 44	57.38		121,0 92	415	0.080 44	NS
	I		0	0	0.080 44	-		0	0	0.080 44	-		122,7 22	216	0.080 44	NS
P	S	01473	199	2,780	0.080 44	19.09	01474	93	19,96 7	0.080 44	2.66	01475	- 11,26 2	21,32 7	0.080 44	2.53
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		17,84 4	445	0.080 44	NS		- 10,62 6	3,304	0.080 44	16.33		34,91 3	2,859	0.080 44	17.59
	I		17,84 4	25	0.080 44	NS		0	0	0.080 44	-		0	0	0.080 44	-
P	S	01476	-1,200	3,292	0.080 44	16.16	01477	374	120	0.080 44	NS	01478	344	9,941	0.080 44	5.34
	I		0	0	0.080 44	-		-75	91	0.080 44	NS		0	0	0.080 44	-
S	S		113,9 05	721	0.080 44	60.88		24,52 8	535	0.080 44	95.55		8,547	1,192	0.080 44	43.96
	I		-1,473	155	0.080 44	NS		24,52 8	206	0.080 44	NS		0	0	0.080 44	-
P	S	01479	3,372	33,56 3	0.080 44	1.57	01480	-4,126	10,67 5	0.080 44	5.00	01481	-655	167	0.080 44	NS
	I		0	0	0.080 44	-		0	0	0.080 44	-		-127	89	0.080 44	NS
S	S		- 17,45 3	6,949	0.080 44	7.84		81,35 0	1,164	0.080 44	39.97		150,4 76	739	0.080 44	55.38
	I		0	0	0.080 44	-		0	0	0.080 44	-		5,962	552	0.080 44	95.31
P	S	01482	155	3,194	0.080 44	16.62	01483	-204	20,68 5	0.080 44	2.57	01484	-42	21,36 5	0.080 44	2.49
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		18,24 4	840	0.080 44	61.46		-9,912	3,537	0.080 44	15.24		42,71 0	3,335	0.080 44	14.89
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	01485	-1,926	3,658	0.080 44	14.56	01486	366	207	0.080 44	NS	01487	303	10,22 2	0.080 44	5.19
	I		0	0	0.080 44	-		-35	13	0.080 44	NS		0	0	0.080 44	-
S	S		133,2 49	1,080	0.080 44	39.19		24,96 4	769	0.080 44	66.43		9,290	1,283	0.080 44	40.80
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	01488	2,633	33,69 6	0.080 44	1.57	01489	-9,146	11,20 4	0.080 44	4.80	01490	-2,637	301	0.080 44	NS
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 16,48 0	6,795	0.080 44	8.01		85,08 4	1,423	0.080 44	32.48		171,0 70	692	0.080 44	56.73
	I		0	0	0.080 44	-		0	0	0.080 44	-		10,71 1	533	0.080 44	97.99
P	S	01491	143	3,253	0.080 44	16.32	01492	-109	20,70 3	0.080 44	2.56	01493	2,248	20,69 0	0.080 44	2.56
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		19,28 9	911	0.080 44	56.58		-9,225	3,593	0.080 44	14.98		46,31 8	3,774	0.080 44	13.08
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	01494	-769	3,969	0.080 44	13.39	01495	448	185	0.080 44	NS	01496	385	10,07 9	0.080 44	5.26
	I		0	0	0.080 44	-		-41	27	0.080 44	NS		0	0	0.080 44	-
S	S		139,0	1,264	0.080	33.11		26,29	795	0.080	64.12		10,37	1,287	0.080	40.60



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	I		44 989	32	0.080 44	NS		1 0	0	0.080 44	-		8 0	0	0.080 44	-
P	S	01497	4,233	33,29 2	0.080 44	1.58	01498	249	10,50 5	0.080 44	5.05	01499	-2,708	349	0.080 44	NS
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 16,08 2	6,566	0.080 44	8.28		82,98 3	1,941	0.080 44	23.90		163,7 35	842	0.080 44	47.33
	I		0	0	0.080 44	-		0	0	0.080 44	-		10,84 2	647	0.080 44	80.71
P	S	01500	184	3,080	0.080 44	17.23	01501	840	20,37 7	0.080 44	2.60	01502	3,183	21,64 1	0.080 44	2.44
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		19,94 4	881	0.080 44	58.44		-8,881	3,534	0.080 44	15.23		38,79 2	3,790	0.080 44	13.18
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	01503	-2,063	3,836	0.080 44	13.88	01504	871	111	0.080 44	NS	01505	773	9,547	0.080 44	5.55
	I		0	0	0.080 44	-		21	167	0.080 44	NS		0	0	0.080 44	-
S	S		127,2 21	1,125	0.080 44	38.05		28,25 9	720	0.080 44	70.58		10,49 1	1,252	0.080 44	41.73
	I		0	0	0.080 44	-		28,25 9	77	0.080 44	NS		0	0	0.080 44	-
P	S	01506	3,861	33,44 8	0.080 44	1.58	01507	-9,967	11,39 1	0.080 44	4.73	01508	-2,064	277	0.080 44	NS
	I		0	0	0.080 44	-		0	0	0.080 44	-		-154	18	0.080 44	NS
S	S		- 16,69 3	6,488	0.080 44	8.39		70,77 1	1,334	0.080 44	35.52		141,2 30	656	0.080 44	63.53
	I		0	0	0.080 44	-		0	0	0.080 44	-		4,728	713	0.080 44	73.93
P	S	01509	462	2,661	0.080 44	19.94	01510	2,128	20,05 6	0.080 44	2.64	01511	-7,338	22,48 4	0.080 44	2.39
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		23,28 7	546	0.080 44	93.81		- 10,08 8	3,361	0.080 44	16.04		32,74 0	3,146	0.080 44	16.04
	I		- 15,96 0	342	0.080 44	NS		0	0	0.080 44	-		0	0	0.080 44	-
P	S	01512	-1,567	3,553	0.080 44	14.98	01513	0	0	0.080 44	-	01514	2,053	8,528	0.080 44	6.21
	I		0	0	0.080 44	-		13	254	0.080 44	NS		0	0	0.080 44	-
S	S		98,01 1	765	0.080 44	59.06		33,30 2	355	0.080 44	NS		12,41 3	975	0.080 44	53.43
	I		-3,788	210	0.080 44	NS		33,30 2	549	0.080 44	91.82		0	0	0.080 44	-
P	S	01515	7,962	32,26 0	0.080 44	1.63	01516	-6,933	10,73 1	0.080 44	5.00	01517	-1,243	171	0.080 44	NS
	I		0	0	0.080 44	-		0	0	0.080 44	-		-198	299	0.080 44	NS
S	S		- 18,99 4	6,114	0.080 44	8.93		54,21 2	419	0.080 44	NS		98,96 5	294	0.080 44	NS
	I		0	0	0.080 44	-		- 14,27 6	167	0.080 44	NS		99,35 6	549	0.080 44	82.09
P	S	01518	963	1,827	0.080 44	29.02	01519	4,327	18,13 4	0.080 44	2.91	01520	1,122	19,50 5	0.080 44	2.72
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		28,26 9	248	0.080 44	NS		-8,016	2,439	0.080 44	22.03		17,54 5	2,993	0.080 44	17.27
	I		28,26 9	568	0.080 44	89.46		0	0	0.080 44	-		0	0	0.080 44	-
P	S	01521	-1,992	2,707	0.080 44	19.67	01522	0	0	0.080 44	-	01523	3,255	6,651	0.080 44	7.94
	I		0	0	0.080 44	-		-152	581	0.080 44	91.40		0	0	0.080 44	-
S	S		60,13 6	352	0.080 44	NS		0	0	0.080 44	-		13,03 0	410	0.080 44	NS
	I		57,35 3	234	0.080 44	NS		33,11 3	2,340	0.080 44	21.55		13,03 0	44	0.080 44	NS



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
P	S	01524	10,78	28,94	0.080	1.80	01525	3,402	7,415	0.080	7.12	01526	0	0	0.080	-
	I		10	80	0.080	-		0	0	0.080	-		-202	808	0.080	65.73
S	S		-23,77	5,381	0.080	10.22		17,960	232	0.080	NS		0	0	0.080	-
	I		90	0	0.080	-		-13,475	800	0.080	67.72		48,701	754	0.080	65.21
P	S	01527	821	480	0.080	NS	01528	2,507	13,990	0.080	3.78	01529	13,629	14,550	0.080	3.57
	I		1,628	35	0.080	NS		0	0	0.080	-		0	0	0.080	-
S	S		0	0	0.080	-		-12,420	1,302	0.080	41.55		-4,531	2,515	0.080	21.26
	I		36,980	1,409	0.080	35.57		0	0	0.080	-		0	0	0.080	-
P	S	01530	-3,677	1,096	0.080	48.71	01531	0	0	0.080	-	01532	896	3,733	0.080	14.20
	I		1,414	62	0.080	NS		-42	1,167	0.080	45.50		0	0	0.080	-
S	S		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-
	I		1,233	1,736	0.080	30.53		51,809	4,525	0.080	10.81		14,719	963	0.080	53.90
P	S	01533	1,356	22,721	0.080	2.33	01534	-12,649	4,930	0.080	10.98	01535	0	0	0.080	-
	I		0	0	0.080	-		0	0	0.080	-		-42	1,601	0.080	33.16
S	S		-32,354	4,017	0.080	13.86		-5,337	14	0.080	NS		0	0	0.080	-
	I		0	0	0.080	-		-31,128	1,517	0.080	36.65		-14,684	4,081	0.080	13.30
P	S	01536	0	0	0.080	-	01537	-8,009	8,109	0.080	6.63	01538	5,758	9,492	0.080	5.54
	I		-1,741	1,102	0.080	48.31		0	0	0.080	-		0	0	0.080	-
S	S		0	0	0.080	-		-22,712	243	0.080	NS		13,700	466	0.080	NS
	I		36,468	3,659	0.080	13.71		1,912	191	0.080	NS		-45,203	253	0.080	NS
P	S	01539	-17,259	30	0.080	NS	01540	0	0	0.080	-	01541	-11,969	226	0.080	NS
	I		-12,988	1,554	0.080	34.84		652	1,123	0.080	47.23		-15,277	212	0.080	NS
S	S		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-
	I		-29,073	1,832	0.080	30.26		50,963	1,956	0.080	25.04		16,052	1,239	0.080	41.81
P	S	01542	-32,122	11,088	0.080	5.02	01543	2,378	341	0.080	NS	01544	0	0	0.080	-
	I		0	0	0.080	-		-86,388	1,175	0.080	51.08		-54,108	1,679	0.080	34.21
S	S		-31,796	1,667	0.080	33.38		-1,850	194	0.080	NS		-28,454	6,950	0.080	7.97
	I		0	0	0.080	-		-4,946	335	0.080	NS		-103,394	396	0.080	NS
P	S	01545	0	0	0.080	-	01546	-19,970	710	0.080	77.04	02511	0	0	0.080	-
	I		-29,542	1,318	0.080	42.08		0	0	0.080	-		-75,939	1,669	0.080	35.46
S	S		8,848	4,897	0.080	10.70		-10,416	468	0.080	NS		-50,374	14,853	0.080	3.85
	I		0	0	0.080	-		1,462	438	0.080	NS		0	0	0.080	-



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
					44					44					44	
P	S	02512	0	0	0.080	-	02513	0	0	0.080	-	02514	0	0	0.080	-
	I		-	1,848	0.080	32.50		-	2,353	0.080	24.71		-6,876	969	0.080	55.36
			86,917		44			62,888		44					44	
S	S		-	14,938	0.080	3.82		-9,198	14,268	0.080	3.77		-2,702	16,382	0.080	3.25
	I		48,796	0	0.080	-		0	0	0.080	-		0	0	0.080	-
			0		44					44					44	
Piano Terra SolettaP2-P3-P6-P5																
P	S	00005	-	833	0.080	66.19	00006	-	2,470	0.080	22.12	00007	-	3,530	0.080	15.33
	I		25,389	0	0.080	-		19,218	0	0.080	-		12,550	0	0.080	-
			0		44			0		44			0		44	
S	S		-1,857	3,597	0.080	14.80		-	14,005	0.080	3.86		-	19,666	0.080	2.78
	I		-	903	0.080	61.61		12,706	0	0.080	-		20,117	0	0.080	-
			31,570		44			0		44			0		44	
P	S	00008	-	4,082	0.080	13.34	00009	-	4,180	0.080	13.10	00010	-	2,946	0.080	19.91
	I		17,035	0	0.080	-		20,884	0	0.080	-		69,210	0	0.080	-
			0		44			0		44			0		44	
S	S		-4,409	19,407	0.080	2.75		-8,068	15,951	0.080	3.37		-	10,373	0.080	5.31
	I		0	0	0.080	-		0	0	0.080	-		24,874	0	0.080	-
					44					44			0		44	
P	S	00011	0	0	0.080	-	00012	-	3,226	0.080	16.91	00013	14,843	11,514	0.080	4.51
	I		-	921	0.080	60.43		18,019	0	0.080	-		0	0	0.080	-
			31,831		44			0		44					44	
S	S		-	21	0.080	NS		-	398	0.080	NS		-	3,375	0.080	16.62
	I		29,935	2,913	0.080	19.05		26,820	409	0.080	NS		37,244	0	0.080	-
			-		44			-		44			0		44	
P	S	00014	-	20,674	0.080	2.64	00015	-	25,406	0.080	2.15	00016	-	28,147	0.080	1.94
	I		19,086	0	0.080	-		19,389	0	0.080	-		17,305	0	0.080	-
			0		44			0		44			0		44	
S	S		-	3,583	0.080	15.30		-	7,615	0.080	7.28		2,195	6,395	0.080	8.27
	I		21,604	0	0.080	-		29,472	0	0.080	-		0	0	0.080	-
			0		44			0		44					44	
P	S	00017	-	32,301	0.080	1.69	00018	-	32,447	0.080	1.68	00019	-	34,274	0.080	1.58
	I		18,353	0	0.080	-		17,126	0	0.080	-		15,250	0	0.080	-
			0		44			0		44			0		44	
S	S		-	6,116	0.080	8.86		-7,391	5,910	0.080	9.08		-	6,327	0.080	8.55
	I		13,558	0	0.080	-		0	0	0.080	-		12,821	0	0.080	-
			0		44					44			0		44	
P	S	00020	-	32,033	0.080	1.71	00021	-	32,090	0.080	1.69	00022	-	32,162	0.080	1.70
	I		22,013	0	0.080	-		14,892	0	0.080	-		17,897	0	0.080	-
			0		44			0		44			0		44	
S	S		-	6,856	0.080	7.99		-	5,716	0.080	9.51		-	7,727	0.080	7.09
	I		20,627	0	0.080	-		15,875	0	0.080	-		21,082	0	0.080	-
			0		44			0		44			0		44	
P	S	00023	-	32,160	0.080	1.69	00024	-	34,767	0.080	1.56	00025	-	33,986	0.080	1.60
	I		16,664	0	0.080	-		15,604	0	0.080	-		15,018	0	0.080	-
			0		44			0		44			0		44	
S	S		-	6,954	0.080	7.81		-	6,128	0.080	8.90		-	5,996	0.080	9.10



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
			15,49		44			17,99		44			18,21		44	
	I		6 0	0	0.080 44	-		7 0	0	0.080 44	-		7 0	0	0.080 44	-
P	S	00026	- 15,34	34,81 9	0.080 44	1.56	00027	- 15,73	32,16 0	0.080 44	1.69	00028	- 16,70	32,12 4	0.080 44	1.69
	I		0 0	0	0.080 44	-		9 0	0	0.080 44	-		4 0	0	0.080 44	-
S	S		- 17,63	6,034	0.080 44	9.03		- 17,37	6,908	0.080 44	7.89		- 19,70	7,660	0.080 44	7.14
	I		2 0	0	0.080 44	-		6 0	0	0.080 44	-		7 0	0	0.080 44	-
P	S	00029	- 13,50	32,06 3	0.080 44	1.69	00030	- 20,84	32,06 0	0.080 44	1.71	00031	- 17,15	34,34 2	0.080 44	1.59
	I		7 0	0	0.080 44	-		1 0	0	0.080 44	-		0 0	0	0.080 44	-
S	S		- 18,08	5,764	0.080 44	9.46		- 20,21	6,876	0.080 44	7.96		- 13,30	6,127	0.080 44	8.84
	I		1 0	0	0.080 44	-		8 0	0	0.080 44	-		3 0	0	0.080 44	-
P	S	00032	- 20,71	33,02 9	0.080 44	1.66	00033	- 23,58	33,36 8	0.080 44	1.65	00034	- 25,29	30,73 0	0.080 44	1.79
	I		7 0	0	0.080 44	-		0 0	0	0.080 44	-		7 0	0	0.080 44	-
S	S		- 13,38	5,997	0.080 44	9.03		- 16,31	6,213	0.080 44	8.76		-1,276	7,172	0.080 44	7.42
	I		6 0	0	0.080 44	-		8 0	0	0.080 44	-		0	0	0.080 44	-
P	S	00035	- 25,54	30,55 6	0.080 44	1.80	00036	- 23,87	30,72 6	0.080 44	1.79	00037	4,675	32,13 8	0.080 44	1.64
	I		7 0	0	0.080 44	-		2 0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 14,51	8,509	0.080 44	6.38		- 13,35	6,117	0.080 44	8.86		-5,667	6,435	0.080 44	8.32
	I		5 0	0	0.080 44	-		8 0	0	0.080 44	-		0	0	0.080 44	-
P	S	00038	86,66 9	23,13 4	0.080 44	1.99	00039	-5,895	272	0.080 44	NS	00040	31,51 5	133	0.080 44	NS
	I		0	0	0.080 44	-		-5,738	27	0.080 44	NS		31,51 5	68	0.080 44	NS
S	S		8,555	3,938	0.080 44	13.31		- 60,37	220	0.080 44	NS		-8,368	301	0.080 44	NS
	I		0	0	0.080 44	-		3 - 24,18 9	191	0.080 44	NS		0	0	0.080 44	-
P	S	00041	25,71 3	109	0.080 44	NS	00042	18,30 2	267	0.080 44	NS	00043	1,583	1,050	0.080 44	50.44
	I		0	0	0.080 44	-		0	0	0.080 44	-		-7,763	95	0.080 44	NS
S	S		-7,372	429	0.080 44	NS		-5,964	304	0.080 44	NS		-9,608	687	0.080 44	78.41
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00044	- 25,60	115	0.080 44	NS	00045	- 32,95	704	0.080 44	79.18	00046	0	0	0.080 44	-
	I		3 - 12,51 8	422	0.080 44	NS		4 - 45,95 0	149	0.080 44	NS		- 68,01 2	1,563	0.080 44	37.46
S	S		-3,860	209	0.080 44	NS		- 15,56	790	0.080 44	68.79		- 13,51 8	108	0.080 44	NS
	I		- 16,74 8	75	0.080 44	NS		3 0	0	0.080 44	-		-7,765	484	0.080 44	NS
P	S	00052	- 41,09	881	0.080 44	64.01	00053	- 49,49	4,155	0.080 44	13.73	00055	- 69,58	5,998	0.080 44	9.78
	I		6 - 26,78 7	5,662	0.080 44	9.76		5 0	0	0.080 44	-		6 0	0	0.080 44	-
S	S		-989	426	0.080	NS		-	6,525	0.080	8.99		-	8,740	0.080	7.00



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	I		- 65,97 9	12,19 9	0.080 44	4.79		69,57 2 0	0	0.080 44	-		100,9 16 0	0	0.080 44	-
P	S	00137	185	1,068	0.080 44	49.70	00380	12,84 0	2,130	0.080 44	24.44	00381	- 35,69 8 0	9,472	0.080 44	5.91
	I		- 24,31 0	4,238	0.080 44	12.99		0	0	0.080 44	-		0	0	0.080 44	-
S	S		27,70 1	1,584	0.080 44	32.11		32,93 0	296	0.080 44	NS		- 38,52 8 0	1,109	0.080 44	50.67
	I		32,27 6	1,727	0.080 44	29.24		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00382	- 93,20 6 0	26,56 2	0.080 44	2.28	00383	-8,929	30,83 2	0.080 44	1.75	00384	-7,839	31,98 1	0.080 44	1.68
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 58,13 0 0	6,169	0.080 44	9.36		- 48,15 4 0	6,664	0.080 44	8.55		- 34,07 1 0	8,208	0.080 44	6.80
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00385	815	35,91 4	0.080 44	1.48	00386	10,25 0	33,05 7	0.080 44	1.58	00387	2,049	33,71 3	0.080 44	1.57
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 35,58 7 0	7,252	0.080 44	7.72		- 30,13 0 0	7,613	0.080 44	7.29		- 26,58 1 0	8,986	0.080 44	6.15
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00388	3,697	37,46 6	0.080 44	1.41	00389	6,711	34,63 6	0.080 44	1.52	00390	1,607	34,21 2	0.080 44	1.55
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 27,57 6 0	7,584	0.080 44	7.29		- 23,39 7 0	7,658	0.080 44	7.18		- 25,24 1 0	9,365	0.080 44	5.89
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00391	-914	34,48 9	0.080 44	1.54	00392	-498	35,61 5	0.080 44	1.49	00393	1,225	38,57 8	0.080 44	1.37
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 26,58 2 0	9,495	0.080 44	5.82		- 20,37 1 0	7,717	0.080 44	7.09		- 24,64 4 0	7,827	0.080 44	7.04
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00394	-279	35,52 4	0.080 44	1.50	00395	882	35,91 9	0.080 44	1.48	00396	942	39,20 6	0.080 44	1.35
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 23,35 7 0	9,602	0.080 44	5.72		- 20,55 7 0	8,037	0.080 44	6.81		- 24,45 3 0	7,982	0.080 44	6.90
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00397	108	35,60 4	0.080 44	1.49	00398	1,514	35,85 6	0.080 44	1.48	00399	1,665	39,71 2	0.080 44	1.33
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 21,95 9 0	9,393	0.080 44	5.84		- 20,99 3 0	8,366	0.080 44	6.55		- 24,61 5 0	7,946	0.080 44	6.93
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00400	588	35,50 2	0.080 44	1.49	00401	1,975	35,53 9	0.080 44	1.49	00402	1,860	39,55 9	0.080 44	1.34
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 21,27 1 0	9,104	0.080 44	6.02		- 21,94 8 0	8,645	0.080 44	6.35		- 25,52 2 0	7,915	0.080 44	6.97
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00403	822	35.27	0.080	1.50	00404	1.846	34.91	0.080	1.52	00405	1.870	38.92	0.080	1.36



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
	I		0	3 0	44 0.080	-		0	9 0	44 0.080	-		0	8 0	44 0.080	-
S	S		- 22,08 4	8,749	0.080 44	6.27		- 22,71 3	8,843	0.080 44	6.21		- 26,06 0	7,706	0.080 44	7.16
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00406	-37	34,37 3	0.080 44	1.54	00407	446	33,22 0	0.080 44	1.60	00408	-539	35,91 6	0.080 44	1.48
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 22,78 7	8,127	0.080 44	6.76		- 24,51 5	8,825	0.080 44	6.24		- 26,44 2	7,151	0.080 44	7.72
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00409	-4,553	30,61 2	0.080 44	1.75	00410	-4,432	27,74 8	0.080 44	1.93	00411	-3,609	26,74 4	0.080 44	2.00
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 23,71 2	6,782	0.080 44	8.11		- 22,06 6	7,713	0.080 44	7.11		- 20,71 6	5,070	0.080 44	10.80
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00412	- 12,19 0	19,50 2	0.080 44	2.77	00413	- 13,46 7	11,85 7	0.080 44	4.57	00414	- 16,55 3	5,704	0.080 44	9.54
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 13,93 5	3,688	0.080 44	14.70		- 11,54 8	3,597	0.080 44	15.02		-8,048	1,653	0.080 44	32.51
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	00416	- 113,0 11	817	0.080 44	76.05	00417	- 22,56 3	2,023	0.080 44	27.14	00418	0	0	0.080 44	-
	I		- 113,0 11	722	0.080 44	86.06		- 22,56 3	279	0.080 44	NS		- 30,35 5	1,414	0.080 44	39.27
S	S		- 45,29 3	2,921	0.080 44	19.42		0	0	0.080 44	-		0	0	0.080 44	-
	I		- 35,78 7	376	0.080 44	NS		- 69,52 8	2,080	0.080 44	28.21		-496	2,521	0.080 44	21.08
P	S	00729	0	0	0.080 44	-	00730	15,88 1	1,780	0.080 44	29.11	00731	8,156	716	0.080 44	73.24
	I		29,56 8	3,820	0.080 44	13.28		0	0	0.080 44	-		1,438	393	0.080 44	NS
S	S		- 89,81 8	3,364	0.080 44	17.92		9,648	168	0.080 44	NS		78,56 3	675	0.080 44	69.26
	I		0	0	0.080 44	-		- 39,64 0	99	0.080 44	NS		79,69 5	32	0.080 44	NS
P	S	00732	63,96 8	68	0.080 44	NS	00733	44,84 2	65	0.080 44	NS	00734	41,19 3	78	0.080 44	NS
	I		63,96 8	419	0.080 44	NS		44,84 2	60	0.080 44	NS		41,19 3	94	0.080 44	NS
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
	I		19,47 2	306	0.080 44	NS		9,371	93	0.080 44	NS		8,507	101	0.080 44	NS
P	S	00735	37,02 3	85	0.080 44	NS	00736	32,53 8	59	0.080 44	NS	00737	25,85 0	102	0.080 44	NS
	I		37,02 3	26	0.080 44	NS		12,61 3	216	0.080 44	NS		11,70 4	199	0.080 44	NS
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
	I		9,370	159	0.080 44	NS		13,67 3	292	0.080 44	NS		14,39 4	225	0.080 44	NS
P	S	00738	15,68 7	24	0.080 44	NS	00739	5,860	43	0.080 44	NS	00740	0	0	0.080 44	-
	I		10,97 9	226	0.080 44	NS		5,070	17	0.080 44	NS		-2,359	243	0.080 44	NS
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
	I		10,08	129	0.080	NS		8,677	71	0.080	NS		15,43	308	0.080	NS



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
			6		44					44			7		44	
P	S	00741	0	0	0.080	-	00742	0	0	0.080	-	00743	0	0	0.080	-
	I		-	640	0.080	85.11		-	545	0.080	NS		-	553	0.080	NS
			17,10 1		44			19,35 9		44			47,48 3		44	
S	S	00744	0	0	0.080	-	00745	0	0	0.080	-	00746	0	0	0.080	-
	I		23,02 7	428	0.080	NS		16,39 0	222	0.080	NS		12,35 8	69	0.080	NS
			44		44			44		44			44		44	
P	S	00747	0	0	0.080	-	00748	0	0	0.080	-	00749	-5,501	83	0.080	NS
	I		-	890	0.080	66.24		-	1,352	0.080	44.72		-5,501	81	0.080	NS
			73,03 1		44			92,04 7		44			44		44	
S	S	00750	0	0	0.080	-	00751	0	0	0.080	-	00752	-	211	0.080	NS
	I		14,42 2	255	0.080	NS		-7,693	356	0.080	NS		59,38 7	158	0.080	NS
			44		44			44		44			-		44	
P	S	00753	14,29 6	128	0.080	NS	00754	0	0	0.080	-	00755	104,9 48	16,91 4	0.080	2.64
	I		13,35 6	116	0.080	NS		39,56 2	2,024	0.080	24.66		0	0	0.080	-
			44		44			44		44			44		44	
S	S	00756	0	0	0.080	-	00757	-2,250	177	0.080	NS	00758	0	0	0.080	-
	I		-	412	0.080	NS		-2,250	347	0.080	NS		54,96 0	51	0.080	NS
			28,13 7		44			44		44			44		44	
P	S	00759	129,4 96	3,255	0.080	13.10	00760	0	0	0.080	-	00761	0	0	0.080	-
	I		0	0	0.080	-		68,50 8	383	0.080	NS		34,57 4	7,216	0.080	6.97
			44		44			44		44			44		44	
S	S	00762	0	0	0.080	-	00763	6,562	978	0.080	53.75	00764	0	0	0.080	-
	I		22,72 0	961	0.080	53.34		0	0	0.080	-		294	2,075	0.080	25.58
			44		44			44		44			44		44	
P	S	00765	0	0	0.080	-	00766	0	0	0.080	-	00767	0	0	0.080	-
	I		34,04 9	13,29 4	0.080	3.79		9,954	16,34 3	0.080	3.20		13,98 8	18,32 7	0.080	2.84
			44		44			44		44			44		44	
S	S	00768	0	0	0.080	-	00769	0	0	0.080	-	00770	0	0	0.080	-
	I		5,341	626	0.080	84.13		3,289	2,205	0.080	23.96		5,635	810	0.080	64.99
			44		44			44		44			44		44	
P	S	00771	0	0	0.080	-	00772	0	0	0.080	-	00773	0	0	0.080	-
	I		2,577	18,05 5	0.080	2.93		573	15,90 7	0.080	3.33		-32	12,80 8	0.080	4.15
			44		44			44		44			44		44	
S	S	00774	0	0	0.080	-	00775	0	0	0.080	-	00776	0	0	0.080	-
	I		-509	781	0.080	68.03		430	2,189	0.080	24.24		1,224	418	0.080	NS
			44		44			44		44			44		44	
P	S	00777	0	0	0.080	-	00778	0	0	0.080	-	00779	-	7,181	0.080	7.83
	I		-	8,054	0.080	6.75		-	2,496	0.080	21.60		38,85 0	0	0.080	-
			15,67 9		44			10,14 6		44			0		44	
S	S	00780	0	0	0.080	-	00781	0	0	0.080	-	00782	0	0	0.080	-
	I		-3,492	1,727	0.080	30.91		-4,034	612	0.080	87.28		-	720	0.080	75.41
			44		44			44		44			14,92 4		44	
P	S	00783	-	16,99 7	0.080	3.46	00784	22,60 0	106	0.080	NS	00785	3,515	331	0.080	NS
	I		72,28 7	0	0.080	-		22,60 0	131	0.080	NS		-1,244	69	0.080	NS
			0		44			44		44			44		44	
S	S	00786	-	101	0.080	NS	00787	-5,565	138	0.080	NS	00788	-	274	0.080	NS
	I		61,94 7	434	0.080	NS		-9,604	58	0.080	NS		10,28 9	0	0.080	-
			-		44			44		44			0		44	
P	S	00789	0	0	0.080	-	00790	28,21 1	43	0.080	NS	00791	-4,709	258	0.080	NS
	I		43,27 7	835	0.080	59.41		28,21 1	310	0.080	NS		0	0	0.080	-
			44		44			44		44			44		44	
S	S	00792	11,79	93	0.080	NS	00793	-6,890	329	0.080	NS	00794	-5,746	240	0.080	NS
	I															



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	I		4 - 15,46 1	4,471	0.080 44	12.15		-2,878	41	0.080 44	NS		0	0	0.080 44	-
P	S	00973	- 26,02 4	162	0.080 44	NS	00975	- 37,86 6	127	0.080 44	NS	01030	- 14,14 5	4,005	0.080 44	13.54
	I		- 42,49 8	130	0.080 44	NS		- 59,67 5	327	0.080 44	NS		0	0	0.080 44	-
S	S		- 14,23 5	362	0.080 44	NS		- 15,10 2	515	0.080 44	NS		- 11,09 2	16,30 3	0.080 44	3.31
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	01032	- 19,20 8	1,235	0.080 44	44.24	01033	-6,883	3,257	0.080 44	16.47	01036	- 18,55 1	5,132	0.080 44	10.64
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 26,07 7	9,699	0.080 44	5.69		- 17,86 2	19,41 0	0.080 44	2.81		-4,220	18,81 8	0.080 44	2.84
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	01037	- 41,78 7	371	0.080 44	NS	01040	- 28,50 0	2,525	0.080 44	21.93	01059	- 15,98 1	33,40 8	0.080 44	1.63
	I		- 29,69 7	632	0.080 44	87.79		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 21,08 2	4,303	0.080 44	12.73		- 12,65 4	14,05 6	0.080 44	3.85		- 12,70 8	5,359	0.080 44	10.10
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	01061	- 15,15 3	32,05 0	0.080 44	1.69	01062	- 18,57 9	35,04 4	0.080 44	1.56	01064	- 15,34 1	33,58 9	0.080 44	1.62
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 10,89 0	6,842	0.080 44	7.89		- 11,99 4	5,624	0.080 44	9.61		-6,092	5,339	0.080 44	10.04
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	01067	- 15,53 7	32,07 2	0.080 44	1.69	01069	- 19,47 9	35,05 7	0.080 44	1.56	01071	- 12,11 4	32,16 6	0.080 44	1.68
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 12,57 3	6,834	0.080 44	7.92		- 10,36 2	5,669	0.080 44	9.51		-3,565	6,238	0.080 44	8.56
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	01072	- 16,89 1	33,50 1	0.080 44	1.63	01075	- 16,00 0	33,63 8	0.080 44	1.62	01077	- 27,08 1	33,26 4	0.080 44	1.66
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		- 11,57 6	5,347	0.080 44	10.10		-5,790	5,411	0.080 44	9.90		-5,438	5,763	0.080 44	9.29
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	01079	- 26,52 4	32,16 1	0.080 44	1.72	01080	74,33 2	28,02 2	0.080 44	1.68	01082	-9,275	30,68 7	0.080 44	1.75
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		-3,568	5,678	0.080 44	9.40		18,89 3	6,949	0.080 44	7.42		12,68 3	6,716	0.080 44	7.75
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	01085	- 24,47 1	32,38 6	0.080 44	1.70	01087	- 20,63 0	32,73 7	0.080 44	1.67	01089	- 10,37 4	32,15 7	0.080 44	1.68
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
S	S		-5,930	5,417	0.080	9.89		-	5,483	0.080	9.86		-6,104	6,146	0.080	8.72



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
					44			12,10		44					44	
	I		0	0	0.080	-		1 0	0	0.080	-		0	0	0.080	-
P	S	01090	- 21,20	31,01 9	0.080 44	1.77	01093	- 18,27	31,27 3	0.080 44	1.74	01095	- 20,17	30,27 2	0.080 44	1.81
	I		7 0	0	0.080 44	-		0 0	0	0.080 44	-		1 0	0	0.080 44	-
S	S		- 24,91	7,991	0.080 44	6.89		-2,003	7,030	0.080 44	7.58		- 27,13	7,998	0.080 44	6.91
	I		8 0	0	0.080 44	-		0	0	0.080 44	-		3 0	0	0.080 44	-
P	S	01097	- 18,43	30,49 6	0.080 44	1.79	01098	- 19,88	32,68 3	0.080 44	1.67	01101	- 15,32	30,93 1	0.080 44	1.76
	I		9 0	0	0.080 44	-		5 0	0	0.080 44	-		7 0	0	0.080 44	-
S	S		-1,486	5,067	0.080 44	10.50		-9,586	5,619	0.080 44	9.59		2,535	6,835	0.080 44	7.74
	I		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
P	S	01103	- 16,64	27,99 7	0.080 44	1.94	01105	- 13,00	8,367	0.080 44	6.47	01106	- 19,35	25,75 5	0.080 44	2.12
	I		3 0	0	0.080 44	-		5 0	0	0.080 44	-		5 0	0	0.080 44	-
S	S		-5,428	5,090	0.080 44	10.52		- 26,50	1,475	0.080 44	37.44		-8,888	4,406	0.080 44	12.21
	I		0	0	0.080 44	-		6 0	0	0.080 44	-		0	0	0.080 44	-
P	S	01109	- 23,39	17,68 4	0.080 44	3.11	01111	- 43,52	564	0.080 44	NS	01113	7,534	8,834	0.080 44	5.94
	I		1 0	0	0.080 44	-		- 36,88	2,401	0.080 44	23.35		0	0	0.080 44	-
S	S		-2,905	3,111	0.080 44	17.14		0	0	0.080 44	-		0	0	0.080 44	-
	I		0	0	0.080 44	-		- 101,7	3,144	0.080 44	19.48		9,777	448	0.080 44	NS
								76								
P	S	01547	- 32,61	331	0.080 44	NS	01548	- 46,90	573	0.080 44	99.23	01549	- 16,17	2,688	0.080 44	20.24
	I		5 -	156	0.080 44	NS		7 -	570	0.080 44	96.53		9 0	0	0.080 44	-
S	S		32,61 5					23,96 0					-7,566	640	0.080 44	83.91
	I		- 34,50	133	0.080 44	NS		-4,945	394	0.080 44	NS		-	343	0.080 44	NS
			4 -	361	0.080 44	NS		-2,589	873	0.080 44	61.06		25,49 4			
P	S	01550	0	0	0.080 44	-	01551	0	0	0.080 44	-	01552	0	0	0.080 44	-
	I		- 21,78	2,117	0.080 44	25.91		- 25,99	3,118	0.080 44	17.70		- 30,25	3,353	0.080 44	16.56
S	S		5 -	1,193	0.080 44	45.14		3 -	2,740	0.080 44	19.90		0 -	2,794	0.080 44	19.58
	I		- 19,08	411	0.080 44	NS		5 0	0	0.080 44	-		1 0	0	0.080 44	-
			6					0					0			
P	S	01553	0	0	0.080 44	-	01554	- 13,01	1,305	0.080 44	41.49	01555	- 11,72	1,141	0.080 44	47.36
	I		- 34,71	2,240	0.080 44	24.95		0 0	0	0.080 44	-		4 -	663	0.080 44	80.81
S	S		5 -	1,049	0.080 44	52.43		- 23,73	58	0.080 44	NS		0	0	0.080 44	-
	I		1 0	0	0.080 44	-		8 -	225	0.080 44	NS		- 23,09	1,367	0.080 44	40.20
			0					0					2			
P	S	01556	0	0	0.080 44	-	01557	0	0	0.080 44	-	01558	0	0	0.080 44	-



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
	I		[N] - 16,38 2	[N-m] 6,314	[cm²/cm] 0.080 44	8.62		[N] - 20,32 1	[N-m] 8,395	[cm²/cm] 0.080 44	6.52		[N] - 21,22 0	[N-m] 6,881	[cm²/cm] 0.080 44	7.96
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
	I		- 21,87 9	4,167	0.080 44	13.16		- 19,70 2	5,038	0.080 44	10.85		- 22,41 3	4,281	0.080 44	12.82
P	S	01559	-7,401	448	0.080 44	NS	01560	-6,030	12,34 9	0.080 44	4.34	01561	0	0	0.080 44	-
	I		- 19,18 3	567	0.080 44	96.36		0	0	0.080 44	-		- 15,87 6	5,399	0.080 44	10.07
S	S		0	0	0.080 44	-		- 19,04 7	1,503	0.080 44	36.34		0	0	0.080 44	-
	I		- 28,93 0	2,136	0.080 44	25.95		0	0	0.080 44	-		- 23,69 4	3,521	0.080 44	15.62
P	S	01562	0	0	0.080 44	-	01563	0	0	0.080 44	-	01564	0	0	0.080 44	-
	I		- 12,76 6	11,52 9	0.080 44	4.69		- 13,27 4	11,94 9	0.080 44	4.53		- 11,76 5	5,940	0.080 44	9.10
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
	I		- 22,90 8	6,409	0.080 44	8.57		- 23,16 4	6,537	0.080 44	8.41		- 25,22 2	3,940	0.080 44	13.99
P	S	01565	748	9,832	0.080 44	5.39	01566	-3,990	4,208	0.080 44	12.69	01567	0	0	0.080 44	-
	I		0	0	0.080 44	-		5,353	1,584	0.080 44	33.25		- 11,21 5	11,47 1	0.080 44	4.71
S	S		- 29,15 9	967	0.080 44	57.33		0	0	0.080 44	-		0	0	0.080 44	-
	I		0	0	0.080 44	-		- 11,72 8	946	0.080 44	57.12		- 24,12 7	4,943	0.080 44	11.13
P	S	01568	0	0	0.080 44	-	01569	0	0	0.080 44	-	01570	-743	1,846	0.080 44	28.79
	I		-7,690	15,09 2	0.080 44	3.56		-7,562	11,66 9	0.080 44	4.60		0	0	0.080 44	-
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
	I		- 23,99 8	6,581	0.080 44	8.36		- 24,09 8	5,282	0.080 44	10.42		- 20,82 6	2,241	0.080 44	24.44
P	S	01571	-287	17,97 6	0.080 44	2.95	01572	0	0	0.080 44	-	01573	0	0	0.080 44	-
	I		0	0	0.080 44	-		-4,456	6,724	0.080 44	7.95		-8,446	16,07 7	0.080 44	3.34
S	S		- 25,48 8	2,647	0.080 44	20.83		0	0	0.080 44	-		0	0	0.080 44	-
	I		- 11,31 1	67	0.080 44	NS		- 26,32 2	2,807	0.080 44	19.67		- 24,21 5	5,274	0.080 44	10.44
P	S	01574	0	0	0.080 44	-	01575	0	0	0.080 44	-	01576	- 18,38 5	16,12 8	0.080 44	3.38
	I		-4,511	15,82 4	0.080 44	3.38		-5,116	7,076	0.080 44	7.56		0	0	0.080 44	-
S	S		0	0	0.080 44	-		0	0	0.080 44	-		- 28,70 7	1,842	0.080 44	30.08
	I		- 23,74 1	5,464	0.080 44	10.07		- 22,64 3	2,945	0.080 44	18.65		0	0	0.080 44	-
P	S	01577	-867	6,258	0.080 44	8.50	01578	0	0	0.080 44	-	01579	0	0	0.080 44	-
	I		12,27 7	2,962	0.080 44	17.59		-3,372	13,38 9	0.080 44	3.99		-7,665	18,06 3	0.080 44	2.97
S	S		- 23,52 2	130	0.080 44	NS		0	0	0.080 44	-		0	0	0.080 44	-
	I		- 12,93 4	1,151	0.080 44	47.03		- 27,60 7	3,983	0.080 44	13.89		- 23,42 0	5,024	0.080 44	10.94
P	S	01580	0	0	0.080	-	01581	1.128	2.731	0.080	19.41	01582	747	20.23	0.080	2.62



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	I		-3,875	13,234	0.08044	4.04		0	0	0.08044	-		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		-24,765	3,173	0.08044	17.36
	I		-22,121	3,971	0.08044	13.82		-19,901	1,707	0.08044	32.04		-11,654	381	0.08044	NS
P	S	01583	0	0	0.08044	-	01584	0	0	0.08044	-	01585	0	0	0.08044	-
	I		12,115	6,835	0.08044	7.63		-3,720	17,576	0.08044	3.04		-2,288	16,920	0.08044	3.15
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-14,832	1,710	0.08044	31.75		-23,096	3,992	0.08044	13.77		-21,956	4,252	0.08044	12.90
P	S	01586	0	0	0.08044	-	01587	-17,513	17,884	0.08044	3.05	01588	-25	7,231	0.08044	7.34
	I		-4,408	7,335	0.08044	7.29		0	0	0.08044	-		15,475	4,343	0.08044	11.94
S	S		0	0	0.08044	-		-16,670	1,739	0.08044	31.30		-22,330	532	0.08044	NS
	I		-19,881	2,163	0.08044	25.29		0	0	0.08044	-		-13,115	1,397	0.08044	38.76
P	S	01589	0	0	0.08044	-	01590	0	0	0.08044	-	01591	0	0	0.08044	-
	I		-272	14,206	0.08044	3.74		-5,162	18,910	0.08044	2.83		-3,574	13,638	0.08044	3.91
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-27,239	3,502	0.08044	15.79		-21,798	4,145	0.08044	13.23		-20,297	3,241	0.08044	16.89
P	S	01592	2,449	3,647	0.08044	14.50	01593	676	21,003	0.08044	2.53	01594	0	0	0.08044	-
	I		0	0	0.08044	-		17,200	858	0.08044	60.27		14,324	7,912	0.08044	6.56
S	S		-25,261	72	0.08044	NS		-23,910	3,323	0.08044	16.56		0	0	0.08044	-
	I		-18,205	1,003	0.08044	54.39		-20,664	100	0.08044	NS		-14,572	1,856	0.08044	29.24
P	S	01595	0	0	0.08044	-	01596	0	0	0.08044	-	01597	0	0	0.08044	-
	I		-2,146	18,148	0.08044	2.94		-2,457	17,143	0.08044	3.11		-4,638	7,474	0.08044	7.15
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-28,288	4,133	0.08044	13.40		-20,435	3,778	0.08044	14.49		-18,698	1,885	0.08044	28.96
P	S	01598	-17,626	18,482	0.08044	2.95	01599	-247	7,638	0.08044	6.95	01600	0	0	0.08044	-
	I		0	0	0.08044	-		16,794	5,318	0.08044	9.73		731	14,624	0.08044	3.63
S	S		-16,420	1,721	0.08044	31.62		-21,290	678	0.08044	80.83		0	0	0.08044	-
	I		0	0	0.08044	-		-12,547	1,430	0.08044	37.83		-26,656	3,430	0.08044	16.10
P	S	01601	0	0	0.08044	-	01602	0	0	0.08044	-	01603	3,049	4,157	0.08044	12.71
	I		-4,249	19,201	0.08044	2.78		-4,013	13,748	0.08044	3.89		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-20,501	3,880	0.08044	14.11		-19,161	3,106	0.08044	17.59		-17,018	1,421	0.08044	38.33
P	S	01604	371	21,253	0.08044	2.50	01605	0	0	0.08044	-	01606	0	0	0.08044	-
	I		18,143	1,691	0.08044	30.53		15,341	8,533	0.08044	6.08		-1,607	18,383	0.08044	2.90



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
S	S		- 23,05 0	3,412	0.080 44	16.10		0	0	0.080 44	-		0	0	0.080 44	-
	I		- 10,42 5	499	0.080 44	NS		- 14,61 4	2,185	0.080 44	24.84		- 28,02 5	4,097	0.080 44	13.51
P	S	01607	0	0	0.080 44	-	01608	0	0	0.080 44	-	01609	- 16,13 2	18,66 3	0.080 44	2.91
	I		-3,493	17,22 6	0.080 44	3.10		-5,134	7,584	0.080 44	7.06		0	0	0.080 44	-
S	S		0	0	0.080 44	-		0	0	0.080 44	-		- 16,99 2	1,614	0.080 44	33.74
	I		- 19,46 9	3,660	0.080 44	14.93		- 18,13 4	1,815	0.080 44	30.06		0	0	0.080 44	-
P	S	01610	-478	7,768	0.080 44	6.84	01611	0	0	0.080 44	-	01612	0	0	0.080 44	-
	I		17,62 5	5,749	0.080 44	8.99		1,004	14,79 6	0.080 44	3.58		-3,995	19,29 6	0.080 44	2.77
S	S		- 20,72 1	751	0.080 44	72.92		0	0	0.080 44	-		0	0	0.080 44	-
	I		- 12,16 1	1,706	0.080 44	31.70		- 26,36 8	3,443	0.080 44	16.04		- 19,71 1	3,824	0.080 44	14.30
P	S	01613	0	0	0.080 44	-	01614	4,255	4,309	0.080 44	12.24	01615	692	21,25 4	0.080 44	2.50
	I		-4,445	13,77 9	0.080 44	3.88		0	0	0.080 44	-		0	0	0.080 44	-
S	S		0	0	0.080 44	-		0	0	0.080 44	-		- 22,81 3	3,416	0.080 44	16.08
	I		- 18,57 6	3,072	0.080 44	17.77		- 17,22 3	1,443	0.080 44	37.75		- 10,37 5	826	0.080 44	65.29
P	S	01616	0	0	0.080 44	-	01617	0	0	0.080 44	-	01618	0	0	0.080 44	-
	I		15,79 4	8,657	0.080 44	5.99		-1,577	18,42 0	0.080 44	2.89		-6,784	17,51 6	0.080 44	3.06
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
	I		- 14,56 7	2,213	0.080 44	24.52		- 27,87 5	4,101	0.080 44	13.49		- 18,90 8	3,647	0.080 44	14.98
P	S	01619	0	0	0.080 44	-	01620	- 15,68 1	18,67 3	0.080 44	2.91	01621	-386	7,714	0.080 44	6.89
	I		-5,403	7,607	0.080 44	7.04		0	0	0.080 44	-		18,51 9	5,617	0.080 44	9.19
S	S		0	0	0.080 44	-		- 17,02 8	1,617	0.080 44	33.68		- 20,53 6	788	0.080 44	69.47
	I		- 17,79 9	1,813	0.080 44	30.07		0	0	0.080 44	-		- 12,37 8	1,676	0.080 44	32.27
P	S	01622	0	0	0.080 44	-	01623	0	0	0.080 44	-	01624	0	0	0.080 44	-
	I		969	14,72 2	0.080 44	3.60		-4,368	19,25 6	0.080 44	2.78		-4,785	13,76 5	0.080 44	3.89
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
	I		- 26,40 9	3,432	0.080 44	16.09		- 19,20 1	3,828	0.080 44	14.27		- 18,12 5	3,074	0.080 44	17.75
P	S	01625	3,752	4,245	0.080 44	12.44	01626	2,121	21,05 7	0.080 44	2.51	01627	0	0	0.080 44	-
	I		0	0	0.080 44	-		21,53 5	1,341	0.080 44	38.30		16,15 9	8,296	0.080 44	6.24
S	S		0	0	0.080 44	-		- 22,83 7	3,456	0.080 44	15.89		0	0	0.080 44	-
	I		- 16,67 6	1,403	0.080 44	38.80		- 11,24 1	234	0.080 44	NS		- 15,12 1	2,126	0.080 44	25.55
P	S	01628	0	0	0.080 44	-	01629	0	0	0.080 44	-	01630	0	0	0.080 44	-
	I		-2,197	18,27 5	0.080 44	2.91		-4,381	17,20 1	0.080 44	3.11		-5,749	7,530	0.080 44	7.11
S	S		0	0	0.080	-		0	0	0.080	-		0	0	0.080	-



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	I		- 19,55 1	3,351	0.080 44	16.31		- 18,30 8	3,655	0.080 44	14.93		- 17,30 1	1,832	0.080 44	29.74
P	S	01631	- 16,76 6	18,51 8	0.080 44	2.94	01632	275	7,625	0.080 44	6.96	01633	0	0	0.080 44	-
	I		0	0	0.080 44	-		19,56 6	3,108	0.080 44	16.58		299	14,42 7	0.080 44	3.68
S	S		- 16,72 0	1,732	0.080 44	31.43		- 21,00 8	808	0.080 44	67.80		0	0	0.080 44	-
	I		0	0	0.080 44	-		- 13,71 9	1,167	0.080 44	46.44		- 26,67 9	3,312	0.080 44	16.68
P	S	01634	0	0	0.080 44	-	01635	0	0	0.080 44	-	01636	2,420	3,846	0.080 44	13.75
	I		-6,121	19,10 3	0.080 44	2.81		-5,529	13,70 4	0.080 44	3.91		0	0	0.080 44	-
S	S		0	0	0.080 44	-		0	0	0.080 44	-		- 25,21 0	118	0.080 44	NS
	I		- 18,41 2	3,833	0.080 44	14.24		- 17,24 9	3,020	0.080 44	18.04		- 17,05 7	950	0.080 44	57.33
P	S	01637	1,987	21,45 7	0.080 44	2.47	01638	0	0	0.080 44	-	01639	0	0	0.080 44	-
	I		0	0	0.080 44	-		15,70 3	7,456	0.080 44	6.95		-4,263	17,96 2	0.080 44	2.97
S	S		- 25,13 1	3,661	0.080 44	15.05		0	0	0.080 44	-		0	0	0.080 44	-
	I		- 14,55 0	167	0.080 44	NS		- 23,53 8	1,792	0.080 44	30.68		- 18,66 4	3,396	0.080 44	16.08
P	S	01640	0	0	0.080 44	-	01641	0	0	0.080 44	-	01642	- 17,68 9	18,16 3	0.080 44	3.00
	I		-5,553	17,17 0	0.080 44	3.12		-6,815	7,383	0.080 44	7.27		0	0	0.080 44	-
S	S		0	0	0.080 44	-		0	0	0.080 44	-		- 16,13 0	1,726	0.080 44	31.51
	I		- 16,81 2	3,682	0.080 44	14.79		- 15,98 6	1,842	0.080 44	29.52		0	0	0.080 44	-
P	S	01643	-110	7,158	0.080 44	7.42	01644	0	0	0.080 44	-	01645	0	0	0.080 44	-
	I		16,88 5	3,486	0.080 44	14.84		-2,175	13,94 1	0.080 44	3.82		- 10,37 8	18,84 9	0.080 44	2.86
S	S		- 22,41 4	652	0.080 44	84.20		0	0	0.080 44	-		0	0	0.080 44	-
	I		- 18,02 6	1,169	0.080 44	46.66		- 27,10 3	3,163	0.080 44	17.47		- 16,28 4	3,905	0.080 44	13.93
P	S	01646	0	0	0.080 44	-	01647	-2,143	3,405	0.080 44	15.64	01648	1,904	19,88 9	0.080 44	2.66
	I		-7,106	13,57 2	0.080 44	3.95		0	0	0.080 44	-		0	0	0.080 44	-
S	S		0	0	0.080 44	-		0	0	0.080 44	-		- 27,01 9	3,167	0.080 44	17.45
	I		- 14,75 6	3,100	0.080 44	17.51		- 15,87 2	1,402	0.080 44	38.78		0	0	0.080 44	-
P	S	01649	0	0	0.080 44	-	01650	0	0	0.080 44	-	01651	0	0	0.080 44	-
	I		12,32 5	6,174	0.080 44	8.44		-9,519	17,53 8	0.080 44	3.07		-7,758	17,07 5	0.080 44	3.15
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-
	I		- 20,29 7	1,531	0.080 44	35.74		- 16,02 2	3,505	0.080 44	15.52		- 12,89 2	3,720	0.080 44	14.55
P	S	01652	0	0	0.080 44	-	01653	- 23,23 9	17,75 9	0.080 44	3.09	01654	-2,157	6,232	0.080 44	8.55
	I		-8,460	7,142	0.080 44	7.53		0	0	0.080 44	-		9,504	1,693	0.080 44	30.91



Solette - Verifiche pressoflessione retta allo stato limite ultimo																		
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS		
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			
S	S		0	0	0.080 44	-		- 24,28 3 0	2,259	0.080 44	24.37		- 24,67 6 - 25,85 1	374	0.080 44	NS		
	I		- 12,52 1	1,794	0.080 44	30.16		0	0	0.080 44	-		- 25,85 1	701	0.080 44	78.70		
P	S	01655	0	0	0.080 44	-	01656	0	0	0.080 44	-	01657	0	0	0.080 44	-		
	I		- 11,05 6	13,34 5	0.080 44	4.05		-7,869	17,88 5	0.080 44	3.00		-8,842	13,32 3	0.080 44	4.04		
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-		
	I		- 16,48 8	2,698	0.080 44	20.17		- 10,83 4	3,916	0.080 44	13.78		-9,119	3,037	0.080 44	17.72		
P	S	01658	-5,060	2,939	0.080 44	18.20	01659	-2,512	18,51 0	0.080 44	2.88	01660	0	0	0.080 44	-		
	I		0	0	0.080 44	-		0	0	0.080 44	-		- 20,78 8	6,184	0.080 44	8.86		
S	S		0	0	0.080 44	-		- 32,62 7 0	2,802	0.080 44	19.88		0	0	0.080 44	-		
	I		- 10,54 6	1,324	0.080 44	40.74		0	0	0.080 44	-		- 17,81 8	1,420	0.080 44	38.40		
P	S	01661	0	0	0.080 44	-	01662	0	0	0.080 44	-	01663	0	0	0.080 44	-		
	I		-9,085	16,14 4	0.080 44	3.33		-7,395	16,76 8	0.080 44	3.20		-7,853	6,705	0.080 44	8.01		
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-		
	I		-8,811	3,436	0.080 44	15.66		-5,475	3,509	0.080 44	15.26		1,065	1,388	0.080 44	38.19		
P	S	01664	3,569	15,51 7	0.080 44	3.40	01665	- 25,79 8 0	5,898	0.080 44	9.35	01666	0	0	0.080 44	-		
	I		0	0	0.080 44	-		0	0	0.080 44	-		- 14,46 8	11,59 0	0.080 44	4.68		
S	S		-3,886	2,290	0.080 44	23.32		- 26,91 5 - 21,62 9	28	0.080 44	NS		0	0	0.080 44	-		
	I		0	0	0.080 44	-		- 21,62 9	338	0.080 44	NS		-5,075	2,383	0.080 44	22.45		
P	S	01667	0	0	0.080 44	-	01668	0	0	0.080 44	-	01669	19,31 9 0	4,169	0.080 44	12.36		
	I		-3,467	17,98 4	0.080 44	2.97		3,864	12,84 1	0.080 44	4.11		0	0	0.080 44	-		
S	S		0	0	0.080 44	-		0	0	0.080 44	-		0	0	0.080 44	-		
	I		-2,352	3,259	0.080 44	16.35		1,598	2,402	0.080 44	22.05		20,61 3	612	0.080 44	84.04		
P	S	02515	- 93,82 1 0	23,48 1 0	0.080 44	2.58	02516	30,91 3	81	0.080 44	NS	02517	- 105,9 54 - 103,4 79	409	0.080 44	NS		
	I		0	0	0.080 44	-		55,99 9	424	0.080 44	NS		- 90,90 9 0	102	0.080 44	NS		
S	S		0	0	0.080 44	-		58,67 7	660	0.080 44	73.27		- 90,90 9 0	1,066	0.080 44	56.64		
	I		- 115,2 07	746	0.080 44	83.52		67,70 2	1,705	0.080 44	27.94		0	0	0.080 44	-		
P	S	02518	137,2 68 0	21,66 2 0	0.080 44	1.94												
	I				0.080 44	-												
S	S		31,51 4 0	2,391 0	0.080 44	-												
	I			0.080 44	-													

#### LEGENDA Solette - Verifiche pressoflessione retta allo stato limite ultimo

**D** Direzione [P] = principale - [S] = secondaria.  
**P** Posizione [S] = superiore - [I] = inferiore.  
**N, M** Coppia N-M che dà origine alla massima armatura.  
**Af** Area delle armature per centimetro.



Solette - Verifiche pressoflessione retta allo stato limite ultimo																
D	P	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS	Nodo	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	

**CS** Coefficienti di sicurezza: [NS] = Non Significativo - Per valori di CS maggiori o uguali a 100.

SOLETTE - VERIFICHE PRESSOFLESSIONE RETTA ALLO STATO LIMITE DI DANNO

(Elevazione)

Solette - Verifiche pressoflessione retta allo stato limite di danno																
D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
Piano Terra			SolettaP1-P2-P5-P4													
P	S	00 05 1	78,391	370	0.08044	NS	00 05 2	0	0	0.08044	-	00 05 4	63,541	380	0.08044	NS
	I		78,391	644	0.08044	86.29		-18,143	3,148	0.08044	20.14		63,541	854	0.08044	66.48
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		101,597	11,446	0.08044	4.69		-7,430	3,279	0.08044	19.07		61,569	10,936	0.08044	5.21
P	S	00 05 6	7,869	1,515	0.08044	40.46	00 05 7	-25,471	1,489	0.08044	42.99	00 05 8	-54,899	1,385	0.08044	47.93
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-28,791	1,814	0.08044	35.43		-7,222	4,831	0.08044	12.94		19,762	8,446	0.08044	7.14
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 05 9	-47,188	1,533	0.08044	42.90	00 06 0	-91,119	1,423	0.08044	48.71	00 06 1	-61,626	1,985	0.08044	33.72
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-13,665	8,074	0.08044	7.81		3,060	2,663	0.08044	23.17		-118,427	4,771	0.08044	14.99
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 06 2	-45,872	787	0.08044	83.43	00 06 3	29,330	538	0.08044	NS	00 06 4	50,768	118	0.08044	NS
	I		-45,872	27	0.08044	NS		29,330	430	0.08044	NS		50,768	1,328	0.08044	43.54
S	S		-66,853	3,411	0.08044	19.75		0	0	0.08044	-		0	0	0.08044	-
	I		0	0	0.08044	-		-2,158	1,052	0.08044	59.05		31,487	8,837	0.08044	6.72
P	S	00 09 4	-30,179	418	0.08044	NS	00 09 5	-33,118	1,196	0.08044	54.04	00 09 6	-19,731	1,323	0.08044	48.03
	I		-30,179	210	0.08044	NS		0	0	0.08044	-		0	0	0.08044	-
S	S		-1,455	1,889	0.08044	32.85		-4,285	4,842	0.08044	12.86		9,251	7,210	0.08044	8.49
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 09 7	-35,389	2,025	0.08044	32.00	00 09 8	-60,189	1,504	0.08044	44.42	00 09 9	-104,542	1,673	0.08044	42.07
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		3,178	8,106	0.08044	7.61		1,946	2,826	0.08044	21.86		-96,269	4,148	0.08044	16.81
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 10 0	-57,204	1,098	0.08044	60.63	00 10 1	-1,569	380	0.08044	NS	00 10 2	0	0	0.08044	-
	I		0	0	0.08044	-		-1,569	381	0.08044	NS		47,563	1,732	0.08044	33.53
S	S		-78,163	3,782	0.08044	18.05		-8,055	155	0.08044	NS		0	0	0.08044	-
	I		0	0	0.08044	-		-8,055	747	0.08044	83.80		19,315	5,705	0.08044	10.58
P	S	00 10 3	-40,578	9,418	0.08044	6.93	00 10 4	-72,974	9,125	0.08044	7.44	00 10 5	41,345	10,399	0.08044	5.63
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		46,092	5,691	0.08044	10.23		81,831	4,116	0.08044	13.43		10,317	3,884	0.08044	15.73
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 10 6	-6,378	12,542	0.08044	4.98	00 10 7	28,292	12,921	0.08044	4.62	00 10 8	-42,109	15,182	0.08044	4.30
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		72,018	3,930	0.08044	14.27		-41,386	2,866	0.08044	22.78		12,758	3,007	0.08044	20.25
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 10 9	97,076	14,795	0.08044	3.65	00 11 0	-15,839	15,907	0.08044	3.97	00 11 1	-59,238	16,002	0.08044	4.17
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-



## Solette - Verifiche pressoflessione retta allo stato limite di danno

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
S	S		-25,062	2,927	0.08044	21.86		-7,363	3,171	0.08044	19.72		53,250	4,646	0.08044	12.40
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00112	17,238	15,644	0.08044	3.87	00113	-51,057	15,886	0.08044	4.16	00114	10,268	15,664	0.08044	3.90
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-9,695	3,878	0.08044	16.18		-10,950	2,914	0.08044	21.56		-6,542	3,696	0.08044	16.90
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00115	-29,660	16,417	0.08044	3.92	00116	6,471	16,245	0.08044	3.78	00117	-19,777	16,109	0.08044	3.94
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-4,384	3,068	0.08044	20.31		-2,610	3,587	0.08044	17.33		28,743	4,561	0.08044	13.07
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00118	8,852	15,123	0.08044	4.05	00119	-45,632	15,982	0.08044	4.11	00120	-3,676	15,809	0.08044	3.94
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-6,998	3,558	0.08044	17.57		45,940	4,450	0.08044	13.08		-20,937	3,632	0.08044	17.52
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00121	-15,832	15,899	0.08044	3.98	00122	-41,975	15,947	0.08044	4.10	00123	52,364	14,144	0.08044	4.08
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		1,913	3,662	0.08044	16.87		10,363	2,973	0.08044	20.55		-42,189	3,322	0.08044	19.67
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00124	4,811	14,016	0.08044	4.39	00125	56,794	12,017	0.08044	4.77	00126	-90,347	11,539	0.08044	6.00
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		74,229	4,134	0.08044	13.52		7,252	3,933	0.08044	15.60		67,082	4,335	0.08044	13.03
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00127	7,250	9,194	0.08044	6.67	00128	-72,921	9,024	0.08044	7.52	00137	0	0	0.08044	-
	I		0	0	0.08044	-		0	0	0.08044	-		32,727	3,422	0.08044	17.32
S	S		24,943	2,290	0.08044	26.16		84,283	4,343	0.08044	12.68		0	0	0.08044	-
	I		0	0	0.08044	-		0	0	0.08044	-		17,087	2,266	0.08044	26.72
P	S	00379	-15,941	406	0.08044	NS	00380	0	0	0.08044	-	00381	-42,007	3,301	0.08044	19.80
	I		-15,941	242	0.08044	NS		11,531	405	0.08044	NS		0	0	0.08044	-
S	S		-17,219	969	0.08044	65.36		-4,210	79	0.08044	NS		-31,472	493	0.08044	NS
	I		0	0	0.08044	-		-4,210	104	0.08044	NS		0	0	0.08044	-
P	S	00382	-73,585	7,771	0.08044	8.74	00383	-31,274	9,131	0.08044	7.06	00384	-14,478	12,940	0.08044	4.88
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-51,006	1,664	0.08044	39.71		-37,291	2,200	0.08044	29.53		-28,041	3,128	0.08044	20.53
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00385	-1,833	15,060	0.08044	4.12	00386	16,125	14,986	0.08044	4.05	00387	6,833	16,660	0.08044	3.68
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-29,419	3,122	0.08044	20.60		-25,455	3,233	0.08044	19.80		-17,140	4,154	0.08044	15.25
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00388	-1,097	16,740	0.08044	3.71	00389	4,171	18,426	0.08044	3.34	00390	6,301	18,209	0.08044	3.37
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-22,691	4,114	0.08044	15.50		-16,834	3,697	0.08044	17.12		-12,493	4,530	0.08044	13.90
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00391	690	18,229	0.08044	3.39	00392	3,480	19,482	0.08044	3.16	00393	3,778	18,610	0.08044	3.31
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-18,080	4,398	0.08044	14.42		-10,783	3,949	0.08044	15.91		-10,513	4,609	0.08044	13.62
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-



Solette - Verifiche pressoflessione retta allo stato limite di danno

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
P	S	00394	1,018	18,871	0.08044	3.28	00395	918	19,308	0.08044	3.20	00396	681	20,991	0.08044	2.95
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-13,969	4,470	0.08044	14.11		-10,648	4,055	0.08044	15.49		-13,642	4,295	0.08044	14.68
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00397	1,969	19,402	0.08044	3.18	00398	2,228	19,322	0.08044	3.20	00399	1,565	21,043	0.08044	2.94
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-11,396	4,544	0.08044	13.84		-11,347	4,119	0.08044	15.26		-13,468	4,246	0.08044	14.85
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00400	1,639	19,400	0.08044	3.19	00401	3,522	19,062	0.08044	3.23	00402	-1,210	20,975	0.08044	2.96
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-10,247	4,423	0.08044	14.19		-12,925	4,097	0.08044	15.37		-14,756	4,218	0.08044	14.97
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00403	-296	18,886	0.08044	3.28	00404	4,326	18,410	0.08044	3.35	00405	-244	20,019	0.08044	3.10
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-11,077	4,139	0.08044	15.18		-14,777	4,041	0.08044	15.62		-15,461	3,995	0.08044	15.82
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00406	-3,250	17,829	0.08044	3.49	00407	2,988	16,464	0.08044	3.75	00408	-4,209	17,512	0.08044	3.56
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-11,289	3,777	0.08044	16.64		-17,054	3,701	0.08044	17.11		-15,660	3,501	0.08044	18.06
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00409	-8,260	14,444	0.08044	4.33	00410	-1,961	11,448	0.08044	5.42	00411	792	8,665	0.08044	7.14
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-10,893	2,970	0.08044	21.15		-11,615	2,718	0.08044	23.14		-7,724	2,703	0.08044	23.15
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00412	-6,609	6,545	0.08044	9.55	00413	-10,310	2,818	0.08044	22.28	00414	-16,451	377	0.08044	NS
I			0	0	0.08044	-		0	0	0.08044	-		-16,451	149	0.08044	NS
S	S		-4,078	1,407	0.08044	44.26		-5,762	462	0.08044	NS		586	508	0.08044	NS
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00415	46,274	13,842	0.08044	4.20	00609	-104,656	81	0.08044	NS	00610	0	0	0.08044	-
I			0	0	0.08044	-		0	0	0.08044	-		-14,269	158	0.08044	NS
S	S		39,960	5,048	0.08044	11.63		-314,276	802	0.08044	NS		0	0	0.08044	-
I			0	0	0.08044	-		0	0	0.08044	-		-98,290	957	0.08044	73.03
P	S	00611	4,549	154	0.08044	NS	00612	0	0	0.08044	-	00613	0	0	0.08044	-
I			0	0	0.08044	-		-9,968	551	0.08044	NS		-5,156	221	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
I			-96,164	1,527	0.08044	45.66		-76,916	1,587	0.08044	42.95		-53,221	1,650	0.08044	40.15
P	S	00614	0	0	0.08044	-	00615	0	0	0.08044	-	00616	-1,138	139	0.08044	NS
I			2,499	200	0.08044	NS		6,998	425	0.08044	NS		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
I			-17,291	1,669	0.08044	37.95		1,485	1,395	0.08044	44.32		12,529	1,326	0.08044	45.95
P	S	00617	0	0	0.08044	-	00618	0	0	0.08044	-	00619	0	0	0.08044	-
I			-1,483	356	0.08044	NS		1,859	258	0.08044	NS		1,893	295	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
I			12,956	1,109	0.08044	54.91		41,048	893	0.08044	65.63		66,407	792	0.08044	71.39
P	S	00620	0	0	0.08044	-	00621	0	0	0.08044	-	00622	0	0	0.08044	-



Solette - Verifiche pressoflessione retta allo stato limite di danno

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
	I		0	0	0.08044	-		145	85	0.08044	NS		1,795	242	0.08044	NS
S	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		65,829	534	0.08044	NS		94,081	368	0.08044	NS		83,995	326	0.08044	NS
P	S	00 62 3	0	0	0.08044	-	00 62 4	0	0	0.08044	-	00 62 5	0	0	0.08044	-
	I		6,030	310	0.08044	NS		4,775	190	0.08044	NS		3,022	57	0.08044	NS
S	S		109,187	17	0.08044	NS		120,423	38	0.08044	NS		128,950	325	0.08044	NS
	I		112,523	178	0.08044	NS		120,423	96	0.08044	NS		0	0	0.08044	-
P	S	00 62 6	0	0	0.08044	-	00 62 7	0	0	0.08044	-	00 62 8	0	0	0.08044	-
	I		4,137	109	0.08044	NS		2,612	214	0.08044	NS		9,204	334	0.08044	NS
S	S		146,478	333	0.08044	NS		133,819	318	0.08044	NS		160,175	343	0.08044	NS
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 62 9	0	0	0.08044	-	00 63 0	0	0	0.08044	-	00 63 1	0	0	0.08044	-
	I		6,482	69	0.08044	NS		3,031	127	0.08044	NS		4,812	60	0.08044	NS
S	S		154,121	375	0.08044	NS		173,615	794	0.08044	60.20		158,105	458	0.08044	NS
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 63 2	0	0	0.08044	-	00 63 3	0	0	0.08044	-	00 63 4	0	0	0.08044	-
	I		9,549	351	0.08044	NS		2,448	200	0.08044	NS		7,133	76	0.08044	NS
S	S		180,157	496	0.08044	95.28		173,634	593	0.08044	80.60		182,883	729	0.08044	64.52
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 63 5	0	0	0.08044	-	00 63 6	0	0	0.08044	-	00 63 7	0	0	0.08044	-
	I		2,827	133	0.08044	NS		5,637	71	0.08044	NS		10,251	361	0.08044	NS
S	S		187,814	917	0.08044	50.86		171,888	627	0.08044	76.45		187,164	653	0.08044	71.50
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 63 8	0	0	0.08044	-	00 63 9	0	0	0.08044	-	00 64 0	0	0	0.08044	-
	I		4,070	138	0.08044	NS		4,355	111	0.08044	NS		4,171	113	0.08044	NS
S	S		170,917	623	0.08044	77.07		184,374	791	0.08044	59.31		179,895	824	0.08044	57.38
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 64 1	0	0	0.08044	-	00 64 2	0	0	0.08044	-	00 64 3	0	0	0.08044	-
	I		4,480	130	0.08044	NS		9,360	357	0.08044	NS		3,997	106	0.08044	NS
S	S		168,366	558	0.08044	86.42		175,497	503	0.08044	94.72		152,009	446	0.08044	NS
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 64 4	0	0	0.08044	-	00 64 5	0	0	0.08044	-	00 64 6	0	0	0.08044	-
	I		2,984	121	0.08044	NS		5,129	72	0.08044	NS		2,188	218	0.08044	NS
S	S		166,579	677	0.08044	71.45		148,943	502	0.08044	99.23		144,272	301	0.08044	NS
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 64 7	0	0	0.08044	-	00 64 8	0	0	0.08044	-	00 64 9	0	0	0.08044	-
	I		6,717	356	0.08044	NS		1,561	153	0.08044	NS		2,814	77	0.08044	NS
S	S		136,535	162	0.08044	NS		110,869	33	0.08044	NS		118,963	231	0.08044	NS
	I		0	0	0.08044	-		110,869	109	0.08044	NS		0	0	0.08044	-
P	S	00 65 0	0	0	0.08044	-	00 65 1	0	0	0.08044	-	00 65 2	0	0	0.08044	-
	I		6,524	164	0.08044	NS		6,896	349	0.08044	NS		1,479	317	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		101,701	321	0.08044	NS		96,278	463	0.08044	NS		60,931	601	0.08044	94.82
P	S	00 65 3	0	0	0.08044	-	00 65 4	847	33	0.08044	NS	00 65 5	0	0	0.08044	-
	I		3,533	138	0.08044	NS		0	0	0.08044	-		3,317	372	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		73,457	704	0.08044	79.50		42,975	871	0.08044	67.11		40,924	1,119	0.08044	52.38
P	S	00 65 6	0	0	0.08044	-	00 65 7	0	0	0.08044	-	00 65 8	0	0	0.08044	-



**Solette - Verifiche pressoflessione retta allo stato limite di danno**

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
	I		1,444	319	0.08044	NS		-853	490	0.08044	NS		716	30	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		18,861	1,285	0.08044	47.01		-13,961	1,440	0.08044	43.80		-8,826	1,634	0.08044	38.35
P	S	00659	0	0	0.08044	-	00660	0	0	0.08044	-	00661	0	0	0.08044	-
	I		-248	18	0.08044	NS		-2,916	479	0.08044	NS		-19,672	324	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-50,247	1,671	0.08044	39.50		-40,880	1,672	0.08044	39.03		-103,188	1,374	0.08044	51.15
P	S	00662	0	0	0.08044	-	00663	-62,509	97	0.08044	NS	00664	-228,787	311	0.08044	NS
	I		-3,030	609	0.08044	NS		0	0	0.08044	-		0	0	0.08044	-
S	S		0	0	0.08044	-		-302,988	800	0.08044	NS		-88,768	652	0.08044	NS
	I		-115,352	898	0.08044	79.35		0	0	0.08044	-		0	0	0.08044	-
P	S	00665	-103,014	805	0.08044	87.29	00666	-115,109	1,994	0.08044	35.73	00667	-87,483	1,131	0.08044	61.02
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-7,060	838	0.08044	74.60		0	0	0.08044	-		3,181	768	0.08044	80.32
	I		0	0	0.08044	-		-4,849	531	0.08044	NS		0	0	0.08044	-
P	S	00668	-91,704	213	0.08044	NS	00669	-5,370	287	0.08044	NS	00670	6,135	656	0.08044	93.67
	I		-91,704	184	0.08044	NS		0	0	0.08044	-		0	0	0.08044	-
S	S		-8,814	727	0.08044	86.19		38,580	3,705	0.08044	15.87		59,231	797	0.08044	71.68
	I		0	0	0.08044	-		0	0	0.08044	-		59,231	335	0.08044	NS
P	S	00671	0	0	0.08044	-	00672	0	0	0.08044	-	00673	0	0	0.08044	-
	I		2,889	135	0.08044	NS		5,335	473	0.08044	NS		5,905	186	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		70,528	1,401	0.08044	40.12		61,459	2,016	0.08044	28.25		75,648	2,368	0.08044	23.56
P	S	00674	0	0	0.08044	-	00675	0	0	0.08044	-	00676	1,105	276	0.08044	NS
	I		5,123	117	0.08044	NS		3,709	540	0.08044	NS		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		73,883	2,534	0.08044	22.07		60,519	2,419	0.08044	23.57		67,938	2,456	0.08044	22.97
P	S	00677	0	0	0.08044	-	00678	0	0	0.08044	-	00679	0	0	0.08044	-
	I		3,848	413	0.08044	NS		4,070	166	0.08044	NS		1,134	380	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		56,397	2,119	0.08044	27.07		55,822	1,896	0.08044	30.28		42,139	1,733	0.08044	33.77
P	S	00680	915	82	0.08044	NS	00681	0	0	0.08044	-	00682	0	0	0.08044	-
	I		0	0	0.08044	-		1,312	60	0.08044	NS		1,368	261	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		47,207	1,420	0.08044	40.92		40,080	1,189	0.08044	49.36		36,260	1,073	0.08044	54.98
P	S	00683	0	0	0.08044	-	00684	0	0	0.08044	-	00685	249	34	0.08044	NS
	I		2,151	256	0.08044	NS		778	273	0.08044	NS		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		31,947	178	0.08044	NS
	I		35,162	851	0.08044	69.43		28,648	710	0.08044	83.97		31,947	429	0.08044	NS
P	S	00686	0	0	0.08044	-	00687	0	0	0.08044	-	00688	0	0	0.08044	-
	I		1,090	103	0.08044	NS		485	217	0.08044	NS		1,616	303	0.08044	NS
S	S		28,747	251	0.08044	NS		26,753	226	0.08044	NS		27,331	297	0.08044	NS
	I		28,747	332	0.08044	NS		26,753	349	0.08044	NS		27,331	247	0.08044	NS
P	S	00689	0	0	0.08044	-	00690	0	0	0.08044	-	00691	0	0	0.08044	-
	I		739	148	0.08044	NS		342	90	0.08044	NS		1,081	96	0.08044	NS
S	S		23,381	343	0.08044	NS		26,857	754	0.08044	79.26		22,580	457	0.08044	NS
	I		23,381	177	0.08044	NS		0	0	0.08044	-		22,580	40	0.08044	NS



Solette - Verifiche pressoflessione retta allo stato limite di danno

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
P	S	00692	0	0	0.08044	-	00693	0	0	0.08044	-	00694	0	0	0.08044	-
	I		1,683	315	0.08044	NS		343	222	0.08044	NS		1,054	59	0.08044	NS
S	S		25,161	478	0.08044	NS		22,120	548	0.08044	NS		24,037	649	0.08044	92.44
	I		25,161	22	0.08044	NS		0	0	0.08044	-		0	0	0.08044	-
P	S	00695	0	0	0.08044	-	00696	0	0	0.08044	-	00697	0	0	0.08044	-
	I		397	105	0.08044	NS		914	120	0.08044	NS		1,596	326	0.08044	NS
S	S		24,062	844	0.08044	71.08		21,211	533	0.08044	NS		23,577	534	0.08044	NS
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00698	0	0	0.08044	-	00699	0	0	0.08044	-	00700	0	0	0.08044	-
	I		632	173	0.08044	NS		624	90	0.08044	NS		557	75	0.08044	NS
S	S		20,816	526	0.08044	NS		23,037	727	0.08044	82.63		22,836	722	0.08044	83.22
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00701	0	0	0.08044	-	00702	0	0	0.08044	-	00703	0	0	0.08044	-
	I		719	180	0.08044	NS		1,646	325	0.08044	NS		857	156	0.08044	NS
S	S		20,559	450	0.08044	NS		23,007	396	0.08044	NS		20,203	321	0.08044	NS
	I		20,559	49	0.08044	NS		23,007	89	0.08044	NS		20,203	152	0.08044	NS
P	S	00704	0	0	0.08044	-	00705	0	0	0.08044	-	00706	0	0	0.08044	-
	I		472	96	0.08044	NS		924	30	0.08044	NS		492	269	0.08044	NS
S	S		23,095	528	0.08044	NS		22,544	315	0.08044	NS		20,716	103	0.08044	NS
	I		0	0	0.08044	-		22,544	202	0.08044	NS		20,716	423	0.08044	NS
P	S	00707	0	0	0.08044	-	00708	0	0	0.08044	-	00709	814	31	0.08044	NS
	I		1,768	311	0.08044	NS		1,394	279	0.08044	NS		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		23,187	560	0.08044	NS		19,935	686	0.08044	87.94		23,947	717	0.08044	83.68
P	S	00710	0	0	0.08044	-	00711	0	0	0.08044	-	00712	0	0	0.08044	-
	I		1,450	374	0.08044	NS		2,370	313	0.08044	NS		507	367	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		20,123	1,017	0.08044	59.30		23,519	1,245	0.08044	48.22		20,952	1,506	0.08044	40.00
P	S	00713	0	0	0.08044	-	00714	691	142	0.08044	NS	00715	0	0	0.08044	-
	I		1,048	165	0.08044	NS		0	0	0.08044	-		1,025	540	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		23,213	1,649	0.08044	36.42		23,876	1,992	0.08044	30.12		20,947	2,149	0.08044	28.03
P	S	00716	0	0	0.08044	-	00717	0	0	0.08044	-	00718	1,187	71	0.08044	NS
	I		2,318	269	0.08044	NS		1,055	582	0.08044	NS		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		24,687	2,331	0.08044	25.71		22,131	2,448	0.08044	24.57		25,581	2,613	0.08044	22.91
P	S	00719	0	0	0.08044	-	00720	0	0	0.08044	-	00721	0	0	0.08044	-
	I		1,415	99	0.08044	NS		1,604	418	0.08044	NS		3,897	311	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		27,910	2,400	0.08044	24.86		25,050	2,091	0.08044	28.65		34,121	1,229	0.08044	48.15
P	S	00722	0	0	0.08044	-	00723	4,230	182	0.08044	NS	00724	-56,262	342	0.08044	NS
	I		5,294	468	0.08044	NS		0	0	0.08044	-		-56,262	337	0.08044	NS
S	S		25,705	1,142	0.08044	52.41		46,238	3,765	0.08044	15.45		-2,791	1,226	0.08044	50.71
	I		25,705	96	0.08044	NS		0	0	0.08044	-		0	0	0.08044	-
P	S	00725	-71,675	1,098	0.08044	61.70	00726	-83,813	943	0.08044	72.87	00727	-92,016	568	0.08044	NS
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-3,525	1,262	0.08044	49.31		1,504	938	0.08044	65.91		-4,468	811	0.08044	76.82



## Solette - Verifiche pressoflessione retta allo stato limite di danno

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00728	-303,870	953	0.08044	90.45	00891	4,845	8,620	0.08044	7.14	00892	27,296	14,947	0.08044	4.00
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		0	0	0.08044	-		-39,082	2,894	0.08044	22.50		-24,165	4,740	0.08044	13.48
	I		-95,745	683	0.08044	NS		0	0	0.08044	-		0	0	0.08044	-
P	S	00894	-39,239	15,731	0.08044	4.14	00896	42,786	15,832	0.08044	3.69	00898	-16,886	17,174	0.08044	3.69
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		48,292	5,456	0.08044	10.63		-26,315	4,272	0.08044	15.00		-25,901	4,438	0.08044	14.43
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00901	-1,360	15,360	0.08044	4.04	00902	-42,637	16,689	0.08044	3.92	00904	-15,629	13,057	0.08044	4.84
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-46,066	4,536	0.08044	14.48		-14,452	4,013	0.08044	15.73		1,874	3,803	0.08044	16.25
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00906	57,456	9,394	0.08044	6.10	00909	20,184	14,284	0.08044	4.22	00910	-2,726	13,296	0.08044	4.68
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-32,784	1,863	0.08044	34.67		-26,175	4,811	0.08044	13.32		14,312	3,774	0.08044	16.11
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00912	-28,576	8,954	0.08044	7.18	00914	53,576	12,081	0.08044	4.77	00917	-2,570	16,437	0.08044	3.78
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		39,688	2,149	0.08044	27.32		48,220	4,927	0.08044	11.78		-28,290	4,619	0.08044	13.91
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00918	-58,206	16,346	0.08044	4.08	00921	-8,407	17,767	0.08044	3.52	00922	-9,472	17,975	0.08044	3.49
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		22,840	4,939	0.08044	12.17		-31,620	4,579	0.08044	14.09		-31,776	4,484	0.08044	14.39
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00923	9,699	16,830	0.08044	3.63	00924	-26,457	16,447	0.08044	3.90	00928	-14,378	17,193	0.08044	3.67
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-15,044	4,496	0.08044	14.05		18,022	5,099	0.08044	11.86		-23,668	4,504	0.08044	14.18
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00930	38,893	14,989	0.08044	3.92	00932	-48,008	15,427	0.08044	4.27	00935	39,818	15,765	0.08044	3.72
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-13,060	5,238	0.08044	12.03		53,547	5,482	0.08044	10.51		-30,754	4,208	0.08044	15.31
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00936	-57,490	16,595	0.08044	4.01	00939	99,725	11,930	0.08044	4.51	00940	-11,641	15,052	0.08044	4.18
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-17,882	4,079	0.08044	15.54		-45,876	2,771	0.08044	23.69		-6,352	4,101	0.08044	15.23
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00943	-61,272	11,440	0.08044	5.85	00944	1,130	14,559	0.08044	4.25	00947	-7,174	1,249	0.08044	50.06
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		12,320	2,534	0.08044	24.05		8,868	3,895	0.08044	15.72		-43,329	2,569	0.08044	25.48
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00948	40,089	456	0.08044	NS	00951	-17,315	1,129	0.08044	56.11	00953	-20,982	1,556	0.08044	40.90
	I		45,176	590	0.08044	98.77		0	0	0.08044	-		0	0	0.08044	-
S	S		0	0	0.08044	-		-21,979	2,222	0.08044	28.68		6,589	6,053	0.08044	10.14
	I		8,829	2,836	0.08044	21.59		0	0	0.08044	-		0	0	0.08044	-



Solette - Verifiche pressoflessione retta allo stato limite di danno

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
P	S	00 95 5	-82,952	1,349	0.08044	50.89	00 95 7	-74,075	2,189	0.08044	31.04	00 95 8	-44,226	1,137	0.08044	57.63
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-1,665	2,380	0.08044	26.08		-127,224	4,483	0.08044	16.11		8,627	8,455	0.08044	7.24
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 96 1	-48,995	2,386	0.08044	27.62	01 04 3	-130,784	1,392	0.08044	52.08	01 04 4	-62,845	1,924	0.08044	34.84
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-339	5,711	0.08044	10.85		-15,616	2,921	0.08044	21.64		-115,051	4,539	0.08044	15.69
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01 04 7	-36,270	1,742	0.08044	37.25	01 04 8	-68,873	1,855	0.08044	36.40	01 05 1	-37,034	799	0.08044	81.28
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		7,945	7,987	0.08044	7.67		-3,566	5,056	0.08044	12.31		-23,826	1,600	0.08044	39.92
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01 05 2	45,148	130	0.08044	NS	01 05 5	-25,246	943	0.08044	67.86	01 05 6	-25,045	1,334	0.08044	47.96
	I		45,148	1,036	0.08044	56.25		0	0	0.08044	-		0	0	0.08044	-
S	S		0	0	0.08044	-		-16,988	3,405	0.08044	18.60		12,525	6,848	0.08044	8.90
	I		54,405	3,736	0.08044	15.40		0	0	0.08044	-		0	0	0.08044	-
P	S	01 43 7	7,436	159	0.08044	NS	01 43 8	-21,342	143	0.08044	NS	01 43 9	96,605	2,330	0.08044	23.21
	I		7,436	301	0.08044	NS		-21,342	247	0.08044	NS		0	0	0.08044	-
S	S		2,952	209	0.08044	NS		0	0	0.08044	-		36,103	122	0.08044	NS
	I		2,952	271	0.08044	NS		7,030	591	0.08044	NS		36,103	354	0.08044	NS
P	S	01 44 0	78,625	1,657	0.08044	33.52	01 44 1	16,902	1,616	0.08044	37.48	01 44 2	0	0	0.08044	-
	I		0	0	0.08044	-		0	0	0.08044	-		-64,897	604	0.08044	NS
S	S		25,221	319	0.08044	NS		3,056	460	0.08044	NS		-65,411	35	0.08044	NS
	I		25,221	162	0.08044	NS		0	0	0.08044	-		-65,411	459	0.08044	NS
P	S	01 44 3	0	0	0.08044	-	01 44 4	0	0	0.08044	-	01 44 5	-15,078	1,126	0.08044	56.10
	I		-5,913	707	0.08044	88.29		-12,923	441	0.08044	NS		0	0	0.08044	-
S	S		9,100	3,419	0.08044	17.90		-504	506	0.08044	NS		0	0	0.08044	-
	I		0	0	0.08044	-		-504	202	0.08044	NS		-28,036	524	0.08044	NS
P	S	01 44 6	0	0	0.08044	-	01 44 7	0	0	0.08044	-	01 44 8	-5,435	2,407	0.08044	25.92
	I		1,968	528	0.08044	NS		-1,105	790	0.08044	78.52		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-82,603	1,317	0.08044	52.11		10,613	1,249	0.08044	48.90		-3,059	526	0.08044	NS
P	S	01 44 9	-19,634	5,885	0.08044	49.80	01 45 0	-3,401	122	0.08044	NS	01 45 1	0	0	0.08044	-
	I		0	0	0.08044	-		-3,401	43	0.08044	NS		47	721	0.08044	85.91
S	S		-13,418	856	0.08044	73.63		0	0	0.08044	-		0	0	0.08044	-
	I		0	0	0.08044	-		-32,679	1,043	0.08044	61.93		18,752	2,187	0.08044	27.63
P	S	01 45 2	-382	1,242	0.08044	49.90	01 45 3	-7,653	2,898	0.08044	21.59	01 45 4	0	0	0.08044	-
	I		0	0	0.08044	-		0	0	0.08044	-		593	334	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		1,710	1,055	0.08044	58.58		-6,201	477	0.08044	NS		3,162	1,165	0.08044	52.95
P	S	01 45 5	899	98	0.08044	NS	01 45 6	1,199	6,104	0.08044	10.13	01 45 7	-4,476	8,123	0.08044	7.67
	I		899	175	0.08044	NS		0	0	0.08044	-		0	0	0.08044	-
S	S		0	0	0.08044	-		-4,267	507	0.08044	NS		9,205	991	0.08044	61.75
	I		11,052	1,616	0.08044	37.78		0	0	0.08044	-		0	0	0.08044	-



Solette - Verifiche pressoflessione retta allo stato limite di danno

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
P	S	01458	989	837	0.08044	73.91	01459	0	0	0.08044	-	01460	1,190	3,008	0.08044	20.56
	I		0	0	0.08044	-		89	403	0.08044	NS		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		2,455	134	0.08044	NS
	I		25,478	343	0.08044	NS		17,325	1,578	0.08044	38.36		2,455	162	0.08044	NS
P	S	01461	6,421	12,419	0.08044	4.95	01462	-7,743	3,955	0.08044	15.82	01463	0	0	0.08044	-
	I		0	0	0.08044	-		0	0	0.08044	-		-481	88	0.08044	NS
S	S		-9,840	2,440	0.08044	25.71		27,668	371	0.08044	NS		0	0	0.08044	-
	I		0	0	0.08044	-		0	0	0.08044	-		65,618	376	0.08044	NS
P	S	01464	754	981	0.08044	63.08	01465	1,916	8,118	0.08044	7.61	01466	-14,805	9,075	0.08044	6.96
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		0	0	0.08044	-		-4,534	1,322	0.08044	47.13		20,172	1,368	0.08044	44.08
	I		11,327	655	0.08044	93.16		0	0	0.08044	-		0	0	0.08044	-
P	S	01467	-24	1,340	0.08044	46.23	01468	0	0	0.08044	-	01469	1,268	4,186	0.08044	14.77
	I		0	0	0.08044	-		392	152	0.08044	NS		0	0	0.08044	-
S	S		72,142	331	0.08044	NS		0	0	0.08044	-		2,901	794	0.08044	77.72
	I		0	0	0.08044	-		16,679	628	0.08044	96.48		0	0	0.08044	-
P	S	01470	5,405	14,564	0.08044	4.22	01471	-3,890	4,540	0.08044	13.71	01472	-1,577	66	0.08044	NS
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-10,061	3,021	0.08044	20.77		55,206	613	0.08044	93.73		112,517	262	0.08044	NS
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01473	705	1,479	0.08044	41.84	01474	1,471	9,223	0.08044	6.70	01475	-6,600	9,601	0.08044	6.51
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		11,497	414	0.08044	NS		-4,084	1,646	0.08044	37.83		30,520	1,408	0.08044	42.23
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01476	-326	1,654	0.08044	37.47	01477	135	133	0.08044	NS	01478	1,191	4,732	0.08044	13.07
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		102,568	624	0.08044	85.89		17,251	390	0.08044	NS		3,379	1,087	0.08044	56.73
	I		0	0	0.08044	-		17,251	61	0.08044	NS		0	0	0.08044	-
P	S	01479	4,624	15,335	0.08044	4.01	01480	-1,930	4,906	0.08044	12.66	01481	-81	141	0.08044	NS
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-9,254	3,214	0.08044	19.51		71,061	771	0.08044	72.85		138,361	596	0.08044	85.03
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01482	707	1,681	0.08044	36.81	01483	1,449	9,628	0.08044	6.42	01484	-10,021	10,156	0.08044	6.18
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		11,845	711	0.08044	85.77		-3,411	1,774	0.08044	35.07		37,301	1,630	0.08044	36.14
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01485	-916	1,815	0.08044	34.17	01486	87	172	0.08044	NS	01487	1,251	4,881	0.08044	12.67
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		118,631	801	0.08044	65.28		17,603	616	0.08044	98.24		4,046	1,186	0.08044	51.95
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01488	4,220	15,489	0.08044	3.98	01489	-6,476	5,179	0.08044	12.06	01490	-1,793	226	0.08044	NS
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-8,539	3,157	0.08044	19.84		74,872	880	0.08044	63.47		153,176	709	0.08044	69.77
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	0149	717	1,703	0.08044	36.34	0149	1,669	9,661	0.08044	6.40	0149	-23,276	10,136	0.08044	6.30



## Solette - Verifiche pressoflessione retta allo stato limite di danno

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
	I	1	0	0	0.08044	-	2	0	0	0.08044	-	3	0	0	0.08044	-
S	S		12,600	789	0.08044	77.21		-2,711	1,802	0.08044	34.50		39,712	1,999	0.08044	29.37
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01494	52	1,947	0.08044	31.81	01495	141	155	0.08044	NS	01496	1,368	4,822	0.08044	12.82
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		123,062	963	0.08044	53.92		18,672	645	0.08044	93.68		4,816	1,189	0.08044	51.77
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01497	5,371	15,313	0.08044	4.02	01498	-10,256	5,429	0.08044	11.56	01499	-1,860	250	0.08044	NS
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-8,215	3,063	0.08044	20.44		72,878	1,160	0.08044	48.29		150,038	674	0.08044	73.77
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01500	760	1,627	0.08044	38.03	01501	2,465	9,507	0.08044	6.49	01502	-21,486	10,420	0.08044	6.11
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		13,770	754	0.08044	80.67		-2,407	1,786	0.08044	34.79		33,771	1,895	0.08044	31.24
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01503	-1,037	1,918	0.08044	32.34	01504	563	76	0.08044	NS	01505	1,717	4,573	0.08044	13.51
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		113,288	843	0.08044	62.54		20,004	568	0.08044	NS		5,610	1,140	0.08044	53.94
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01506	4,721	15,347	0.08044	4.01	01507	-7,018	5,260	0.08044	11.88	01508	-1,332	224	0.08044	NS
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-8,485	3,036	0.08044	20.63		62,826	815	0.08044	69.74		130,041	521	0.08044	98.57
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01509	987	1,424	0.08044	43.44	01510	3,639	9,329	0.08044	6.61	01511	-3,203	10,120	0.08044	6.15
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		15,774	562	0.08044	NS		-3,432	1,732	0.08044	35.92		28,694	1,466	0.08044	40.66
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01512	-530	1,800	0.08044	34.44	01513	0	0	0.08044	-	01514	2,630	4,074	0.08044	15.15
	I		0	0	0.08044	-		-100	66	0.08044	NS		0	0	0.08044	-
S	S		88,681	622	0.08044	87.99		24,450	168	0.08044	NS		6,736	930	0.08044	66.02
	I		0	0	0.08044	-		24,450	362	0.08044	NS		0	0	0.08044	-
P	S	01515	7,227	14,704	0.08044	4.17	01516	-4,150	5,001	0.08044	12.45	01517	-576	125	0.08044	NS
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-10,177	2,845	0.08044	22.06		44,680	374	0.08044	NS		91,668	138	0.08044	NS
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01518	1,372	1,015	0.08044	60.92	01519	5,110	8,360	0.08044	7.36	01520	-13,424	9,599	0.08044	6.57
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		20,301	72	0.08044	NS		-4,705	1,434	0.08044	43.46		15,663	1,510	0.08044	40.18
	I		20,301	393	0.08044	NS		0	0	0.08044	-		0	0	0.08044	-
P	S	01521	-962	1,453	0.08044	42.68	01522	0	0	0.08044	-	01523	3,432	3,149	0.08044	19.58
	I		0	0	0.08044	-		-335	227	0.08044	NS		0	0	0.08044	-
S	S		53,776	213	0.08044	NS		0	0	0.08044	-		8,089	365	0.08044	NS
	I		0	0	0.08044	-		34,294	1,134	0.08044	52.17		0	0	0.08044	-
P	S	01524	9,442	13,050	0.08044	4.69	01525	-11,868	4,328	0.08044	14.53	01526	0	0	0.08044	-
	I		0	0	0.08044	-		0	0	0.08044	-		-1,824	75	0.08044	NS
S	S		-14,244	2,475	0.08044	25.		12,189	164	0.08044	NS		0	0	0.08044	-



**Solette - Verifiche pressoflessione retta allo stato limite di danno**

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
	I		0	0	0.08044	49 -		0	0	0.08044	-		41,791	663	0.08044	88.31
P	S	01 52 7	1,079	321	0.08044	NS	01 52 8	2,247	6,282	0.08044	9.8 3	01 52 9	-28,721	8,190	0.08044	7.85
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		0	0	0.08044	-		-8,677	774	0.08044	80. 94		-6,344	1,567	0.08044	39.86
	I		28,704	1,252	0.08044	47. 61		0	0	0.08044	-		0	0	0.08044	-
P	S	01 53 0	-2,641	793	0.08044	78. 38	01 53 1	0	0	0.08044	-	01 53 2	-2,515	1,642	0.08044	37.85
	I		0	0	0.08044	-		132	510	0.08044	NS		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		4,307	563	0.08044	NS		48,705	2,192	0.08044	26. 45		9,983	849	0.08044	72.00
P	S	01 53 3	-4,465	9,698	0.08044	6.4 2	01 53 4	-9,342	2,749	0.08044	22. 81	01 53 5	0	0	0.08044	-
	I		0	0	0.08044	-		0	0	0.08044	-		326	394	0.08044	NS
S	S		-21,191	1,662	0.08044	38. 30		0	0	0.08044	-		0	0	0.08044	-
	I		0	0	0.08044	-		-15,076	254	0.08044	NS		-28,687	1,318	0.08044	48.76
P	S	01 53 6	0	0	0.08044	-	01 53 7	-18,449	3,240	0.08044	19. 58	01 53 8	11,618	5,325	0.08044	11.46
	I		-3,652	634	0.08044	98. 17		0	0	0.08044	-		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		353 0	403 0	0.08044	NS
	I		35,084	1,878	0.08044	31. 47		-8,399	336	0.08044	NS		0	0	0.08044	-
P	S	01 53 9	0	0	0.08044	-	01 54 0	0	0	0.08044	-	01 54 1	-18,105	104	0.08044	NS
	I		-16,939	257	0.08044	NS		944	546	0.08044	NS		-18,105	176	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-49,268	862	0.08044	76. 49		43,043	1,464	0.08044	39. 92		8,277	1,126	0.08044	54.41
P	S	01 54 2	-45,866	3,723	0.08044	17. 64	01 54 3	-9,936	236	0.08044	NS	01 54 4	0	0	0.08044	-
	I		0	0	0.08044	-		-9,936	65	0.08044	NS		-76,820	590	0.08044	NS
S	S		-18,194	378	0.08044	NS		0	0	0.08044	-		-106,620	491	0.08044	NS
	I		0	0	0.08044	-		-3,803	272	0.08044	NS		-106,620	141	0.08044	NS
P	S	01 54 5	0	0	0.08044	-	01 54 6	-13,859	371	0.08044	NS	02 51 1	0	0	0.08044	-
	I		-15,874	644	0.08044	98. 18		-13,859	14	0.08044	NS		-138,177	640	0.08044	NS
S	S		10,993	2,303	0.08044	26. 51		-8,570	109	0.08044	NS		-169,800	2,444	0.08044	30.94
	I		0	0	0.08044	-		-8,570	368	0.08044	NS		0	0	0.08044	-
P	S	02 51 2	0	0	0.08044	-	02 51 3	0	0	0.08044	-	02 51 4	0	0	0.08044	-
	I		-159,761	585	0.08044	NS		-51,623	1,093	0.08044	60. 50		-29,481	1,321	0.08044	48.70
S	S		-180,901	2,389	0.08044	32. 02		-5,961	6,869	0.08044	9.0 9		9,118	7,457	0.08044	8.21
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
<b>Piano Terra</b>																
<b>Soletta P2-P3-P6-P5</b>																
P	S	00 00 5	-32,363	777	0.08044	83. 10	00 00 6	-14,485	1,544	0.08044	40. 88	00 00 7	-11,041	2,087	0.08044	30.11
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-372	2,289	0.08044	27. 07		-7,388	6,938	0.08044	9.0 1		-13,394	9,223	0.08044	6.83
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 00 8	-10,945	2,179	0.08044	28. 83	00 00 9	-11,138	2,058	0.08044	30. 54	00 01 0	-17,822	1,306	0.08044	48.54
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-13,330	9,251	0.08044	6.8 1		-6,192	7,142	0.08044	8.7 4		-12,287	4,310	0.08044	14.60
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 01 1	0	0	0.08044	-	00 01 2	-21,271	2,809	0.08044	22. 67	00 01 3	-18,337	5,694	0.08044	11.14
	I		-32,273	1,011	0.08044	63.		0	0	0.08044	-		0	0	0.08044	-



Solette - Verifiche pressoflessione retta allo stato limite di danno

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
S	S		0	0	0.08044	86		-27,656	521	0.08044	NS		-18,907	2,056	0.08044	30.87
I	I		-33,563	2,217	0.08044	-29.17		-27,656	360	0.08044	NS		0	0	0.08044	-
P	S	00014	-550	9,242	0.08044	6.71	00015	-7,283	11,708	0.08044	5.34	00016	-435	13,192	0.08044	4.70
I	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-12,813	1,960	0.08044	32.13		-6,366	3,564	0.08044	17.52		-16,467	3,099	0.08044	20.42
I	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00017	-10,992	15,438	0.08044	4.07	00018	-7,197	15,775	0.08044	3.96	00019	-4,322	16,816	0.08044	3.70
I	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-14,587	3,191	0.08044	19.78		-11,066	3,186	0.08044	19.72		-17,072	3,419	0.08044	18.52
I	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00020	-11,569	16,108	0.08044	3.90	00021	-2,509	16,301	0.08044	3.81	00022	-4,774	16,605	0.08044	3.75
I	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-14,242	3,894	0.08044	16.20		-19,963	3,271	0.08044	19.43		-17,987	4,418	0.08044	14.35
I	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00023	-2,816	16,727	0.08044	3.72	00024	-4,957	18,057	0.08044	3.45	00025	-3,863	17,760	0.08044	3.51
I	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-22,679	3,953	0.08044	16.13		-23,532	3,644	0.08044	17.52		-18,627	3,457	0.08044	18.35
I	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00026	-4,428	18,134	0.08044	3.44	00027	-2,247	16,874	0.08044	3.68	00028	-3,689	16,758	0.08044	3.71
I	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-23,316	3,635	0.08044	17.56		-23,034	4,001	0.08044	15.95		-18,990	4,396	0.08044	14.44
I	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00029	-1,538	16,569	0.08044	3.75	00030	-9,619	16,410	0.08044	3.82	00031	-5,430	17,202	0.08044	3.63
I	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-21,873	3,400	0.08044	18.74		-16,113	3,919	0.08044	16.14		-20,046	3,483	0.08044	18.25
I	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00032	-9,638	16,402	0.08044	3.82	00033	-14,511	16,306	0.08044	3.87	00034	-8,625	14,757	0.08044	4.24
I	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-15,476	3,267	0.08044	19.34		-18,104	3,376	0.08044	18.78		-16,334	3,610	0.08044	17.53
I	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00035	-13,142	14,398	0.08044	4.38	00036	-6,202	13,974	0.08044	4.47	00037	18,331	14,305	0.08044	4.23
I	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		1,243	4,034	0.08044	15.33		-3,174	2,884	0.08044	21.57		9,353	2,938	0.08044	20.82
I	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00038	87,682	10,109	0.08044	5.42	00039	1,006	252	0.08044	NS	00040	14,810	141	0.08044	NS
I	I		0	0	0.08044	-		1,006	228	0.08044	NS		14,810	77	0.08044	NS
S	S		18,575	1,864	0.08044	32.42		-42,234	470	0.08044	NS		-3,505	198	0.08044	NS
I	I		0	0	0.08044	-		-42,234	712	0.08044	91.80		0	0	0.08044	-
P	S	00041	13,775	239	0.08044	NS	00042	9,970	472	0.08044	NS	00043	-2,344	405	0.08044	NS
I	I		13,775	64	0.08044	NS		9,970	31	0.08044	NS		-2,344	187	0.08044	NS
S	S		-3,214	181	0.08044	NS		-1,945	270	0.08044	NS		-2,419	236	0.08044	NS
I	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00044	-21,950	309	0.08044	NS	00045	-50,999	454	0.08044	NS	00046	0	0	0.08044	-
I	I		-21,950	309	0.08044	NS		-50,999	357	0.08044	NS		-90,724	1,596	0.08044	43.41
S	S		-2,084	229	0.08044	NS		51	343	0.08044	NS		0	0	0.08044	-
I	I		-2,084	31	0.08044	NS		0	0	0.08044	-		-6,387	539	0.08044	NS



Solette - Verifiche pressoflessione retta allo stato limite di danno

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
P	S	00 05 2	-48,392	255	0.08044	NS	00 05 3	-33,154	2,008	0.08044	32. 19	00 05 5	-101,779	4,240	0.08044	16.55
I			-48,392	941	0.08044	69. 99		0	0	0.08044	-		0	0	0.08044	-
S	S		0	0	0.08044	-		-27,506	1,802	0.08044	35. 61		-81,753	4,434	0.08044	15.46
I			-7,429	2,449	0.08044	25. 54		0	0	0.08044	-		0	0	0.08044	-
P	S	00 13 7	-11,221	829	0.08044	75. 82	00 38 0	16,408	1,007	0.08044	60. 19	00 38 1	-46,562	4,865	0.08044	13.51
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		15,611	98	0.08044	NS		17,088	352	0.08044	NS		-57,795	1,048	0.08044	63.57
I			15,611	1,107	0.08044	54. 81		0	0	0.08044	-		0	0	0.08044	-
P	S	00 38 2	-153,039	11,987	0.08044	6.2 0	00 38 3	-26,795	13,283	0.08044	4.8 3	00 38 4	-12,580	13,004	0.08044	4.84
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-69,888	2,867	0.08044	23. 58		-53,619	2,763	0.08044	23. 99		-29,393	3,611	0.08044	17.81
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 38 5	5,484	13,958	0.08044	4.4 1	00 38 6	21,150	12,335	0.08044	4.8 8	00 38 7	14,117	11,839	0.08044	5.14
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-27,987	2,802	0.08044	22. 92		-28,311	2,660	0.08044	24. 15		-18,230	3,387	0.08044	18.72
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 38 8	17,579	12,675	0.08044	4.7 7	00 38 9	26,718	11,190	0.08044	5.3 4	00 39 0	18,277	10,540	0.08044	5.74
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-17,731	2,585	0.08044	24. 52		-16,562	2,381	0.08044	26. 58		-12,198	3,105	0.08044	20.27
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 39 1	13,183	10,177	0.08044	5.9 8	00 39 2	12,957	10,158	0.08044	5.9 9	00 39 3	16,724	11,166	0.08044	5.43
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-15,949	2,973	0.08044	21. 27		-9,018	2,342	0.08044	26. 76		-11,751	2,320	0.08044	27.11
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 39 4	14,614	9,777	0.08044	6.2 1	00 39 5	16,288	9,719	0.08044	6.2 4	00 39 6	16,120	10,886	0.08044	5.57
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-11,108	2,844	0.08044	22. 10		-7,645	2,305	0.08044	27. 14		-10,035	2,291	0.08044	27.39
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 39 7	14,413	9,556	0.08044	6.3 6	00 39 8	17,519	9,663	0.08044	6.2 6	00 39 9	16,177	11,167	0.08044	5.43
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-9,261	2,748	0.08044	22. 81		-7,752	2,370	0.08044	26. 40		-9,861	2,289	0.08044	27.41
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 40 0	13,432	9,765	0.08044	6.2 3	00 40 1	17,033	10,015	0.08044	6.0 5	00 40 2	16,903	11,699	0.08044	5.18
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-8,780	2,745	0.08044	22. 82		-9,070	2,515	0.08044	24. 92		-11,456	2,376	0.08044	26.46
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 40 3	11,577	10,495	0.08044	5.8 1	00 40 4	14,796	10,777	0.08044	5.6 4	00 40 5	12,874	12,673	0.08044	4.81
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-8,384	2,862	0.08044	21. 88		-12,170	2,743	0.08044	22. 94		-12,833	2,525	0.08044	24.94
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00 40 6	7,112	11,419	0.08044	5.3 7	00 40 7	10,251	11,548	0.08044	5.2 9	00 40 8	6,297	13,183	0.08044	4.66
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-9,888	2,945	0.08044	21. 31		-14,351	3,028	0.08044	20. 84		-13,896	2,628	0.08044	24.00
I			0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00	-3,083	11,525	0.08044	5.4	00	14	10,848	0.08044	5.7	00	-2,236	11,130	0.08044	5.58



## Solette - Verifiche pressoflessione retta allo stato limite di danno

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
	I	409	0	0	0.08044	0	410	0	0	0.08044	1	411	0	0	0.08044	-
S	S		-10,994	2,776	0.08044	22.63		-12,192	2,963	0.08044	21.24		-12,526	2,198	0.08044	28.64
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00412	-20,867	8,305	0.08044	7.66	00413	-19,309	4,986	0.08044	12.74	00414	-29,473	2,126	0.08044	30.26
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-7,539	1,752	0.08044	35.70		-5,503	1,576	0.08044	39.59		-6,221	935	0.08044	66.79
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00416	-130,526	548	0.08044	NS	00417	-22,020	1,479	0.08044	43.09	00418	0	0	0.08044	-
	I		-130,526	453	0.08044	NS		0	0	0.08044	-		-34,592	1,025	0.08044	63.17
S	S		-37,987	1,562	0.08044	41.63		-28,387	83	0.08044	NS		0	0	0.08044	-
	I		0	0	0.08044	-		-28,387	1,062	0.08044	60.49		-6,618	1,998	0.08044	31.27
P	S	00729	0	0	0.08044	-	00730	16,271	889	0.08044	68.19	00731	-2,654	21	0.08044	NS
	I		25,424	1,637	0.08044	36.58		0	0	0.08044	-		-2,654	272	0.08044	NS
S	S		-97,482	2,209	0.08044	31.61		-1,883	167	0.08044	NS		66,724	468	0.08044	NS
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	00732	0	0	0.08044	-	00733	27,464	70	0.08044	NS	00734	26,190	79	0.08044	NS
	I		39,689	351	0.08044	NS		27,464	65	0.08044	NS		26,190	95	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		17,396	243	0.08044	NS		6,888	37	0.08044	NS		6,338	61	0.08044	NS
P	S	00735	24,205	116	0.08044	NS	00736	21,760	116	0.08044	NS	00737	17,260	182	0.08044	NS
	I		24,205	57	0.08044	NS		21,760	134	0.08044	NS		17,260	98	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		6,910	45	0.08044	NS		5,997	35	0.08044	NS		6,677	22	0.08044	NS
P	S	00738	10,632	95	0.08044	NS	00739	1,101	88	0.08044	NS	00740	-10,033	58	0.08044	NS
	I		10,632	178	0.08044	NS		1,101	139	0.08044	NS		-10,033	207	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		7,591	54	0.08044	NS		7,043	42	0.08044	NS		7,026	55	0.08044	NS
P	S	00741	-25,743	31	0.08044	NS	00742	0	0	0.08044	-	00743	0	0	0.08044	-
	I		-25,743	318	0.08044	NS		-43,010	414	0.08044	NS		-60,550	374	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		8,440	65	0.08044	NS		9,567	63	0.08044	NS		6,734	52	0.08044	NS
P	S	00744	0	0	0.08044	-	00745	0	0	0.08044	-	00746	-4,230	51	0.08044	NS
	I		-81,783	522	0.08044	NS		-136,129	1,095	0.08044	66.60		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		-94,095	207	0.08044	NS
	I		7,684	157	0.08044	NS		-14,856	369	0.08044	NS		-94,095	154	0.08044	NS
P	S	00747	14,860	91	0.08044	NS	00748	0	0	0.08044	-	00749	123,556	7,643	0.08044	6.79
	I		14,860	52	0.08044	NS		16,536	928	0.08044	65.30		0	0	0.08044	-
S	S		0	0	0.08044	-		-3,320	205	0.08044	NS		0	0	0.08044	-
	I		-47,525	446	0.08044	NS		-3,320	375	0.08044	NS		45,392	146	0.08044	NS
P	S	00750	103,967	3,334	0.08044	16.04	00751	0	0	0.08044	-	00752	0	0	0.08044	-
	I		0	0	0.08044	-		52,562	323	0.08044	NS		39,182	2,932	0.08044	20.04
S	S		0	0	0.08044	-		6,620	434	0.08044	NS		0	0	0.08044	-
	I		22,616	391	0.08044	NS		0	0	0.08044	-		1,754	898	0.08044	68.82
P	S	00753	0	0	0.08044	-	00754	0	0	0.08044	-	00755	0	0	0.08044	-
	I		37,277	5,713	0.08044	10.31		14,820	7,194	0.08044	8.44		17,173	8,194	0.08044	7.39
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		5,227	264	0.08044	NS		3,794	885	0.08044	69.		5,308	356	0.08044	NS



## Solette - Verifiche pressoflessione retta allo stato limite di danno

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
											64					
P	S	00756	0	0	0.08044	-	00757	0	0	0.08044	-	00758	0	0	0.08044	-
	I		-11,524	8,350	0.08044	7.53		-12,683	7,698	0.08044	8.18		-22,222	6,480	0.08044	9.84
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-3,049	305	0.08044	NS		1,278	848	0.08044	72.92		1,483	172	0.08044	NS
P	S	00759	0	0	0.08044	-	00760	0	0	0.08044	-	00761	-89,133	2,850	0.08044	24.26
	I		-51,424	4,493	0.08044	14.71		-40,158	2,237	0.08044	29.14		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-7,674	682	0.08044	91.74		-7,296	160	0.08044	NS		-25,798	285	0.08044	NS
P	S	00762	-124,356	7,179	0.08044	10.03	00963	12,582	187	0.08044	NS	00965	5,405	279	0.08044	NS
	I		0	0	0.08044	-		12,582	212	0.08044	NS		5,405	299	0.08044	NS
S	S		-70,642	193	0.08044	NS		-3,644	119	0.08044	NS		-2,801	159	0.08044	NS
	I		-70,642	306	0.08044	NS		-3,644	45	0.08044	NS		-2,801	79	0.08044	NS
P	S	00966	0	0	0.08044	-	00968	5,663	38	0.08044	NS	00971	-10,846	314	0.08044	NS
	I		21,468	840	0.08044	71.67		14,358	277	0.08044	NS		-11,587	199	0.08044	NS
S	S		0	0	0.08044	-		-3,795	88	0.08044	NS		-2,063	202	0.08044	NS
	I		8,852	1,287	0.08044	47.57		-3,795	59	0.08044	NS		0	0	0.08044	-
P	S	00973	-35,493	322	0.08044	NS	00975	-67,165	170	0.08044	NS	01030	-13,450	2,332	0.08044	27.03
	I		-35,493	467	0.08044	NS		-67,165	503	0.08044	NS		0	0	0.08044	-
S	S		-1,736	237	0.08044	NS		-1,086	264	0.08044	NS		-3,409	7,875	0.08044	7.90
	I		-1,736	69	0.08044	NS		0	0	0.08044	-		0	0	0.08044	-
P	S	01032	-23,897	1,134	0.08044	56.33	01033	-2,638	1,780	0.08044	34.92	01036	-10,626	2,576	0.08044	24.38
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-16,900	5,058	0.08044	12.52		-8,451	8,393	0.08044	7.46		-11,131	9,137	0.08044	6.88
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01037	-21,875	107	0.08044	NS	01040	-9,755	1,428	0.08044	43.93	01059	-3,793	17,482	0.08044	3.56
	I		-21,875	431	0.08044	NS		0	0	0.08044	-		0	0	0.08044	-
S	S		-9,232	1,573	0.08044	39.85		-12,362	6,132	0.08044	10.26		-23,076	3,477	0.08044	18.35
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01061	-3,307	16,856	0.08044	3.69	01062	-5,725	18,093	0.08044	3.45	01064	-3,773	17,511	0.08044	3.55
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-21,048	4,155	0.08044	15.32		-20,902	3,574	0.08044	17.81		-15,702	3,317	0.08044	19.06
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01067	-3,833	16,850	0.08044	3.69	01069	-6,801	17,862	0.08044	3.50	01071	1,562	16,322	0.08044	3.79
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-20,846	4,186	0.08044	15.20		-19,734	3,540	0.08044	17.95		-20,161	3,565	0.08044	17.83
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01072	-4,597	17,386	0.08044	3.58	01075	-4,484	17,366	0.08044	3.59	01077	-15,860	15,481	0.08044	4.08
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-21,757	3,419	0.08044	18.63		-15,478	3,307	0.08044	19.11		-8,262	3,185	0.08044	19.66
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01079	-14,206	15,223	0.08044	4.14	01080	72,154	12,477	0.08044	4.49	01082	13,031	13,929	0.08044	4.37
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-7,838	2,994	0.08044	20.90		28,731	3,286	0.08044	18.14		3,871	3,208	0.08044	19.21
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01	-9,714	15,566	0.08044	4.0	01	-10,366	16,670	0.08044	3.7	01	2,105	16,599	0.08044	3.72



## Solette - Verifiche pressoflessione retta allo stato limite di danno

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
	I	085	0	0	0.08044	-	087	0	0	0.08044	-	089	0	0	0.08044	-
S	S		-14,960	3,129	0.08044	20.18		-20,515	3,359	0.08044	18.94		-21,214	3,613	0.08044	17.62
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01090	-11,668	15,334	0.08044	4.10	01093	-6,227	15,724	0.08044	3.97	01095	-11,595	14,649	0.08044	4.29
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-9,658	3,912	0.08044	16.03		-20,807	3,924	0.08044	16.22		-9,061	3,892	0.08044	16.10
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01097	-3,664	14,304	0.08044	4.35	01098	-10,933	16,367	0.08044	3.84	01101	-4,246	15,207	0.08044	4.10
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-11,003	2,788	0.08044	22.54		-18,813	3,355	0.08044	18.92		-18,693	3,736	0.08044	16.99
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01103	-5,486	12,962	0.08044	4.81	01105	-19,194	4,527	0.08044	14.03	01106	-8,961	11,728	0.08044	5.34
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
S	S		-5,706	2,647	0.08044	23.58		-24,764	1,184	0.08044	54.01		-9,160	2,380	0.08044	26.34
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01109	2,425	8,030	0.08044	7.69	01111	-37,131	93	0.08044	NS	01113	30,700	3,993	0.08044	14.89
	I		0	0	0.08044	-		-37,131	1,071	0.08044	60.65		0	0	0.08044	-
S	S		-18,181	1,637	0.08044	38.74		0	0	0.08044	-		7,641	262	0.08044	NS
	I		0	0	0.08044	-		-97,038	1,951	0.08044	35.77		7,641	750	0.08044	81.76
P	S	01547	-31,025	219	0.08044	NS	01548	-38,136	285	0.08044	NS	01549	-23,956	1,142	0.08044	55.94
	I		-31,025	44	0.08044	NS		-38,136	22	0.08044	NS		0	0	0.08044	-
S	S		-31,004	63	0.08044	NS		-10,010	38	0.08044	NS		-11,586	522	0.08044	NS
	I		-31,004	104	0.08044	NS		-10,010	630	0.08044	99.61		0	0	0.08044	-
P	S	01550	0	0	0.08044	-	01551	0	0	0.08044	-	01552	0	0	0.08044	-
	I		-21,239	1,012	0.08044	62.91		-19,831	1,390	0.08044	45.72		-21,918	1,468	0.08044	43.41
S	S		-11,193	954	0.08044	65.88		-12,512	1,665	0.08044	37.81		-11,277	1,463	0.08044	42.96
	I		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
P	S	01553	0	0	0.08044	-	01554	-17,434	1,189	0.08044	53.29	01555	-10,821	227	0.08044	NS
	I		-26,615	898	0.08044	71.38		0	0	0.08044	-		-10,821	423	0.08044	NS
S	S		-14,595	573	0.08044	NS		-25,724	46	0.08044	NS		0	0	0.08044	-
	I		0	0	0.08044	-		-25,724	93	0.08044	NS		-11,180	555	0.08044	NS
P	S	01556	0	0	0.08044	-	01557	0	0	0.08044	-	01558	0	0	0.08044	-
	I		-13,075	3,172	0.08044	19.86		-14,978	3,719	0.08044	16.98		-15,669	2,765	0.08044	22.86
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-12,789	1,631	0.08044	38.61		-13,446	2,002	0.08044	31.48		-15,303	1,660	0.08044	38.06
P	S	01559	-12,709	382	0.08044	NS	01560	-1,530	4,712	0.08044	13.17	01561	0	0	0.08044	-
	I		0	0	0.08044	-		0	0	0.08044	-		-6,641	3,248	0.08044	19.24
S	S		0	0	0.08044	-		-11,360	683	0.08044	92.04		0	0	0.08044	-
	I		-20,394	789	0.08044	80.60		0	0	0.08044	-		-14,914	1,651	0.08044	38.25
P	S	01562	0	0	0.08044	-	01563	0	0	0.08044	-	01564	0	0	0.08044	-
	I		-8,472	5,578	0.08044	11.23		-9,586	5,131	0.08044	12.22		-9,159	1,998	0.08044	31.37
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-



Solette - Verifiche pressoflessione retta allo stato limite di danno

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
	I		-15,183	2,737	0.08044	23.08		-16,481	2,702	0.08044	23.42		-17,820	1,505	0.08044	42.12
P	S	01565	-9,277	5,313	0.08044	11.80	01566	1,145	781	0.08044	79.19	01567	0	0	0.08044	-
	I		0	0	0.08044	-		1,145	958	0.08044	64.56		-2,899	5,982	0.08044	10.39
S	S		-18,2320	6330	0.080440.08044	NS-		0-15,425	0858	0.080440.08044	-73.65		0-17,257	02,379	0.080440.08044	-26.63
P	S	01568	0	0	0.08044	-	01569	0	0	0.08044	-	01570	-7,266	1,809	0.08044	34.57
	I		-4,745	7,023	0.08044	8.87		-5,668	4,618	0.08044	13.51		0	0	0.08044	-
S	S		0-17,375	02,828	0.080440.08044	-22.40		0-19,527	02,140	0.080440.08044	-29.68		0-17,427	0764	0.080440.08044	-82.93
P	S	01571	8,190	5,847	0.08044	10.48	01572	0	0	0.08044	-	01573	0	0	0.08044	-
	I		0	0	0.08044	-		2,092	4,790	0.08044	12.90		-521	7,891	0.08044	7.86
S	S		-15,044	752	0.08044	83.99		0	0	0.08044	-		0	0	0.08044	-
	I		0	0	0.08044	-		-17,102	1,664	0.08044	38.06		-19,050	2,592	0.08044	24.49
P	S	01574	0	0	0.08044	-	01575	0	0	0.08044	-	01576	-7,599	8,058	0.08044	7.76
	I		-2,557	6,975	0.08044	8.91		-4,440	2,129	0.08044	29.26		0	0	0.08044	-
S	S		0-18,680	02,341	0.080440.08044	-27.11		0-19,015	0995	0.080440.08044	-63.80		-16,8080	1,0290	0.080440.08044	61.52-
P	S	01577	7,460	660	0.08044	92.93	01578	0	0	0.08044	-	01579	0	0	0.08044	-
	I		7,460	2,021	0.08044	30.35		3,350	7,536	0.08044	8.18		531	8,508	0.08044	7.28
S	S		0-15,949	0992	0.080440.08044	-63.75		0-18,349	02,196	0.080440.08044	-28.88		0-20,263	02,494	0.080440.08044	-25.50
P	S	01580	0	0	0.08044	-	01581	-5,623	2,881	0.08044	21.66	01582	11,400	5,508	0.08044	11.08
	I		-2,168	5,214	0.08044	11.91		0	0	0.08044	-		0	0	0.08044	-
S	S		0-19,244	01,647	0.080440.08044	-38.56		0-18,189	0517	0.080440.08044	-NS		-14,715-14,715	679108	0.080440.08044	92.98NS
P	S	01583	0	0	0.08044	-	01584	0	0	0.08044	-	01585	0	0	0.08044	-
	I		6,759	5,996	0.08044	10.24		3,507	9,045	0.08044	6.82		349	7,664	0.08044	8.08
S	S		0-17,185	01,688	0.080440.08044	-37.52		0-19,483	02,372	0.080440.08044	-26.78		0-21,002	02,043	0.080440.08044	-31.15
P	S	01586	0	0	0.08044	-	01587	-5,034	9,371	0.08044	6.65	01588	10,253	194	0.08044	NS
	I		-2,793	1,973	0.08044	31.51		0	0	0.08044	-		10,253	3,181	0.08044	19.21
S	S		0	0	0.08044	-		-19,478	1,315	0.08044	48.31		0	0	0.08044	-
	I		-20,480	742	0.08044	85.72		0	0	0.08044	-		-15,413	1,194	0.08044	52.92
P	S	01589	0	0	0.08044	-	01590	0	0	0.08044	-	01591	0	0	0.08044	-
	I		6,276	8,511	0.08044	7.22		2,855	9,176	0.08044	6.73		-603	5,323	0.08044	11.65
S	S		0-18,247	02,167	0.080440.08044	-29.27		0-20,594	02,283	0.080440.08044	-27.86		0-21,233	01,395	0.080440.08044	-45.64
P	S	01592	-4,310	3,380	0.08044	18.43	01593	12,521	4,864	0.08044	12.53	01594	0	0	0.08044	-
	I		0	0	0.08044	-		0	0	0.08044	-		8,762	6,906	0.08044	8.87



## Solette - Verifiche pressoflessione retta allo stato limite di danno

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
S	S		-20,974	77	0.08044	NS		-13,823	556	0.08044	NS		0	0	0.08044	-
	I		-20,974	141	0.08044	NS		-13,823	359	0.08044	NS		-16,608	1,813	0.08044	34.91
P	S	01 59 5	0	0	0.08044	-	01 59 6	0	0	0.08044	-	01 59 7	0	0	0.08044	-
	I		5,271	9,691	0.08044	6.3 5		1,729	7,944	0.08044	7.7 8		-1,803	1,846	0.08044	33.63
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-19,477	2,345	0.08044	27. 09		-21,470	1,907	0.08044	33. 39		-21,752	587	0.08044	NS
P	S	01 59 8	-5,893	10,047	0.08044	6.2 1	01 59 9	0	0	0.08044	-	01 60 0	0	0	0.08044	-
	I		0	0	0.08044	-		11,377	4,026	0.08044	15. 16		7,509	9,124	0.08044	6.72
S	S		-22,387	1,489	0.08044	42. 82		0	0	0.08044	-		0	0	0.08044	-
	I		0	0	0.08044	-		-14,635	1,352	0.08044	46. 69		-17,995	2,255	0.08044	28.12
P	S	01 60 1	0	0	0.08044	-	01 60 2	0	0	0.08044	-	01 60 3	-3,614	3,837	0.08044	16.22
	I		3,956	9,532	0.08044	6.4 6		413	5,368	0.08044	11. 53		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-20,840	2,289	0.08044	27. 80		-21,959	1,377	0.08044	46. 28		-22,085	338	0.08044	NS
P	S	01 60 4	13,247	4,428	0.08044	13. 75	01 60 5	0	0	0.08044	-	01 60 6	0	0	0.08044	-
	I		13,247	122	0.08044	NS		9,578	7,435	0.08044	8.2 3		6,049	10,042	0.08044	6.12
S	S		-12,992	501	0.08044	NS		0	0	0.08044	-		0	0	0.08044	-
	I		-12,992	462	0.08044	NS		-16,287	1,912	0.08044	33. 09		-19,506	2,404	0.08044	26.42
P	S	01 60 7	0	0	0.08044	-	01 60 8	0	0	0.08044	-	01 60 9	-3,813	10,373	0.08044	6.00
	I		2,493	8,101	0.08044	7.6 2		-900	1,805	0.08044	34. 36		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		-23,524	1,463	0.08044	43.64
	I		-21,780	1,925	0.08044	33. 10		-22,575	574	0.08044	NS		0	0	0.08044	-
P	S	01 61 0	0	0	0.08044	-	01 61 1	0	0	0.08044	-	01 61 2	0	0	0.08044	-
	I		12,053	4,404	0.08044	13. 84		8,036	9,393	0.08044	6.5 3		4,447	9,692	0.08044	6.35
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-14,329	1,406	0.08044	44. 88		-17,943	2,307	0.08044	27. 48		-20,977	2,321	0.08044	27.42
P	S	01 61 3	0	0	0.08044	-	01 61 4	-2,530	3,968	0.08044	15. 66	01 61 5	14,138	4,332	0.08044	14.03
	I		950	5,412	0.08044	11. 43		0	0	0.08044	-		14,138	261	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		-12,993	473	0.08044	NS
	I		-22,249	1,390	0.08044	45. 86		-22,920	370	0.08044	NS		-12,993	505	0.08044	NS
P	S	01 61 6	0	0	0.08044	-	01 61 7	0	0	0.08044	-	01 61 8	0	0	0.08044	-
	I		9,980	7,544	0.08044	8.1 0		6,315	10,120	0.08044	6.0 7		2,690	8,145	0.08044	7.58
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-16,327	1,937	0.08044	32. 66		-19,535	2,417	0.08044	26. 28		-21,725	1,928	0.08044	33.04
P	S	01 61 9	0	0	0.08044	-	01 62 0	-3,308	10,434	0.08044	5.9 6	01 62 1	0	0	0.08044	-
	I		-615	1,802	0.08044	34. 40		0	0	0.08044	-		12,762	4,286	0.08044	14.21
S	S		0	0	0.08044	-		-23,686	1,478	0.08044	43. 21		0	0	0.08044	-
	I		-22,634	569	0.08044	NS		0	0	0.08044	-		-14,595	1,379	0.08044	45.78
P	S	01 62 2	0	0	0.08044	-	01 62 3	0	0	0.08044	-	01 62 4	0	0	0.08044	-
	I		8,179	9,309	0.08044	6.5 8		4,305	9,654	0.08044	6.3 8		694	5,413	0.08044	11.43



## Solette - Verifiche pressoflessione retta allo stato limite di danno

D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]			[N]	[N-m]	[cm <sup>2</sup> /cm]	
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-18,033	2,286	0.08044	27.74		-20,734	2,299	0.08044	27.67		-21,823	1,369	0.08044	46.54
P	S	01625	-2,942	3,906	0.08044	15.92	01626	16,077	4,593	0.08044	13.20	01627	0	0	0.08044	-
	I		0	0	0.08044	-		0	0	0.08044	-		10,145	7,220	0.08044	8.47
S	S		0	0	0.08044	-		-13,838	536	0.08044	NS		0	0	0.08044	-
	I		-22,390	341	0.08044	NS		-13,838	413	0.08044	NS		-16,890	1,859	0.08044	34.06
P	S	01628	0	0	0.08044	-	01629	0	0	0.08044	-	01630	0	0	0.08044	-
	I		5,906	9,927	0.08044	6.19		1,830	8,071	0.08044	7.66		-1,624	1,830	0.08044	33.92
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-19,318	2,354	0.08044	26.98		-20,834	1,890	0.08044	33.67		-21,504	563	0.08044	NS
P	S	01631	-4,716	10,220	0.08044	6.10	01632	13,598	39	0.08044	NS	01633	0	0	0.08044	-
	I		0	0	0.08044	-		13,598	3,609	0.08044	16.86		7,659	8,887	0.08044	6.90
S	S		-22,851	1,526	0.08044	41.81		0	0	0.08044	-		0	0	0.08044	-
	I		0	0	0.08044	-		-15,991	1,248	0.08044	50.67		-18,363	2,161	0.08044	29.35
P	S	01634	0	0	0.08044	-	01635	0	0	0.08044	-	01636	-4,272	3,545	0.08044	17.57
	I		2,897	9,439	0.08044	6.54		-1,235	5,399	0.08044	11.49		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		-20,852	132	0.08044	NS
	I		-19,624	2,219	0.08044	28.63		-19,915	1,311	0.08044	48.48		-20,852	114	0.08044	NS
P	S	01637	15,285	5,472	0.08044	11.09	01638	0	0	0.08044	-	01639	0	0	0.08044	-
	I		0	0	0.08044	-		9,603	6,494	0.08044	9.42		4,106	9,490	0.08044	6.49
S	S		-17,402	783	0.08044	80.91		0	0	0.08044	-		0	0	0.08044	-
	I		-17,402	72	0.08044	NS		-18,454	1,654	0.08044	38.35		-18,598	2,219	0.08044	28.59
P	S	01640	0	0	0.08044	-	01641	0	0	0.08044	-	01642	-5,178	9,732	0.08044	6.41
	I		-1,033	7,921	0.08044	7.83		-4,725	1,918	0.08044	32.50		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		-19,947	1,374	0.08044	46.26
	I		-18,194	1,823	0.08044	34.79		-18,225	575	0.08044	NS		0	0	0.08044	-
P	S	01643	11,400	641	0.08044	95.19	01644	0	0	0.08044	-	01645	0	0	0.08044	-
	I		11,400	2,432	0.08044	25.09		5,496	8,158	0.08044	7.54		-674	9,080	0.08044	6.83
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-20,153	942	0.08044	67.49		-19,081	1,946	0.08044	32.63		-16,625	2,079	0.08044	30.44
P	S	01646	0	0	0.08044	-	01647	-8,388	3,290	0.08044	19.03	01648	11,055	5,992	0.08044	10.19
	I		-5,706	5,397	0.08044	11.56		0	0	0.08044	-		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		-23,649	907	0.08044	70.41
	I		-14,904	1,295	0.08044	48.77		-16,119	380	0.08044	NS		0	0	0.08044	-
P	S	01649	0	0	0.08044	-	01650	0	0	0.08044	-	01651	0	0	0.08044	-
	I		6,413	5,408	0.08044	11.36		-359	8,867	0.08044	6.99		-5,932	7,720	0.08044	8.09
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-21,687	1,330	0.08044	47.90		-16,612	1,981	0.08044	31.95		-11,686	1,702	0.08044	36.95
P	S	01652	0	0	0.08044	-	01653	-11,642	9,060	0.08044	6.94	01654	4,580	1,261	0.08044	48.83
	I		-10,181	2,072	0.08044	30.29		0	0	0.08044	-		4,580	928	0.08044	66.35



Solette - Verifiche pressoflessione retta allo stato limite di danno																
D	P	No do	N	M	Af	CS	No do	N	M	Af	CS	No do	N	M	Af	CS
			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]			[N]	[N-m]	[cm²/cm]	
S	S		0	0	0.08044	-		-14,398	1,259	0.08044	50.13		0	0	0.08044	-
	I		-9,996	561	0.08044	NS		0	0	0.08044	-		-27,656	561	0.08044	NS
P	S	01655	0	0	0.08044	-	01656	0	0	0.08044	-	01657	0	0	0.08044	-
	I		-2,146	7,233	0.08044	8.59		-6,011	8,646	0.08044	7.22		-8,912	5,397	0.08044	11.61
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-18,920	1,585	0.08044	40.05		-10,366	1,845	0.08044	34.03		-4,051	1,232	0.08044	50.54
P	S	01658	-13,279	2,819	0.08044	22.36	01659	-3,180	6,835	0.08044	9.10	01660	0	0	0.08044	-
	I		0	0	0.08044	-		0	0	0.08044	-		-11,007	4,115	0.08044	15.27
S	S		0	0	0.08044	-		-35,650	1,129	0.08044	57.42		0	0	0.08044	-
	I		-4,433	359	0.08044	NS		0	0	0.08044	-		-22,378	864	0.08044	73.79
P	S	01661	0	0	0.08044	-	01662	0	0	0.08044	-	01663	0	0	0.08044	-
	I		-10,085	8,188	0.08044	7.66		-5,123	7,470	0.08044	8.35		-3,697	2,203	0.08044	28.25
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-10,083	1,571	0.08044	39.95		-2,467	1,487	0.08044	41.79		4,489	561	0.08044	NS
P	S	01664	-11,947	8,274	0.08044	7.60	01665	-46,608	2,053	0.08044	32.01	01666	0	0	0.08044	-
	I		0	0	0.08044	-		0	0	0.08044	-		-30,704	6,251	0.08044	10.31
S	S		2,167	1,227	0.08044	50.34		-29,525	10	0.08044	NS		0	0	0.08044	-
	I		0	0	0.08044	-		-29,525	181	0.08044	NS		-6,159	986	0.08044	63.33
P	S	01667	0	0	0.08044	-	01668	0	0	0.08044	-	01669	27,402	2,238	0.08044	26.68
	I		-4,537	8,319	0.08044	7.49		12,898	5,473	0.08044	11.13		0	0	0.08044	-
S	S		0	0	0.08044	-		0	0	0.08044	-		0	0	0.08044	-
	I		-1,923	1,296	0.08044	47.92		3,002	958	0.08044	64.40		16,979	575	0.08044	NS
P	S	02515	-148,207	10,761	0.08044	6.87	02516	0	0	0.08044	-	02517	-126,312	420	0.08044	NS
	I		0	0	0.08044	-		37,048	477	0.08044	NS		-126,312	63	0.08044	NS
S	S		0	0	0.08044	-		0	0	0.08044	-		-111,814	821	0.08044	86.45
	I		-115,523	612	0.08044	NS		50,236	1,234	0.08044	46.89		0	0	0.08044	-
P	S	02518	140,717	9,606	0.08044	5.26										
	I		0	0	0.08044	-										
S	S		37,319	1,189	0.08044	49.55										
	I		0	0	0.08044	-										

LEGENDA Solette - Verifiche pressoflessione retta allo stato limite di danno

**D** Direzione [P] = principale - [S] = secondaria.  
**P** Posizione [S] = superiore - [I] = inferiore.  
**N, M** Coppia N-M che dà origine alla massima armatura.  
**Af** Area delle armature per centimetro.  
**CS** Coefficienti di sicurezza: [NS] = Non Significativo - Per valori di CS maggiori o uguali a 100.

SOLETTE - VERIFICHE PRESSOFLESSIONE RETTA ALLO STATO LIMITE DI ESERCIZIO (Elevazione)

Solette - Verifiche pressoflessione retta allo stato limite di esercizio																
D	NO DO	σ ct	σ cc	σ at	NO DO	σ ct	σ cc	σ at	NO DO	σ ct	σ cc	σ at	NO DO	σ ct	σ cc	σ at
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
Soletta P1-P2-P5-P4				AA= PCA		CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
Piano Terra						SolettaP1-P2-P5-P4										
SHELL: [00052-01438-00414]AA= PCA						CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00947-00101-01442]AA= PCA						CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01493-00922-00923]AA= PCA						CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00052-00094-01438]AA= PCA						CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										



## Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00414-01438-00413]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00413-01438-01444]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00657-01535-00658]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00413-01444-01448]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01440-00128-00415]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00412-01448-00411]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01493-00921-00922]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00411-01452-00410]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01457-00108-00932]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00411-01448-01452]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00645-00644-01508]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00410-01456-00409]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01440-00415-00054]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00410-01452-01456]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00102-00051-01439]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00409-01456-01461]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00409-01461-00408]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00408-01461-00407]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01043-00664-00061]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00406-01465-01470]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00406-01470-00405]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00405-01470-00404]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01493-00116-00921]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00404-01470-01474]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01484-00917-00115]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00403-01479-00402]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01502-00898-00118]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00403-01474-01479]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00101-00948-01441]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00402-01479-00401]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01502-00118-00896]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00401-01479-01483]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01502-00117-00898]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00400-01483-01488]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01543-01440-01052]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00400-01488-00399]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01511-00120-00901]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00398-01488-01492]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00397-01492-01497]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00397-01497-00396]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										



## Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01511-00902-00120]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00395-01501-00394]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00395-01497-01501]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00394-01506-00393]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01525-01520-00123]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00394-01501-01506]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01525-00123-00944]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00392-01510-00391]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01520-00894-00122]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00391-01515-00390]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01520-00122-00892]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00391-01510-01515]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00948-00102-01441]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00390-01515-01519]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01520-00892-00123]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00389-01519-00388]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00063-01543-01052]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00388-01524-00387]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01529-00124-00940]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00388-01519-01524]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01529-00940-00125]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00387-01524-01528]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01538-00127-00891]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00386-01528-01533]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00099-00957-02511]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00386-01533-00385]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01538-00943-00127]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00384-01533-01537]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01538-00126-00943]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00384-01537-00383]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01543-00128-01440]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00383-01537-01542]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00383-01542-00382]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00382-01542-00381]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00064-01440-00054]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00381-01542-01546]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01462-01457-00932]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00380-01546-01437]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00623-01467-00624]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00380-01437-00137]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										



## Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00407-01461-01465]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00407-01465-00406]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01461-01456-01460]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01461-01460-01465]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01466-00109-00930]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01470-01465-01469]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01462-00932-00109]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01470-01469-01474]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01439-00914-00103]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00393-01506-01510]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01479-01474-01478]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01479-01478-01483]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01439-00051-00914]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01488-01483-01487]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01488-01487-01492]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01437-01546-00056]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00393-01510-00392]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01497-01492-01496]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01497-01496-01501]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01506-01501-01505]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01453-01449-00106]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01543-01538-00891]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01529-00125-00939]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01441-00912-00104]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01534-01529-00939]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01534-00126-01538]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01511-00119-00902]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01544-01539-01543]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00057-01545-01056]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01507-00119-01511]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01506-01505-01510]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01475-00113-00918]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01484-00114-00917]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01484-00115-00924]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00623-00622-01467]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00387-01528-00386]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01525-00124-01529]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01489-01484-00924]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01475-00935-00112]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01475-00928-00113]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										



## Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01516-00894-01520]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01475-00112-00928]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01466-00936-00111]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01515-01514-01519]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01480-00114-01484]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01466-00930-00110]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01466-00110-00936]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01544-01051-00062]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01498-00117-01502]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01457-00909-00108]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01457-00107-00909]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01449-00904-00106]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01453-00106-00910]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01449-00906-00105]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01449-00105-00904]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01441-00102-01439]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01441-00103-00912]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01441-01439-00103]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01052-01440-00064]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00061-02512-01044]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01543-00891-00128]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01534-00939-00126]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01525-00944-00124]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00100-00947-01442]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01516-00901-00121]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01516-01511-00901]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01516-00121-00894]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01507-01502-00896]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01507-00896-00119]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01498-01493-00923]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01498-00923-00117]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01489-00116-01493]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01489-00924-00116]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01480-00918-00114]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01480-01475-00918]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01471-01466-00111]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01471-00111-00935]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01471-00935-01475]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01462-00109-01466]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00381-01546-00380]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										



## Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00641-00640-01499]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01453-00910-00107]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01453-00107-01457]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01445-01441-00104]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01445-00104-00906]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01445-00906-01449]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01533-01532-01537]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00664-02512-00061]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01539-01538-01543]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01539-01534-01538]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01530-01525-01529]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01530-01529-01534]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01521-01520-01525]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01521-01516-01520]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01051-01543-00063]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01512-01511-01516]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01512-01507-01511]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01503-01502-01507]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01503-01498-01502]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01494-01493-01498]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01494-01489-01493]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01485-01484-01489]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01485-01480-01484]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01476-01475-01480]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01476-01471-01475]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01467-01466-01471]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01467-01462-01466]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00654-00653-01526]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01458-01457-01462]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01458-01453-01457]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00654-01526-00655]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01450-01449-01453]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01450-01445-01449]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01442-01441-01445]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01442-00101-01441]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01437-00056-00379]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01544-01543-01051]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00645-01508-00646]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01499-01494-01498]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01535-01534-01539]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										



## Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01535-01530-01534]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01526-01521-01525]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01526-01525-01530]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01517-01512-01516]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01517-01516-01521]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01508-01503-01507]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01508-01507-01512]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01499-01498-01503]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01490-01489-01494]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01490-01485-01489]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00635-00634-01490]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01481-01480-01485]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01481-01476-01480]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01472-01471-01476]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01472-01467-01471]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01463-01462-01467]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01463-01458-01462]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00665-00664-01043]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01454-01450-01453]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01454-01453-01458]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01446-01445-01450]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01446-01442-01445]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00413-01448-00412]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00641-01503-00642]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00643-00642-01503]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00643-01503-01508]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00641-01499-01503]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00633-00632-01485]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00644-00643-01508]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00724-00961-00725]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00646-01508-01512]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00637-00636-01494]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00647-00646-01512]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00637-01494-00638]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00725-00098-00726]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01451-00718-00717]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00653-00652-01526]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00633-01490-00634]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00631-00630-01481]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00958-00097-02514]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										



Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00633-01485-01490]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00098-00955-00726]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00396-01497-00395]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00639-00638-01499]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00638-01494-01499]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00639-01499-00640]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00636-00635-01490]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00636-01490-01494]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00648-00647-01512]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00648-01512-01517]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00660-01535-01539]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00661-01539-00662]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00661-00660-01539]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00659-01535-00660]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00662-01539-01544]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00650-00649-01517]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00624-01472-00625]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00728-00099-02511]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00655-01526-01530]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00655-01530-00656]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00657-00656-01530]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00658-01535-00659]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00657-01530-01535]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00649-00648-01517]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00663-01544-02512]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00652-01521-01526]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00652-00651-01521]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00663-00662-01544]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00650-01517-01521]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00650-01521-00651]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [02512-01544-00062]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [02512-00062-01044]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00624-01467-01472]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00625-01472-00626]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00617-00616-01454]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00614-01450-00615]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00667-00666-00060]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00617-01458-00618]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00615-01454-00616]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00615-01450-01454]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										



Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00666-00665-00060]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00611-01446-00612]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00619-01458-01463]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00611-00610-01446]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01542-01541-01546]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00618-01458-00619]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00617-01454-01458]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [02511-00100-01442]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [02511-00957-00100]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00610-01442-01446]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00609-01442-00610]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00609-02511-01442]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00613-01450-00614]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00612-01446-01450]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00612-01450-00613]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00727-00099-00728]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00627-01476-00628]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00627-01472-01476]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00629-00628-01476]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00626-01472-00627]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00629-01476-01481]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01542-01537-01541]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00631-01481-01485]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00631-01485-00632]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00629-01481-00630]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00620-01463-00621]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00622-01463-01467]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00620-00619-01463]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00621-01463-00622]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01513-00685-00684]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01504-00691-00690]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00955-00099-00727]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01527-01522-00679]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00404-01474-00403]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01451-00720-00719]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00059-00668-01048]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01522-00682-00681]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01056-01545-00058]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00060-00665-01043]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01448-01444-01447]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										



D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01448-01447-01452]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00726-00955-00727]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00401-01483-00400]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00097-00961-00724]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01456-01452-01455]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00961-00098-00725]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01048-00667-00060]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01456-01455-01460]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01540-00671-00670]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00056-01546-01055]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01465-01460-01464]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01047-02513-00059]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00668-00667-01048]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01459-00713-00712]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01465-01464-01469]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01540-00672-00671]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01486-00700-00699]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01491-00696-01495]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01545-02513-00058]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [02514-00097-00724]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01474-01473-0147																



## Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00385-01533-00384]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01495-00694-00693]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01486-00701-00700]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01509-00687-01513]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01509-00688-00687]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01522-00680-00679]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01447-00720-01451]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01444-01443-01447]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01536-00675-00674]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01513-00687-00686]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01500-01495-00693]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00096-00958-01443]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01492-01487-01491]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01531-00676-00675]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01501-01496-01500]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01536-00674-00673]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01546-00057-01055]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01501-01500-01505]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01504-00690-00689]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01500-00693-00692]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01495-00695-00694]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01486-00699-00698]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01491-00697-00696]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01477-00705-00704]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01477-00704-00703]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01532-01527-01531]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01491-01486-00698]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01510-01505-01509]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01528-01523-01527]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01509-01504-00689]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01468-00710-00709]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01468-00709-00708]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01528-01527-01532]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01524-01519-01523]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01459-00714-00713]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01473-00706-01477]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01459-00715-00714]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01510-01509-01514]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01451-00719-00718]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01464-01459-00712]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										



Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01464-00712-00711]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01455-01451-00717]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01443-00723-00722]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01443-02514-00723]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01443-00958-02514]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01519-01518-01523]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00058-02513-01047]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01536-00673-00672]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01536-00672-01540]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01527-00677-01531]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01527-00678-00677]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01518-01513-00684]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01518-00684-00683]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01509-00689-00688]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01537-01532-01536]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01500-00692-00691]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01500-00691-01504]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01491-00698-00697]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01519-01514-01518]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01482-01477-00703]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01482-00703-00702]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01482-00702-00701]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01482-00701-01486]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01473-00708-00707]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01473-01468-00708]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01473-00707-00706]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01464-00711-00710]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01464-00710-01468]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01455-00716-00715]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01455-00715-01459]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01455-00717-00716]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01447-00722-00721]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01447-01443-00722]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01447-00721-00720]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01524-01523-01528]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00399-01488-00398]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01438-00951-01444]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01537-01536-01541]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01541-01540-01545]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01541-01536-01540]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										



[illegible]



**Sollette - Verifiche pressoflessione retta allo stato limite di esercizio**

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
P	00110	0.000	-5.074	191.155	00111	0.000	-5.101	168.316	00112	0.000	-4.941	202.191	00113	0.000	-5.110	173.832
S		0.549	-0.656	6.425		0.942	-0.674	11.705		0.604	-0.733	7.051		0.524	-0.669	6.068
P	00114	0.000	-4.947	198.515	00115	0.000	-5.254	191.045	00116	0.000	-5.097	202.317	00117	0.000	-5.120	189.752
S		0.698	-0.789	8.236		0.579	-0.679	6.803		0.684	-0.744	8.125		0.928	-0.796	11.337
P	00118	0.000	-4.828	193.050	00119	0.000	-5.094	174.758	00120	0.000	-5.053	196.071	00121	0.000	-5.005	187.838
S		0.588	-0.699	6.886		0.900	-0.677	11.140		0.547	-0.747	6.265		0.563	-0.671	6.589
P	00122	0.000	-5.040	176.821	00123	0.000	-4.280	193.916	00124	0.000	-4.241	167.555	00125	0.000	-3.520	166.254
S		0.558	-0.562	6.687		0.443	-0.767	4.827		0.905	-0.540	11.410		0.510	-0.525	6.094
P	00126	1.679	-2.255	19.277	00127	1.462	-1.496	17.498	00128	0.600	-1.211	6.288	00137	0.296	-0.297	3.553
S		0.708	-0.472	8.856		0.271	-0.261	3.261		0.477	-0.209	6.247		0.362	-0.551	4.057
P	00379	0.000	-0.200	0.000	00380	0.139	-0.181	1.611	00381	0.593	-1.069	6.397	00382	1.443	-2.183	16.207
S		0.056	-0.419	0.132		0.000	-0.215	0.000		0.000	-0.351	0.000		0.051	-0.660	0.000
P	00383	1.826	-2.112	21.478	00384	0.000	-4.207	156.580	00385	0.000	-4.869	190.857	00386	0.000	-4.696	197.187
S		0.239	-0.687	2.193		0.447	-0.786	4.858		0.445	-0.794	4.816		0.489	-0.794	5.410
P	00387	0.000	-5.161	208.560	00388	0.000	-5.212	204.383	00389	0.000	-5.676	226.865	00390	0.000	-5.580	223.994
S		0.686	-0.912	7.887		0.659	-0.946	7.476		0.596	-0.813	6.826		0.765	-0.964	8.882
P	00391	0.000	-5.618	221.895	00392	0.000	-5.939	236.645	00393	0.000	-5.671	225.365	00394	0.000	-5.773	228.428
S		0.725	-0.969	8.334		0.654	-0.827	7.583		0.787	-0.971	9.171		0.751	-0.962	8.702
P	00395	0.000	-5.877	231.811	00396	0.000	-6.406	251.580	00397	0.000	-5.903	234.226	00398	0.000	-5.880	233.263
S		0.680	-0.852	7.909		0.714	-0.916	8.269		0.770	-0.957	8.953		0.692	-0.869	8.038
P	00399	0.000	-6.427	253.156	00400	0.000	-5.899	233.848	00401	0.000	-5.824	232.150	00402	0.000	-6.428	252.388
S		0.707	-0.907	8.182		0.749	-0.925	8.730		0.692	-0.882	8.013		0.702	-0.911	8.106
P	00403	0.000	-5.798	228.796	00404	0.000	-5.671	226.924	00405	0.000	-6.194	243.235	00406	0.000	-5.545	216.432
S		0.701	-0.878	8.152		0.685	-0.892	7.913		0.664	-0.879	7.640		0.641	-0.816	7.432
P	00407	0.000	-5.184	207.128	00408	0.000	-5.525	214.025	00409	0.000	-4.620	175.747	00410	0.000	-3.736	145.861
S		0.631	-0.860	7.227		0.582	-0.801	6.658		0.501	-0.672	5.752		0.472	-0.651	5.395
P	00411	1.812	-1.826	21.729	00412	1.396	-1.481	16.631	00413	0.604	-0.761	7.016	00414	0.188	-0.429	1.900
S		0.489	-0.630	5.659		0.240	-0.345	2.718		0.054	-0.202	0.430		0.084	-0.212	0.821
P	00415	1.179	-1.104	14.255	00609	0.000	-0.487	0.000	00610	0.000	-0.102	0.000	00611	0.027	0.000	0.363
S		0.332	-0.252	4.098		0.000	-1.665	0.000		0.000	-0.416	0.000		0.000	-0.551	0.000
P	00612	0.077	-0.142	0.833	00613	0.028	-0.061	0.287	00614	0.045	-0.025	0.565	00615	0.132	-0.083	1.653
S		0.004	-0.593	0.000		0.138	-0.566	1.015		0.280	-0.475	3.072		0.313	-0.387	3.645
P	00616	0.036	-0.045	0.417	00617	0.079	-0.092	0.932	00618	0.053	-0.041	0.658	00619	0.079	-0.067	0.963
S		0.353	-0.354	4.231		0.298	-0.294	3.582		0.350	-0.155	4.486		0.416	-0.039	5.557
P	00620	0.020	0.000	0.279	00621	0.012	-0.012	0.148	00622	0.063	-0.051	0.775	00623	0.081	-0.039	1.040
S		0.361	0.000	4.879		0.426	0.000	5.971		0.381	0.000	5.326		0.452	0.000	6.489
P	00624	0.069	-0.035	0.877	00625	0.016	0.000	0.218	00626	0.035	-0.007	0.469	00627	0.059	-0.041	0.740
S		0.469	0.000	6.789		0.447	0.000	6.605		0.505	0.000	7.498		0.466	0.000	6.902
P	00628	0.100	-0.036	1.298	00629	0.054	-0.007	0.718	00630	0.028	-0.007	0.372	00631	0.042	-0.010	0.558
S		0.553	0.000	8.231		0.529	0.000	7.881		0.635	0.000	9.363		0.546	0.000	8.098
P	00632	0.105	-0.037	1.358	00633	0.058	-0.041	0.723	00634	0.042	0.000	0.579	00635	0.031	-0.010	0.400
S		0.624	0.000	9.267		0.615	0.000	9.101		0.660	0.000	9.763		0.707	0.000	10.402
P	00636	0.050	-0.010	0.666	00637	0.110	-0.037	1.425	00638	0.055	-0.026	0.705	00639	0.036	-0.004	0.477
S		0.613	0.000	9.061		0.666	0.000	9.858		0.609	0.000	9.000		0.677	0.000	10.011
P	00640	0.035	-0.005	0.463	00641	0.057	-0.026	0.737	00642	0.107	-0.041	1.378	00643	0.052	-0.024	0.664
S		0.661	0.000	9.763		0.591	0.000	8.764		0.606	0.000	8.997		0.519	0.000	7.723
P	00644	0.031	-0.010	0.403	00645	0.033	0.000	0.450	00646	0.065	-0.050	0.807	00647	0.097	-0.052	1.230
S		0.592	0.000	8.735		0.509	0.000	7.544		0.515	0.000	7.605		0.505	0.000	7.398
P	00648	0.053	-0.045	0.645	00649	0.018	0.000	0.241	00650	0.082	-0.036	1.056	00651	0.099	-0.052	1.254
S		0.436	0.000	6.293		0.442	0.000	6.444		0.447	0.000	6.322		0.452	0.000	6.310
P	00652	0.083	-0.074	1.011	00653	0.044	-0.021	0.567	00654	0.013	-0.008	0.161	00655	0.115	-0.092	1.413
S		0.360	-0.018	4.833		0.424	0.000	5.731		0.359	-0.150	4.616		0.390	-0.191	4.979



**Solette - Verifiche pressoflessione retta allo stato limite di esercizio**

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
P	00656	0.073	-0.063	0.896	00657	0.116	-0.123	1.377	00658	0.005	0.000	0.071	00659	0.017	-0.015	0.205
S		0.344	-0.299	4.198		0.258	-0.433	2.839		0.313	-0.446	3.549		0.158	-0.565	1.283
P	00660	0.090	-0.108	1.047	00661	0.002	-0.142	0.000	00662	0.106	-0.130	1.231	00663	0.000	-0.277	0.000
S		0.156	-0.500	1.350		0.000	-0.579	0.000		0.000	-0.457	0.000		0.000	-1.612	0.000
P	00664	0.000	-1.139	0.000	00665	0.000	-0.764	0.000	00666	0.000	-1.115	0.000	00667	0.000	-0.724	0.000
S		0.000	-0.551	0.000		0.156	-0.244	1.739		0.107	-0.158	1.200		0.184	-0.173	2.227
P	00668	0.000	-0.558	0.000	00669	0.000	-0.136	0.000	00670	0.137	-0.093	1.707	00671	0.026	-0.010	0.338
S		0.071	-0.243	0.591		0.844	-0.691	10.352		0.345	0.000	4.843		0.426	0.000	5.956
P	00672	0.124	-0.081	1.552	00673	0.064	-0.015	0.847	00674	0.041	-0.001	0.559	00675	0.124	-0.103	1.521
S		0.543	-0.089	7.197		0.688	-0.144	9.072		0.712	-0.216	9.287		0.633	-0.257	8.165
P	00676	0.058	-0.049	0.703	00677	0.102	-0.072	1.266	00678	0.050	-0.017	0.652	00679	0.082	-0.073	0.993
S		0.662	-0.236	8.588		0.557	-0.222	7.190		0.507	-0.191	6.557		0.421	-0.220	5.355
P	00680	0.015	-0.012	0.191	00681	0.011	-0.001	0.154	00682	0.063	-0.052	0.769	00683	0.058	-0.042	0.723
S		0.380	-0.140	4.922		0.305	-0.129	3.919		0.277	-0.126	3.549		0.229	-0.096	2.944
P	00684	0.062	-0.057	0.758	00685	0.005	-0.005	0.062	00686	0.022	-0.014	0.276	00687	0.051	-0.047	0.616
S		0.180	-0.098	2.289		0.137	-0.032	1.804		0.108	-0.031	1.411		0.110	-0.044	1.421
P	00688	0.066	-0.054	0.806	00689	0.041	-0.036	0.504	00690	0.009	-0.007	0.113	00691	0.034	-0.026	0.423
S		0.092	-0.028	1.203		0.069	-0.031	0.883		0.068	-0.001	0.916		0.044	-0.011	0.572
P	00692	0.069	-0.057	0.840	00693	0.051	-0.049	0.619	00694	0.016	-0.009	0.207	00695	0.016	-0.014	0.194
S		0.048	-0.002	0.646		0.033	-0.003	0.455		0.052	-0.002	0.703		0.073	-0.024	0.947
P	00696	0.037	-0.031	0.459	00697	0.070	-0.060	0.861	00698	0.045	-0.041	0.550	00699	0.018	-0.014	0.226
S		0.032	-0.002	0.438		0.039	0.000	0.537		0.030	-0.006	0.409		0.059	-0.012	0.773
P	00700	0.015	-0.011	0.184	00701	0.048	-0.043	0.582	00702	0.071	-0.060	0.874	00703	0.045	-0.039	0.551
S		0.058	-0.011	0.766		0.040	-0.018	0.519		0.056	-0.017	0.728		0.060	-0.036	0.761
P	00704	0.017	-0.014	0.214	00705	0.012	-0.006	0.160	00706	0.064	-0.060	0.768	00707	0.071	-0.058	0.877
S		0.038	0.000	0.528		0.073	-0.029	0.948		0.107	-0.077	1.334		0.140	-0.088	1.763
P	00708	0.061	-0.053	0.745	00709	0.007	-0.002	0.086	00710	0.078	-0.071	0.940	00711	0.075	-0.061	0.919
S		0.153	-0.116	1.891		0.167	-0.102	2.098		0.215	-0.173	2.638		0.271	-0.199	3.361
P	00712	0.083	-0.079	1.002	00713	0.038	-0.030	0.469	00714	0.025	-0.020	0.303	00715	0.119	-0.111	1.439
S		0.315	-0.248	3.879		0.343	-0.263	4.237		0.414	-0.313	5.123		0.434	-0.357	5.329
P	00716	0.068	-0.048	0.851	00717	0.131	-0.121	1.582	00718	0.015	-0.005	0.190	00719	0.031	-0.020	0.387
S		0.489	-0.367	6.054		0.506	-0.392	6.239		0.545	-0.402	6.759		0.511	-0.335	6.398
P	00720	0.094	-0.080	1.149	00721	0.083	-0.053	1.047	00722	0.119	-0.091	1.467	00723	0.028	-0.034	0.331
S		0.427	-0.281	5.337		0.266	-0.042	3.532		0.268	-0.090	3.489		0.870	-0.666	10.749
P	00724	0.000	-0.373	0.000	00725	0.000	-0.624	0.000	00726	0.000	-0.673	0.000	00727	0.000	-0.610	0.000
S		0.192	-0.316	2.116		0.254	-0.302	2.982		0.250	-0.252	2.995		0.202	-0.248	2.362
P	00728	0.000	-1.621	0.000	00891	1.081	-1.191	12.804	00892	0.000	-4.597	193.367	00894	0.000	-4.899	170.738
S		0.000	-0.611	0.000		0.048	-0.429	0.007		0.578	-0.774	6.646		0.976	-0.733	12.071
P	00896	0.000	-4.833	212.772	00898	0.000	-5.371	201.162	00901	0.000	-4.816	187.485	00902	0.000	-5.215	182.337
S		0.628	-0.836	7.228		0.620	-0.835	7.121		0.606	-0.940	6.774		0.585	-0.736	6.787
P	00904	0.000	-3.641	136.016	00906	1.687	-1.433	20.621	00909	0.000	-4.280	178.028	00910	0.000	-3.950	154.875
S		0.459	-0.493	5.460		0.059	-0.387	0.217		0.535	-0.745	6.110		0.495	-0.521	5.906
P	00912	0.922	-1.251	10.576	00914	1.043	-0.935	12.682	00917	0.000	-5.145	199.644	00918	0.000	-5.206	174.517
S		0.176	-0.173	2.274		0.317	-0.199	3.980		0.621	-0.849	7.110		0.865	-0.755	10.551
P	00921	0.000	-5.452	208.124	00922	0.000	-5.491	209.569	00923	0.000	-5.152	206.733	00924	0.000	-5.163	188.912
S		0.640	-0.883	7.320		0.638	-0.881	7.296		0.720	-0.849	8.442		0.918	-0.834	11.145
P	00928	0.000	-5.368	202.312	00930	0.000	-4.552	198.265	00932	0.000	-4.749	161.048	00935	0.000	-4.824	210.630
S		0.630	-0.826	7.264		0.654	-0.780	7.659		0.978	-0.718	12.132		0.620	-0.856	7.082
P	00936	0.000	-5.194	174.498	00939	0.000	-3.182	174.722	00940	0.000	-4.447	169.007	00943	1.672	-2.046	19.501
S		0.572	-0.745	6.604		0.228	-0.578	2.217		0.544	-0.610	6.429		0.309	-0.330	3.670
P	00944	0.000	-4.462	175.771	00947	0.041	-0.347	0.030	00948	0.088	-0.012	1.216	00951	0.000	-0.252	0.000
S		0.544	-0.592	6.462		0.746	-1.074	8.458		0.189	-0.213	2.235		0.142	-0.335	1.417



**Solette - Verifiche pressoflessione retta allo stato limite di esercizio**

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
P	00953	0.134	-0.387	1.229	00955	0.000	-0.676	0.000	00957	0.000	-0.689	0.000	00958	0.000	-0.423	0.000
S		1.092	-1.081	13.123		0.626	-0.665	7.447		0.698	-1.704	6.868		1.651	-1.614	19.866
P	00961	0.159	-0.700	1.092	01043	0.000	-0.875	0.000	01044	0.000	-0.649	0.000	01047	0.089	-0.476	0.481
S		1.120	-1.134	13.425		0.732	-0.862	8.583		0.882	-1.763	9.266		1.565	-1.538	18.813
P	01048	0.000	-0.679	0.000	01051	0.000	-0.439	0.000	01052	0.104	-0.070	1.352	01055	0.000	-0.226	0.000
S		0.972	-1.022	11.590		0.603	-0.824	6.900		0.441	-0.138	5.740		0.386	-0.625	4.269
P	01056	0.089	-0.363	0.659	01437	0.000	-0.064	0.000	01438	0.000	-0.136	0.000	01439	0.386	-0.103	5.235
S		1.288	-1.220	15.564		0.000	-0.182	0.000		0.041	-0.138	0.391		0.072	-0.065	0.939
P	01440	0.257	-0.072	3.508	01441	0.100	-0.230	1.126	01442	0.000	-0.449	0.000	01443	0.057	-0.204	0.460
S		0.000	-0.115	0.000		0.000	-0.106	0.000		0.000	-0.446	0.000		0.618	-0.588	7.464
P	01444	0.000	-0.140	0.000	01445	0.013	-0.193	0.000	01446	0.114	-0.106	1.381	01447	0.123	-0.145	1.439
S		0.032	-0.116	0.253		0.000	-0.276	0.000		0.000	-0.514	0.000		0.171	-0.171	2.057
P	01448	0.482	-0.555	5.673	01449	0.903	-1.035	10.641	01450	0.030	-0.059	0.314	01451	0.134	-0.138	1.608
S		0.000	-0.098	0.000		0.000	-0.163	0.000		0.095	-0.397	0.681		0.429	-0.348	5.270
P	01452	0.231	-0.245	2.757	01453	0.435	-0.485	5.140	01454	0.091	-0.089	1.095	01455	0.007	-0.003	0.085
S		0.131	-0.202	1.459		0.080	-0.186	0.796		0.280	-0.336	3.271		0.287	-0.279	3.456
P	01456	1.220	-1.218	14.640	01457	1.487	-1.532	17.779	01458	0.110	-0.107	1.325	01459	0.074	-0.076	0.882
S		0.037	-0.158	0.265		0.157	-0.139	1.911		0.184	-0.077	2.375		0.309	-0.264	3.776
P	01460	0.571	-0.567	6.859	01461	0.000	-3.881	157.738	01462	0.680	-0.740	8.073	01463	0.033	-0.038	0.388
S		0.000	-0.038	0.000		0.397	-0.564	4.512		0.103	0.000	1.479		0.324	0.000	4.458
P	01464	0.160	-0.158	1.922	01465	1.572	-1.566	18.878	01466	1.679	-1.797	19.967	01467	0.221	-0.227	2.649
S		0.111	-0.121	1.311		0.173	-0.299	1.887		0.273	-0.167	3.432		0.239	0.000	3.537
P	01468	0.029	-0.030	0.349	01469	0.780	-0.776	9.361	01470	0.000	-4.462	179.495	01471	0.830	-0.870	9.900
S		0.127	-0.110	1.556		0.065	-0.143	0.669		0.494	-0.665	5.673		0.240	0.000	3.389
P	01472	0.000	-0.012	0.000	01473	0.249	-0.248	2.992	01474	1.753	-1.753	21.037	01475	1.829	-1.899	21.837
S		0.392	0.000	5.785		0.008	-0.016	0.089		0.225	-0.351	2.509		0.336	-0.158	4.302
P	01476	0.286	-0.294	3.425	01477	0.005	-0.007	0.058	01478	0.872	-0.870	10.470	01479	0.000	-4.653	186.221
S		0.386	0.000	5.632		0.030	-0.021	0.366		0.114	-0.194	1.248		0.525	-0.693	6.043
P	01480	0.917	-0.943	10.966	01481	0.009	-0.013	0.100	01482	0.286	-0.285	3.429	01483	1.814	-1.815	21.763
S		0.331	0.000	4.657		0.497	0.000	7.321		0.042	-0.064	0.482		0.246	-0.370	2.765
P	01484	1.932	-2.020	23.056	01485	0.317	-0.329	3.789	01486	0.011	-0.012	0.124	01487	0.896	-0.894	10.757
S		0.401	-0.175	5.149		0.480	0.000	6.948		0.037	-0.020	0.468		0.131	-0.210	1.448
P	01488	0.000	-4.672	186.600	01489	0.947	-1.002	11.285	01490	0.016	-0.032	0.167	01491	0.291	-0.290	3.489
S		0.514	-0.676	5.920		0.362	0.000	5.079		0.563	0.000	8.279		0.052	-0.077	0.604
P	01492	1.815	-1.816	21.780	01493	1.862	-2.032	22.084	01494	0.339	-0.345	4.054	01495	0.009	-0.011	0.107
S		0.252	-0.373	2.848		0.441	-0.196	5.658		0.512	0.000	7.381		0.042	-0.021	0.530
P	01496	0.884	-0.881	10.609	01497	0.000	-4.612	185.028	01498	0.975	-1.057	11.575	01499	0.020	-0.037	0.210
S		0.131	-0.207	1.453		0.495	-0.655	5.694		0.398	0.000	5.492		0.549	0.000	8.071
P	01500	0.275	-0.274	3.307	01501	1.790	-1.785	21.483	01502	1.936	-2.096	22.987	01503	0.331	-0.344	3.957
S		0.049	-0.064	0.575		0.248	-0.367	2.802		0.426	-0.224	5.420		0.465	0.000	6.704
P	01504	0.007	-0.007	0.089	01505	0.839	-0.834	10.071	01506	0.000	-4.635	185.764	01507	0.961	-1.021	11.439
S		0.035	-0.005	0.460		0.121	-0.192	1.348		0.486	-0.650	5.584		0.311	0.000	4.329
P	01508	0.015	-0.028	0.159	01509	0.239	-0.236	2.874	01510	1.766	-1.753	21.212	01511	1.940	-1.989	23.201
S		0.458	0.000	6.758		0.031	-0.021	0.381		0.230	-0.355	2.576		0.357	-0.191	4.527
P	01512	0.306	-0.317	3.662	01513	0.020	-0.021	0.238	01514	0.754	-0.742	9.070	01515	0.000	-4.462	181.036
S		0.338	0.000	4.901		0.101	-0.046	1.294		0.087	-0.146	0.955		0.447	-0.624	5.092
P	01516	0.909	-0.953	10.840	01517	0.002	-0.010	0.017	01518	0.167	-0.161	2.009	01519	1.606	-1.580	19.317
S		0.170	0.000	2.458		0.349	0.000	5.055		0.089	-0.052	1.127		0.174	-0.306	1.893
P	01520	1.775	-1.886	21.130	01521	0.227	-0.239	2.707	01522	0.050	-0.053	0.593	01523	0.595	-0.574	7.170
S		0.292	-0.220	3.617		0.189	0.000	2.744		0.279	-0.136	3.563		0.004	-0.040	0.010
P	01524	0.000	-3.999	164.149	01525	0.718	-0.802	8.486	01526	0.038	-0.051	0.432	01527	0.043	-0.038	0.526
S		0.369	-0.575	4.113		0.045	-0.008	0.597		0.303	-0.087	3.957		0.280	-0.163	3.540



D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
P	01528	1.230	-1.217	14.772	01529	1.379	-1.564	16.271	01530	0.073	-0.091	0.851	01531	0.105	-0.105	1.260
S		0.049	-0.212	0.348		0.176	-0.268	1.974		0.148	-0.188	1.715		0.542	-0.258	6.925
P	01532	0.303	-0.323	3.603	01533	1.934	-1.970	23.157	01534	0.368	-0.443	4.299	01535	0.114	-0.114	1.364
S		0.120	-0.141	1.411		0.199	-0.485	1.960		0.000	-0.177	0.000		0.169	-0.440	1.614
P	01536	0.086	-0.121	0.985	01537	0.581	-0.753	6.717	01538	0.777	-0.788	9.304	01539	0.003	-0.170	0.000
S		0.426	-0.228	5.408		0.000	-0.094	0.000		0.000	-0.091	0.000		0.000	-0.371	0.000
P	01540	0.097	-0.098	1.161	01541	0.000	-0.101	0.000	01542	0.629	-1.114	6.820	01543	0.000	-0.190	0.000
S		0.327	-0.019	4.383		0.129	-0.161	1.506		0.000	-0.270	0.000		0.000	-0.086	0.000
P	01544	0.000	-0.490	0.000	01545	0.000	-0.239	0.000	01546	0.000	-0.157	0.000	02511	0.000	-0.784	0.000
S		0.000	-0.733	0.000		0.409	-0.363	4.972		0.000	-0.101	0.000		0.197	-1.532	0.363
P	02512	0.000	-0.885	0.000	02513	0.000	-0.483	0.000	02514	0.013	-0.417	0.000				
S		0.161	-1.567	0.000		1.217	-1.325	14.441		1.396	-1.398	16.746				

Soletta P2-P3-P6-P5 S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm Piano Terra	AA= PCA CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
SHELL: [00418-00052-01548]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [01604-00400-00399]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [00055-01111-02517]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [01654-00386-01659]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [00055-02517-00416]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [01111-00746-02517]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [01111-00039-00746]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [00039-01113-00748]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [00039-00748-00747]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [01113-02518-00748]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [01113-00038-02518]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [02516-00731-00380]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [00038-01080-02518]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [01080-00749-02518]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [01080-00037-01669]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [00731-00730-00380]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [01080-01669-00749]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [01549-01548-00414]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [00037-01082-01669]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [01560-00412-00411]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [01082-01664-01669]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [01549-00414-00413]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [01082-00036-01664]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm	
SHELL: [01560-00411-00410]AA= PCA	CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W



## Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00033-01090-01653]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01593-00402-00401]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01090-00032-01647]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00739-00738-00043]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01090-01647-01653]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00965-00737-00042]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00032-01093-01647]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01582-00406-00405]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01093-00031-01642]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01648-00389-00388]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01093-01642-01647]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00031-01087-01642]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00030-01636-01642]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00030-01089-01636]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01089-01631-01636]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00029-01062-01631]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01062-00028-01631]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00005-01548-01549]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00028-01625-01631]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01637-00391-00390]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01064-00027-01625]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00027-01620-01625]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00027-01059-01620]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [02516-00380-00137]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01059-00026-01620]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00736-00735-00963]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00026-01061-01620]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00966-02516-00137]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01061-01614-01620]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00005-00418-01548]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01061-00025-01614]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00025-01067-01614]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01067-00024-01609]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [02515-00382-00381]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00729-02515-00381]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01067-01609-01614]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00730-00381-00380]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00729-00381-00730]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01548-00052-00414]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00732-02516-00966]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										



## Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01588-01582-00404]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01659-00386-00385]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01566-00409-01571]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01588-00404-00403]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01626-00393-00392]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01626-00394-00393]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01555-01549-00413]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01615-00397-00396]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01555-00413-00412]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01659-00385-00384]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01604-00399-00398]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01615-00396-00395]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01611-01610-01616]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00024-01072-01609]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01648-00388-00387]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00971-00739-00043]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00042-00736-00963]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01571-00408-00407]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01654-01648-00387]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01666-00760-00759]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01571-00409-00408]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01654-00387-00386]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01582-00405-00404]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01599-00400-01604]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00040-00732-00966]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01665-01659-00384]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00023-01603-01609]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01621-01615-00395]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01643-01637-00390]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01643-00390-00389]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01577-01571-00407]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01665-00384-00383]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00762-00383-00382]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00762-00382-02515]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01665-00762-00761]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01665-00383-00762]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00023-01075-01603]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01075-00022-01603]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00733-00732-00040]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01643-00389-01648]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										



## Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01599-00401-00400]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00760-01665-00761]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01566-01560-00410]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01566-00410-00409]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01610-01604-00398]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01610-00398-00397]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01610-00397-01615]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01588-00403-01593]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01577-00407-00406]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00022-01598-01603]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01632-00391-01637]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01621-00394-01626]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01621-00395-00394]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00022-01069-01598]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01632-01626-00392]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01632-00392-00391]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01577-00406-01582]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01069-00021-01598]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01599-01593-00401]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01561-01555-01560]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01555-00412-01560]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01071-00020-01592]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01616-01615-01621]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00968-00733-00040]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01585-01579-01584]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01583-01577-01582]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01561-01560-01566]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00734-00733-00968]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01605-01604-01610]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01605-01599-01604]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01583-01582-01588]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01585-01584-01590]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01550-01549-01555]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01550-00005-01549]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01550-01032-00005]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01660-01654-01659]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01660-01659-01665]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00735-00734-00041]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01071-01592-01598]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01594-01593-01599]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										



## Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01594-01588-01593]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01666-01665-00760]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01572-01566-01571]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01572-01571-01577]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01606-01600-01605]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01616-01610-01615]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01627-01626-01632]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01627-01621-01626]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01649-01643-01648]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01649-01648-01654]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01638-01637-01643]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01638-01632-01637]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00041-00734-00968]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00757-01666-00758]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00006-01032-01550]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00020-01098-01587]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01655-01649-01654]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01622-01621-01627]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01622-01616-01621]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01666-01660-01665]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01556-01555-01561]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01556-01550-01555]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01655-01654-01660]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00020-01587-01592]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00749-01669-00750]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01567-01566-01572]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01567-01561-01566]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01606-01605-01611]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01617-01611-01616]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01578-01572-01577]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01578-01577-01583]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01551-01550-01556]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01547-01037-01554]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01611-01605-01610]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01600-01599-01605]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01600-01594-01599]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01644-01638-01643]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00737-00736-00042]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01644-01643-01649]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01633-01627-01632]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										



## Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01633-01632-01638]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01589-01588-01594]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01589-01583-01588]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01552-00008-01036]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01030-00006-01550]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01634-01633-01639]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00758-01666-00759]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00973-00741-00044]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01098-00019-01587]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01613-01607-01612]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00019-01101-01587]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01629-01623-01628]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01601-01595-01600]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01551-00007-01030]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01573-01572-01578]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01573-01567-01572]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01623-01617-01622]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01650-01649-01655]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01650-01644-01649]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00738-00737-00965]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01623-01622-01628]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01661-01660-01666]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01661-01655-01660]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01628-01622-01627]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01628-01627-01633]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01551-01030-01550]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01629-01628-01634]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01595-01589-01594]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01595-01594-01600]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01584-01578-01583]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01584-01583-01589]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01617-01616-01622]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01562-01561-01567]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01562-01556-01561]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01639-01638-01644]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01639-01633-01638]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01101-01581-01587]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01618-01612-01617]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00009-01033-01552]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01036-00007-01551]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										



## Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01669-01663-01668]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01645-01644-01650]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01645-01639-01644]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01613-01612-01618]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01656-01655-01661]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01656-01650-01655]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01634-01628-01633]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01601-01600-01606]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01667-00757-00756]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01579-01578-01584]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01590-01584-01589]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01590-01589-01595]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01568-01567-01573]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01568-01562-01567]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01667-01666-00757]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01657-01656-01662]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01101-00018-01581]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01557-01556-01562]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01667-01661-01666]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01557-01551-01556]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01657-01651-01656]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01579-01573-01578]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01612-01606-01611]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01612-01611-01617]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00043-00738-00965]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01095-00017-01576]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01095-01576-01581]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00975-00743-00045]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00755-01667-00756]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00044-00740-00971]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01640-01634-01639]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01640-01639-01645]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01596-01590-01595]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01596-01595-01601]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01618-01617-01623]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01552-01036-01551]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00045-00742-00973]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01651-01645-01650]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01651-01650-01656]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01662-01656-01661]AA= PCA						CA=FRQ $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}$ =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										



## Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01662-01661-01667]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01574-01568-01573]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01574-01573-01579]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01563-01562-01568]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01563-01557-01562]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00017-01097-01576]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01552-01551-01557]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01607-01601-01606]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01607-01606-01612]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01669-00752-00751]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00741-00740-00044]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00752-01668-00753]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00740-00739-00971]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00754-01667-00755]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01569-01563-01568]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01033-00008-01552]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00016-01570-01576]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00016-01103-01570]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01103-00015-01570]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01636-01635-01641]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01668-01662-01667]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01647-01641-01646]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01547-00011-01037]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01641-01635-01640]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01668-00754-00753]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01646-01645-01651]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01646-01640-01645]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01558-01557-01563]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01558-01552-01557]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01647-01646-01652]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01586-01585-01591]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01586-01580-01585]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01580-01579-01585]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01580-01574-01579]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01602-01596-01601]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01602-01601-01607]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01624-01623-01629]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01668-01667-00754]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01635-01629-01634]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01635-01634-01640]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										



D	σ ct	σ cc	σ at	NO DO	σ ct	σ cc	σ at	NO DO	σ ct	σ cc	σ at	NO DO	σ ct	σ cc	σ at
DO	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	DO	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	DO	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	DO	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01569-01568-01574]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [00015-01565-01570]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01624-01618-01623]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01591-01585-01590]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01591-01590-01596]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [00015-01106-01565]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [00742-00741-00973]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01663-01662-01668]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01630-01624-01629]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01663-01657-01662]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01630-01629-01635]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01619-01618-01624]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01619-01613-01618]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01608-01607-01613]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01608-01602-01607]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01575-01574-01580]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01575-01569-01574]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01652-01646-01651]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01652-01651-01657]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01553-01040-00009]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm															
SHELL: [01553-00009-01552]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm<										



## Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00013-01105-01554]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00750-01669-00751]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01636-01630-01635]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01658-01652-01657]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01592-01591-01597]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01105-00012-01554]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01592-01586-01591]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01559-01553-01558]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01559-01558-01564]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01570-01569-01575]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01570-01564-01569]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00028-01064-01625]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01625-01624-01630]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01625-01619-01624]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01614-01613-01619]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01614-01608-01613]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01581-01575-01580]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00014-01109-01565]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01037-00010-01553]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01097-00016-01576]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01072-00023-01609]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00018-01095-01581]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00012-00417-01554]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00744-00743-00975]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00046-00744-00975]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00417-01547-01554]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00745-00744-00046]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01609-01608-01614]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01609-01603-01608]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00416-00745-00046]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01631-01630-01636]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00417-00053-01547]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01642-01641-01647]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01642-01636-01641]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01576-01570-01575]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01576-01575-01581]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01554-01553-01559]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00053-00011-01547]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01587-01586-01592]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01587-01581-01586]AA= PCA						CA=FRQ $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR $\epsilon_{sm}=0.00000$ A <sub>e</sub> =0.0 cm <sup>2</sup>										



D DO	σ ct	σ cc	σ at	NO DO	σ ct	σ cc	σ at	NO DO	σ ct	σ cc	σ at	NO DO	σ ct	σ cc	σ at	
	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01620-01619-01625]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01620-01614-01619]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01631-01625-01630]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01653-01647-01652]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01653-01652-01658]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01087-00030-01642]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01664-01658-01663]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01664-01663-01669]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01565-01559-01564]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01565-01564-01570]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01598-01597-01603]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01598-01592-01597]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01554-01037-01553]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00039-00747-00746]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00035-01079-01658]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [01089-00029-01631]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00036-01077-01664]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [00035-01658-01664]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
SHELL: [02517-00745-00416]AA= PCA					CA=FRQ ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup> S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm CA=QPR ε <sub>sm</sub> =0.00000 A <sub>e</sub> =0.0 cm <sup>2</sup>											
S <sub>m</sub> =0 mm W <sub>k</sub> =0.00 mm																
P	0000 5	0.000	-0.266	0.000	0000 6	0.115	-0.363	1.008	0000 7	0.231	-0.446	2.447	0000 8	0.259	-0.483	2.779
S		0.160	-0.298	1.709		1.118	-1.245	13.219		1.616	-1.760	19.170		1.694	-1.822	20.141



**Solette - Verifiche pressoflessione retta allo stato limite di esercizio**

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
	6				7				8				9			
S		0.429	-0.738	4.680		0.600	-0.836	6.850		0.451	-0.689	5.051		0.439	-0.657	4.945
P	00390	0.000	-3.836	158.845	00391	0.000	-3.800	154.011	00392	0.000	-3.864	155.994	00393	0.000	-4.211	172.560
S		0.596	-0.796	6.850		0.571	-0.800	6.507		0.460	-0.627	5.275		0.443	-0.641	5.024
P	00394	0.000	-3.774	154.024	00395	0.000	-3.787	155.159	00396	0.000	-4.201	171.703	00397	0.000	-3.735	152.538
S		0.577	-0.767	6.638		0.470	-0.631	5.393		0.449	-0.638	5.110		0.565	-0.739	6.519
P	00398	0.000	-3.769	155.413	00399	0.000	-4.282	175.150	00400	0.000	-3.766	153.465	00401	0.000	-3.812	157.394
S		0.488	-0.652	5.616		0.448	-0.636	5.094		0.556	-0.724	6.425		0.511	-0.685	5.871
P	00402	0.000	-4.361	178.571	00403	0.000	-3.901	157.880	00404	0.000	-3.916	160.656	00405	0.000	-4.523	183.293
S		0.452	-0.650	5.123		0.559	-0.728	6.450		0.536	-0.726	6.144		0.461	-0.667	5.218
P	00406	0.000	-4.040	160.885	00407	0.000	-3.990	161.168	00408	0.000	-4.477	177.704	00409	0.000	-3.889	148.637
S		0.543	-0.720	6.252		0.564	-0.771	6.454		0.455	-0.664	5.144		0.475	-0.657	5.423
P	00410	0.000	-3.597	139.292	00411	0.000	-3.598	138.375	00412	1.556	-1.763	18.357	00413	0.895	-1.095	10.435
S		0.534	-0.714	6.134		0.351	-0.537	3.928		0.255	-0.397	2.844		0.245	-0.382	2.741
P	00414	0.288	-0.573	3.027	00416	0.000	-0.708	0.000	00417	0.000	-0.311	0.000	00418	0.000	-0.297	0.000
S		0.110	-0.292	1.044		0.005	-0.455	0.000		0.000	-0.338	0.000		0.248	-0.457	2.664
P	00729	0.428	-0.244	5.414	00730	0.206	-0.109	2.621	00731	0.000	-0.024	0.000	00732	0.118	0.000	1.638
S		0.000	-0.972	0.000		0.000	-0.113	0.000		0.163	0.000	2.230		0.090	0.000	1.258
P	00733	0.058	0.000	0.854	00734	0.060	0.000	0.877	00735	0.058	0.000	0.868	00736	0.065	0.000	0.945
S		0.038	0.000	0.549		0.036	0.000	0.518		0.040	0.000	0.566		0.046	0.000	0.652
P	00737	0.049	0.000	0.721	00738	0.036	0.000	0.514	00739	0.000	-0.014	0.000	00740	0.000	-0.071	0.000
S		0.042	0.000	0.597		0.039	0.000	0.554		0.033	0.000	0.466		0.048	0.000	0.667
P	00741	0.000	-0.160	0.000	00742	0.000	-0.256	0.000	00743	0.000	-0.348	0.000	00744	0.000	-0.492	0.000
S		0.063	0.000	0.878		0.051	0.000	0.725		0.032	0.000	0.452		0.051	0.000	0.699
P	00745	0.000	-0.846	0.000	00746	0.000	-0.098	0.000	00747	0.053	0.000	0.775	00748	0.266	-0.075	3.475
S		0.000	-0.145	0.000		0.000	-0.508	0.000		0.000	-0.361	0.000		0.000	-0.135	0.000
P	00749	1.789	-1.170	22.390	00750	0.891	-0.302	11.578	00751	0.248	0.000	3.418	00752	0.747	-0.534	9.277
S		0.129	0.000	1.878		0.152	-0.018	2.023		0.105	-0.066	1.325		0.188	-0.186	2.257
P	00753	1.278	-1.068	15.653	00754	1.471	-1.408	17.745	00755	1.658	-1.571	20.021	00756	1.568	-1.670	18.664
S		0.071	-0.039	0.906		0.205	-0.184	2.485		0.088	-0.054	1.112		0.055	-0.078	0.623
P	00757	1.392	-1.505	16.541	00758	1.096	-1.269	12.893	00759	0.549	-0.983	5.932	00760	0.118	-0.450	0.919
S		0.190	-0.191	2.280		0.040	-0.033	0.497		0.113	-0.185	1.248		0.003	-0.075	0.000
P	00761	0.181	-0.987	0.964	00762	0.863	-2.091	8.513	00963	0.026	0.000	0.358	00965	0.017	-0.010	0.211
S		0.000	-0.182	0.000		0.000	-0.371	0.000		0.000	-0.040	0.000		0.000	-0.051	0.000
P	00966	0.107	-0.123	1.259	00968	0.007	-0.016	0.091	00971	0.000	-0.070	0.000	00973	0.000	-0.178	0.000
S		0.205	-0.206	2.452		0.000	-0.047	0.000		0.000	-0.053	0.000		0.000	-0.064	0.000
P	00975	0.000	-0.371	0.000	01030	0.286	-0.495	3.119	01032	0.000	-0.312	0.000	01033	0.229	-0.366	2.548
S		0.000	-0.065	0.000		1.334	-1.436	15.853		0.681	-0.885	7.872		1.611	-1.741	19.132
P	01036	0.361	-0.566	4.029	01037	0.000	-0.179	0.000	01040	0.102	-0.348	0.861	01059	0.000	-4.617	174.678
S		1.650	-1.785	19.601		0.232	-0.415	2.508		1.151	-1.290	13.599		0.446	-0.699	4.978
P	01061	0.000	-4.426	167.742	01062	0.000	-4.852	182.698	01064	0.000	-4.641	176.050	01067	0.000	-4.430	167.748
S		0.597	-0.830	6.818		0.472	-0.711	5.299		0.460	-0.675	5.198		0.595	-0.834	6.784
P	01069	0.000	-4.859	182.566	01071	0.000	-4.446	169.671	01072	0.000	-4.634	174.856	01075	0.000	-4.652	176.164
S		0.478	-0.706	5.397		0.532	-0.735	6.082		0.447	-0.690	4.996		0.465	-0.677	5.262
P	01077	0.000	-4.656	171.043	01079	0.000	-4.500	164.950	01080	0.000	-3.638	185.258	01082	0.000	-4.276	163.169
S		0.513	-0.616	6.007		0.493	-0.609	5.736		0.647	-0.567	7.883		0.627	-0.592	7.575
P	01085	0.000	-4.523	166.478	01087	0.000	-4.541	169.686	01089	0.000	-4.436	170.262	01090	0.000	-4.315	160.682
S		0.468	-0.626	5.379		0.454	-0.682	5.106		0.524	-0.740	5.969		0.612	-0.773	7.109
P	01093	0.000	-4.340	162.741	01095	0.000	-4.215	157.397	01097	0.000	-4.255	158.850	01098	0.000	-4.536	170.036
S		0.604	-0.801	6.949		0.606	-0.782	7.006		0.441	-0.564	5.110		0.471	-0.683	5.331
P	01101	0.000	-4.290	162.376	01103	0.000	-3.907	146.422	01105	0.691	-0.887	7.998	01106	0.000	-3.604	133.179
S		0.591	-0.764	6.836		0.424	-0.543	4.906		0.000	-0.332	0.000		0.360	-0.491	4.126
P	0110	1.459	-1.630	17.253	0111	0.000	-0.403	0.000	0111	0.782	-0.773	9.403	0154	0.000	-0.223	0.000



**Solette - Verifiche pressoflessione retta allo stato limite di esercizio**

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
	9				1				3				7			
S		0.203	-0.361	2.194		0.000	-0.744	0.000		0.000	-0.110	0.000		0.000	-0.214	0.000
P	01548	0.000	-0.195	0.000	01549	0.105	-0.351	0.891	01550	0.063	-0.311	0.379	01551	0.148	-0.394	1.407
S		0.010	-0.232	0.000		0.000	-0.135	0.000		0.000	-0.165	0.000		0.150	-0.306	1.564
P	01552	0.157	-0.420	1.488	01553	0.031	-0.330	0.000	01554	0.056	-0.319	0.276	01555	0.000	-0.117	0.000
S		0.150	-0.295	1.582		0.000	-0.176	0.000		0.000	-0.177	0.000		0.019	-0.189	0.000
P	01556	0.497	-0.666	5.713	01557	0.646	-0.838	7.464	01558	0.484	-0.682	5.506	01559	0.000	-0.100	0.000
S		0.249	-0.433	2.715		0.327	-0.506	3.652		0.252	-0.449	2.722		0.044	-0.291	0.159
P	01560	0.947	-1.001	11.285	01561	0.417	-0.519	4.856	01562	0.984	-1.110	11.624	01563	0.974	-1.112	11.476
S		0.042	-0.216	0.239		0.211	-0.406	2.244		0.453	-0.653	5.135		0.453	-0.660	5.129
P	01564	0.394	-0.528	4.521	01565	0.908	-1.015	10.731	01566	0.183	-0.217	2.143	01567	0.966	-1.038	11.482
S		0.212	-0.434	2.216		0.000	-0.193	0.000		0.000	-0.199	0.000		0.341	-0.549	3.774
P	01568	1.309	-1.401	15.575	01569	0.932	-1.033	11.034	01570	0.171	-0.277	1.891	01571	1.308	-1.286	15.730
S		0.468	-0.682	5.294		0.338	-0.557	3.734		0.072	-0.270	0.565		0.068	-0.277	0.497
P	01572	0.561	-0.590	6.688	01573	1.382	-1.436	16.502	01574	1.354	-1.427	16.137	01575	0.478	-0.568	5.595
S		0.141	-0.352	1.369		0.372	-0.588	4.137		0.366	-0.585	4.070		0.127	-0.340	1.210
P	01576	1.340	-1.452	15.915	01577	0.249	-0.237	3.009	01578	1.153	-1.175	13.803	01579	1.562	-1.609	18.674
S		0.066	-0.249	0.512		0.000	-0.157	0.000		0.242	-0.456	2.578		0.348	-0.566	3.843
P	01580	1.071	-1.142	12.749	01581	0.308	-0.410	3.546	01582	1.349	-1.308	16.245	01583	0.634	-0.630	7.616
S		0.229	-0.445	2.425		0.019	-0.218	0.000		0.078	-0.285	0.629		0.089	-0.299	0.758
P	01584	1.524	-1.548	18.257	01585	1.472	-1.523	17.585	01586	0.474	-0.553	5.568	01587	1.489	-1.598	17.698
S		0.283	-0.498	3.068		0.271	-0.488	2.926		0.057	-0.271	0.361		0.098	-0.301	0.872
P	01588	0.227	-0.199	2.769	01589	1.229	-1.231	14.738	01590	1.642	-1.674	19.655	01591	1.102	-1.164	13.135
S		0.000	-0.150	0.000		0.200	-0.410	2.088		0.286	-0.501	3.106		0.167	-0.385	1.683
P	01592	0.346	-0.439	4.009	01593	1.298	-1.254	15.643	01594	0.683	-0.667	8.216	01595	1.575	-1.589	18.884
S		0.000	-0.155	0.000		0.071	-0.271	0.552		0.083	-0.286	0.696		0.256	-0.467	2.751
P	01596	1.504	-1.548	17.988	01597	0.466	-0.540	5.485	01598	1.536	-1.645	18.274	01599	0.188	-0.155	2.309
S		0.237	-0.454	2.515		0.027	-0.248	0.000		0.099	-0.327	0.853		0.000	-0.156	0.000
P	01600	1.264	-1.261	15.175	01601	1.668	-1.695	19.978	01602	1.109	-1.166	13.227	01603	0.389	-0.481	4.536
S		0.196	-0.400	2.042		0.272	-0.485	2.946		0.157	-0.377	1.550		0.000	-0.194	0.000
P	01604	1.254	-1.208	15.117	01605	0.712	-0.693	8.568	01606	1.595	-1.606	19.129	01607	1.515	-1.556	18.122
S		0.071	-0.263	0.559		0.087	-0.284	0.749		0.254	-0.461	2.732		0.230	-0.447	2.434
P	01608	0.466	-0.536	5.487	01609	1.553	-1.654	18.490	01610	0.168	-0.133	2.069	01611	1.278	-1.274	15.346
S		0.017	-0.244	0.000		0.085	-0.324	0.664		0.000	-0.158	0.000		0.198	-0.400	2.075
P	01612	1.676	-1.702	20.078	01613	1.111	-1.166	13.252	01614	0.398	-0.485	4.641	01615	1.246	-1.193	15.030
S		0.271	-0.483	2.939		0.154	-0.375	1.516		0.000	-0.201	0.000		0.068	-0.260	0.526
P	01616	0.718	-0.698	8.642	01617	1.598	-1.609	19.162	01618	1.516	-1.557	18.132	01619	0.466	-0.536	5.491
S		0.089	-0.285	0.772		0.255	-0.460	2.751		0.230	-0.445	2.443		0.017	-0.243	0.000
P	01620	1.555	-1.653	18.513	01621	0.176	-0.137	2.175	01622	1.272	-1.268	15.273	01623	1.672	-1.700	20.021
S		0.085	-0.326	0.665		0.000	-0.155	0.000		0.198	-0.398	2.072		0.272	-0.480	2.955
P	01624	1.110	-1.168	13.231	01625	0.392	-0.481	4.566	01626	1.279	-1.209	15.459	01627	0.699	-0.678	8.418
S		0.156	-0.373	1.552		0.000	-0.194	0.000		0.075	-0.271	0.607		0.081	-0.280	0.676
P	01628	1.585	-1.599	18.994	01629	1.508	-1.556	18.020	01630	0.464	-0.541	5.453	01631	1.540	-1.644	18.326
S		0.252	-0.455	2.726		0.233	-0.439	2.489		0.025	-0.240	0.000		0.100	-0.333	0.848
P	01632	0.227	-0.180	2.800	01633	1.247	-1.247	14.964	01634	1.654	-1.693	19.792	01635	1.102	-1.174	13.111
S		0.000	-0.149	0.000		0.188	-0.389	1.955		0.272	-0.469	2.967		0.158	-0.357	1.601
P	01636	0.352	-0.450	4.084	01637	1.401	-1.335	16.911	01638	0.659	-0.642	7.934	01639	1.554	-1.582	18.606
S		0.000	-0.146	0.000		0.099	-0.324	0.853		0.061	-0.268	0.422		0.249	-0.442	2.697
P	01640	1.488	-1.557	17.754	01641	0.459	-0.557	5.357	01642	1.510	-1.620	17.950	01643	0.283	-0.250	3.442
S		0.242	-0.423	2.632		0.042	-0.227	0.227		0.100	-0.307	0.897		0.000	-0.141	0.000
P	01644	1.201	-1.217	14.394	01645	1.621	-1.686	19.351	01646	1.083	-1.187	12.841	01647	0.345	-0.470	3.948
S		0.177	-0.377	1.820		0.280	-0.448	3.108		0.185	-0.337	1.993		0.003	-0.173	0.000
P	01648	1.401	-1.361	16.874	01649	0.595	-0.599	7.128	01650	1.504	-1.565	17.956	01651	1.455	-1.560	17.308



# Solette - Verifiche pressoflessione retta allo stato limite di esercizio

D	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$	NO DO	$\sigma_{ct}$	$\sigma_{cc}$	$\sigma_{at}$
		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]		[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]	[N/mm <sup>2</sup> ]
	8				9				0				1			
S		0.075	-0.343	0.503		0.040	-0.265	0.148		0.250	-0.418	2.746		0.265	-0.388	2.990
P	0165 2	0.448	-0.584	5.177	0165 3	1.464	-1.607	17.355	0165 4	0.315	-0.327	3.767	0165 5	1.127	-1.198	13.422
S		0.075	-0.187	0.731		0.116	-0.270	1.159		0.000	-0.146	0.000		0.166	-0.352	1.718
P	0165 6	1.574	-1.679	18.729	0165 7	1.063	-1.191	12.570	0165 8	0.315	-0.464	3.560	0165 9	1.423	-1.479	16.990
S		0.294	-0.401	3.369		0.221	-0.284	2.561		0.051	-0.121	0.505		0.045	-0.404	0.002
P	0166 0	0.466	-0.597	5.400	0166 1	1.429	-1.559	16.959	0166 2	1.432	-1.533	17.027	0166 3	0.466	-0.562	5.446
S		0.027	-0.243	0.000		0.254	-0.353	2.893		0.282	-0.320	3.322		0.122	-0.124	1.467
P	0166 4	1.442	-1.561	17.125	0166 5	0.219	-0.637	1.995	0166 6	0.959	-1.230	11.107	0166 7	1.572	-1.654	18.741
S		0.181	-0.212	2.126		0.000	-0.166	0.000		0.171	-0.235	1.953		0.269	-0.292	3.192
P	0166 8	1.145	-1.123	13.773	0166 9	0.414	-0.296	5.138	0251 5	1.369	-2.866	14.188	0251 6	0.137	0.000	1.847
S		0.215	-0.208	2.593		0.153	-0.072	1.956		0.000	-0.640	0.000		0.357	-0.217	4.499
P	0251 7	0.000	-0.724	0.000	0251 8	0.000	-2.480	175.755								
S		0.000	-0.689	0.000		0.289	-0.202	3.603								

## LEGENDA Solette - Verifiche pressoflessione retta allo stato limite di esercizio

<b>D</b>	Direzione lungo la quale vengono fornite, per ciascun modo, le sollecitazioni.
<b>SHEL</b>	Elementi (shell) in cui viene scomposta (modellata) la soletta, individuati dai relativi vertici.
<b>L</b>	
<b>FRC</b>	Spostamento massimo (freccia) dell'elemento shell [cm].
<b>AA</b>	Identificativo dell'aggressività dell'ambiente: [PCA] = Poco aggressivo - [MDA] = Moderatamente aggressivo - [MLA] = Molto aggressivo.
<b>CA</b>	Identificativo della Combinazione di Azione: [QPR] = Quasi Permanente - [FRQ] = Frequente - [RAR] = Rara.
<b>ε sm</b>	Deformazione media nel calcestruzzo.
<b>Ae</b>	Area efficace del calcestruzzo teso [mm <sup>2</sup> ]
<b>sm</b>	Distanza media tra le fessure [mm].
<b>wk</b>	Apertura massima delle fessure [mm].
<b>σ ct</b>	Valore della tensione massima di trazione nel calcestruzzo [N/mm <sup>2</sup> ].
<b>σ cc</b>	Valore della tensione massima di compressione nel calcestruzzo [N/mm <sup>2</sup> ].
<b>σ at</b>	Valore della tensione massima di trazione nell'acciaio [N/mm <sup>2</sup> ].

## PIANI - VERIFICHE REGOLARITA' (Elevazione)

### REGOLARITÀ DELLA STRUTTURA IN PIANTA

La configurazione in pianta è compatta e approssimativamente simmetrica rispetto a due direzioni ortogonali, in relazione alla distribuzione di masse e rigidezze	SI
Il rapporto tra i lati di un rettangolo in cui l'edificio risulta inscritto è inferiore a 4	SI
Almeno una dimensione di eventuali rientri o sporgenze non supera il 25% della dimensione totale dell'edificio nella corrispondente direzione	SI
I solai possono essere considerati infinitamente rigidi nel loro piano rispetto agli elementi verticali e sufficientemente resistenti	SI

La struttura è regolare in pianta.

### REGOLARITÀ DELLA STRUTTURA IN ALTEZZA

Tutti i sistemi resistenti verticali dell'edificio (quali telai e pareti) si estendono per tutta l'altezza dell'edificio	NO
Massa e rigidezza rimangono costanti o variano gradualmente, senza bruschi cambiamenti, dalla base alla cima dell'edificio (le variazioni di massa da un piano all'altro non superano il 25%, la rigidezza non si abbassa da un piano al sovrastante più del 30% e non aumenta più del 10%); ai fini della rigidezza si possono considerare regolari in altezza strutture dotate di pareti o nuclei in c.a. di sezione costante sull'altezza o di telai controventati in acciaio, ai quali sia affidata almeno il 50% dell'azione sismica alla base	NO
Il rapporto tra resistenza effettiva e resistenza richiesta dal calcolo nelle strutture intelaiate progettate in Classe di Duttilità Bassa non è significativamente diverso per piani diversi (il rapporto fra la resistenza effettiva e quella richiesta calcolata ad un generico piano non deve differire più del 20% dall'analogo rapporto determinato per un altro piano); può fare eccezione l'ultimo piano di strutture intelaiate di almeno tre piani	NO
Eventuali restringimenti della sezione orizzontale dell'edificio avvengono in modo graduale da un piano al successivo, rispettando i seguenti limiti: ad ogni piano il rientro non supera il 30% della dimensione corrispondente al primo piano, né il 20% della dimensione corrispondente al piano immediatamente sottostante. Fa eccezione l'ultimo piano di edifici di almeno quattro piani per il quale non sono previste limitazioni di restringimento	NO

La struttura non è regolare in altezza.

Piano	Quota	Altezza	Piano rigido	Riduz - Tamp	Irreg. Tamp	Massa SLU	RgdSLU		REff		RRic	
	[m]	[m]				[N·s <sup>2</sup> /m]	X	Y	X	Y	X	Y
Piano Terra	-4.30	4.30	NO	NO	NO	317,751	35,317,39 8	52,900,33 7	0	0	0	0
Piano Fondo Vasca	-9.10	4.80	NO	NO	NO	343,376	13,514,31 6	21,304,37 4	0	0	0	0

## LEGENDA

<b>Riduz.Tamp</b>	Per i piani con riduzione dei tamponamenti, sono state incrementate le azioni di calcolo per gli elementi verticali (pilastri e pareti) di un fattore 1,4: [S] = Piano con riduzione dei tamponamenti - [N] = Piano senza riduzione dei tamponamenti.
<b>Irreg.Tamp.</b>	Per piani con distribuzione dei tamponamenti in pianta fortemente irregolare, l'eccentricità accidentale è stata incrementata di un fattore pari a 2: [S] = Distribuzione tamponamenti irregolare fortemente - [N] = Distribuzione tamponamenti regolare.
<b>Piano rigido</b>	[S] = Impalcato infinitamente rigido nel proprio piano - [N] = Impalcato deformabile.
<b>Massa SLU</b>	Massa del piano allo Stato Limite Ultimo.
<b>RgdSLU</b>	Valori delle Rigidezze di Piano, valutate allo SLU, riferite agli assi X ed Y del riferimento globale.
<b>REff</b>	Valori delle Resistenze Effettive di Piano, valutate allo SLU, relative al sistema di riferimento globale X, Y, Z.
<b>RRic</b>	Valori delle Resistenze Richieste di Piano, valutate allo SLU, relative al sistema di riferimento globale X, Y, Z.

## PIANI - VERIFICHE AGLI SPOSTAMENTI



Piani - Verifiche									
Piano	Quot a	Altez za	SxD	SyD	TpCol	Slim	Slim - SxD	Slim - SyD	Note
	[m]	[m]	[cm]	[cm]		[cm]	[cm]	[cm]	
Piano Terra	-4.30	4.30	0.00	0.01	R	2.1500	2.1453	2.1433	Verificato
Piano Fondo Vasca	-9.10	4.80	0.02	0.01	R	2.4000	2.3845	2.3918	Verificato

### LEGENDA Piani - Verifiche allo stato limite di danno/spostamenti

**SxD, SyD** Componenti dello spostamento differenziale rispetto al piano inferiore (Stato Limite di Danno), relative al sistema di riferimento globale X, Y, Z. Il calcolo viene condotto per tutte le coppie di punti allineate in verticale; si riportano i valori massimi.

**TpCol** Tipo di collegamento delle tamponature alla struttura: [R] = Rigido - [E] = Elastico.

**Slim** Valore limite dello spostamento differenziale indicato dalla normativa.

## PIANI - VERIFICHE ALLO SLO (Elevazione)

Piani - Verifiche allo SLO									
Piano	Quot a	Altez za	SpAmmSLO	SpDiffSLO		SpDiff		ClgTomp	Note
				X	Y	X	Y		
	[m]	[m]	[cm]	[cm]	[cm]	[cm]	[cm]		
Piano Terra	-4.30	4.30	1.43	0.00	0.01	1.43	1.43	R	Verificato
Piano Fondo Vasca	-9.10	4.80	1.60	0.01	0.01	1.59	1.59	R	Verificato

### LEGENDA Piani - Verifiche allo SLO

**SpAmmSLO** Spostamento Differenziale rispetto al Piano inferiore Ammissibile.

**SpDiffSLO** Spostamento Differenziale rispetto al Piano inferiore.

**SpDiff** Differenza fra SpAmmSLO e SpDiffSLO nelle direzioni X e Y.

**ClgTomp** Tipo di Collegamento delle Tamponature alla struttura.

## PIANI - EFFETTI DEL SECONDO ORDINE (Elevazione)

Piani - Effetti del secondo ordine										
Piano	Quota	Altezza	SxD	SyD	Pxθ	Pyθ	Txθ	Tyθ	θx	θy
	[m]	[m]	[cm]	[cm]	[N]	[N]	[N]	[N]		
Piano Terra	-4.30	4.30	0.0386	0.0259	4,035,308	4,035,308	1,364,771	1,368,896	0.0003	0.0002
Piano Fondo Vasca	-9.10	4.80	0.1423	0.0906	3.130.900	3.130.900	1.923.308	1.929.121	0.0011	0.0007

### LEGENDA Piani - Effetti del secondo ordine

**Nota: le forze sismiche orizzontali agenti sui piani caratterizzati da valori di θ compresi tra 0.1 e 0.2, sono state incrementate del fattore "1/(1-θ)", per portare in conto gli effetti del secondo ordine. [DM 2008 - par. 7.3.1].**

**SxD, SyD** Componenti dello spostamento differenziale rispetto al piano inferiore (Stato Limite Ultimo), relative al sistema di riferimento globale X, Y, Z. Il calcolo viene condotto per tutte le coppie di punti allineate in verticale; si riportano i valori massimi.

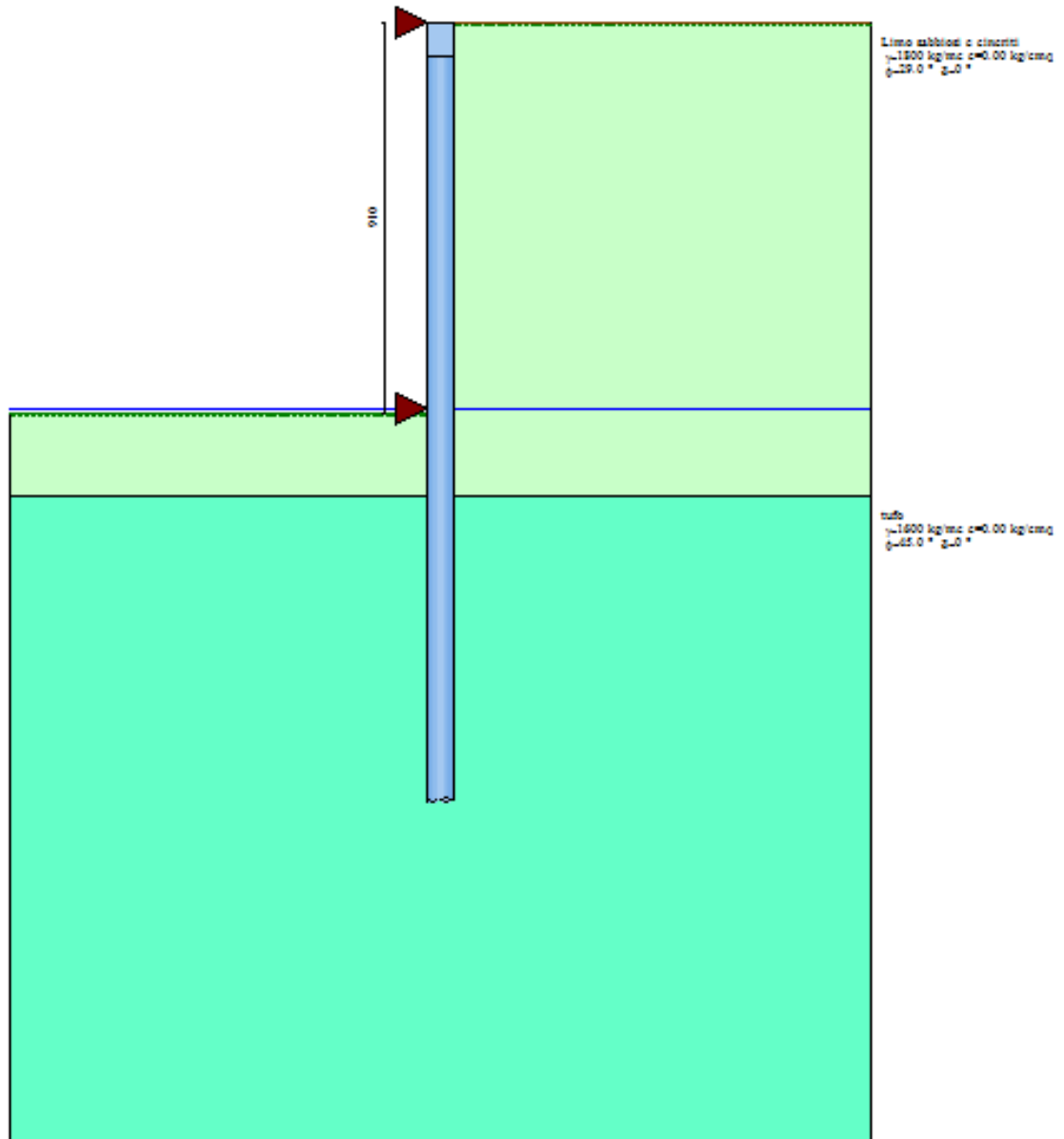
**Pxθ, Pyθ** Valori del carico verticale del piano utilizzato per il calcolo di "θ".

**Txθ, Tyθ** Valori del tagliante di piano utilizzati per il calcolo di "θ".

**θx, θy** Coefficienti "θ" del piano.



# PALIFICATA TIPO – A -



Metodo di analisi

## Calcolo della profondità di infissione

Nel caso generale l'equilibrio della paratia è assicurato dal bilanciamento fra la spinta attiva agente da monte sulla parte fuori terra, la resistenza passiva che si sviluppa da valle verso monte nella zona interrata e la controspinta che agisce da monte verso valle nella zona interrata al di sotto del centro di rotazione.

Nel caso di paratia tirantata nell'equilibrio della struttura intervengono gli sforzi dei tiranti (diretti verso monte); in questo caso, se la paratia non è sufficientemente infissa, la controspinta sarà assente.



Pertanto il primo passo da compiere nella progettazione è il calcolo della profondità di infissione necessaria ad assicurare l'equilibrio fra i carichi agenti (spinta attiva, resistenza passiva, contropinta, tiro dei tiranti ed eventuali carichi esterni).

Nel calcolo classico delle paratie si suppone che essa sia infinitamente rigida e che possa subire una rotazione intorno ad un punto (*Centro di rotazione*) posto al di sotto della linea di fondo scavo (per paratie non tirantate).

Occorre pertanto costruire i diagrammi di spinta attiva e di spinta (resistenza) passiva agenti sulla paratia. A partire da questi si costruiscono i diagrammi risultanti.

Nella costruzione dei diagrammi risultanti si adotterà la seguente notazione:

- $K_{am}$  diagramma della spinta attiva agente da monte
- $K_{av}$  diagramma della spinta attiva agente da valle sulla parte interrata
- $K_{pm}$  diagramma della spinta passiva agente da monte
- $K_{pv}$  diagramma della spinta passiva agente da valle sulla parte interrata.

Calcolati i diagrammi suddetti si costruiscono i diagrammi risultanti

$$D_m = K_{pm} - K_{av} \quad \text{e} \quad D_v = K_{pv} - K_{am}$$

Questi diagrammi rappresentano i valori limiti delle pressioni agenti sulla paratia. La soluzione è ricercata per tentativi facendo variare la profondità di infissione e la posizione del centro di rotazione fino a quando non si raggiunge l'equilibrio sia alla traslazione che alla rotazione.

Per mettere in conto un fattore di sicurezza nel calcolo delle profondità di infissione si può agire con tre modalità :

1. applicazione di un coefficiente moltiplicativo alla profondità di infissione strettamente necessaria per l'equilibrio
2. riduzione della spinta passiva tramite un coefficiente di sicurezza
3. riduzione delle caratteristiche del terreno tramite coefficienti di sicurezza su  $\tan(\phi)$  e sulla coesione

### **Calcolo della spinte**

#### Metodo di Culmann (metodo del cuneo di tentativo)

Il metodo di Culmann adotta le stesse ipotesi di base del metodo di Coulomb: cuneo di spinta a monte della parete che si muove rigidamente lungo una superficie di rottura rettilinea o spezzata (nel caso di terreno stratificato).

La differenza sostanziale è che mentre Coulomb considera un terrapieno con superficie a pendenza costante e carico uniformemente distribuito (il che permette di ottenere una espressione in forma chiusa per il valore della spinta) il metodo di Culmann consente di analizzare situazioni con profilo di forma generica e carichi sia concentrati che distribuiti comunque disposti. Inoltre, rispetto al metodo di Coulomb, risulta più immediato e lineare tener conto della coesione del masso spingente. Il metodo di Culmann, nato come metodo essenzialmente grafico, si è evoluto per essere trattato mediante analisi numerica (noto in questa forma come metodo del cuneo di tentativo).

I passi del procedimento risolutivo sono i seguenti:

- si impone una superficie di rottura (angolo di inclinazione  $\rho$  rispetto all'orizzontale) e si considera il cuneo di spinta delimitato dalla superficie di rottura stessa, dalla parete su cui si calcola la spinta e dal profilo del terreno;
- si valutano tutte le forze agenti sul cuneo di spinta e cioè peso proprio ( $W$ ), carichi sul terrapieno, resistenza per attrito e per coesione lungo la superficie di rottura ( $R$  e  $C$ ) e resistenza per coesione lungo la parete ( $A$ );



- dalle equazioni di equilibrio si ricava il valore della spinta  $S$  sulla parete.

Questo processo viene iterato fino a trovare l'angolo di rottura per cui la spinta risulta massima nel caso di spinta attiva e minima nel caso di spinta passiva.

Le pressioni sulla parete di spinta si ricavano derivando l'espressione della spinta  $S$  rispetto all'ordinata  $z$ . Noto il diagramma delle pressioni si ricava il punto di applicazione della spinta.

### Spinta in presenza di falda

Nel caso in cui a monte della parete sia presente la falda il diagramma delle pressioni risulta modificato a causa della sottospinta che l'acqua esercita sul terreno. Il peso di volume del terreno al di sopra della linea di falda non subisce variazioni. Viceversa al di sotto del livello di falda va considerato il peso di volume efficace

$$\gamma' = \gamma_{\text{sat}} - \gamma_w$$

dove  $\gamma_{\text{sat}}$  è il peso di volume saturo del terreno (dipendente dall'indice dei pori) e  $\gamma_w$  è il peso specifico dell'acqua. Quindi il diagramma delle pressioni al di sotto della linea di falda ha una pendenza minore. Al diagramma così ottenuto va sommato il diagramma triangolare legato alla pressione esercitata dall'acqua.

Il regime di filtrazione della falda può essere *idrostatico o idrodinamico*.

Nell'ipotesi di regime idrostatico sia la falda di monte che di valle viene considerata statica, la pressione in un punto a quota  $h$  al di sotto della linea freatica sarà dunque pari a:

$$\gamma_w \times h$$

### Spinta in presenza di sisma

Per tenere conto dell'incremento di spinta dovuta al sisma si fa riferimento al metodo di **Mononobe-Okabe** (cui fa riferimento la Normativa Italiana).

Il metodo di Mononobe-Okabe considera nell'equilibrio del cuneo spingente la forza di inerzia dovuta al sisma. Indicando con  $W$  il peso del cuneo e con  $C$  il coefficiente di intensità sismica la forza di inerzia valutata come

$$F_i = W \cdot C$$

Indicando con  $S$  la spinta calcolata in condizioni statiche e con  $S_s$  la spinta totale in condizioni sismiche l'incremento di spinta è ottenuto come

$$DS = S - S_s$$

L'incremento di spinta viene applicato a 2/3 dell'altezza della parete stessa (diagramma triangolare con vertice in basso).



## Analisi ad elementi finiti

La paratia è considerata come una struttura a prevalente sviluppo lineare (si fa riferimento ad un metro di larghezza) con comportamento a trave. Come caratteristiche geometriche della sezione si assume il momento d'inerzia  $I$  e l'area  $A$  per metro lineare di larghezza della paratia. Il modulo elastico è quello del materiale utilizzato per la paratia.

La parte fuori terra della paratia è suddivisa in elementi di lunghezza pari a circa 5 centimetri e più o meno costante per tutti gli elementi. La suddivisione è suggerita anche dalla eventuale presenza di tiranti, carichi e vincoli. Infatti questi elementi devono capitare in corrispondenza di un nodo. Nel caso di tirante è inserito un ulteriore elemento atto a schematizzarlo. Detta  $L$  la lunghezza libera del tirante,  $A_f$  l'area di armatura nel tirante ed  $E_s$  il modulo elastico dell'acciaio è inserito un elemento di lunghezza pari ad  $L$ , area  $A_f$ , inclinazione pari a quella del tirante e modulo elastico  $E_s$ . La parte interrata della paratia è suddivisa in elementi di lunghezza, come visto sopra, pari a circa 5 centimetri.

I carichi agenti possono essere di tipo distribuito (spinta della terra, diagramma aggiuntivo di carico, spinta della falda, diagramma di spinta sismica) oppure concentrati. I carichi distribuiti sono riportati sempre come carichi concentrati nei nodi (sotto forma di reazioni di incastro perfetto cambiate di segno).

## Schematizzazione del terreno

La modellazione del terreno si rifà al classico schema di Winkler. Esso è visto come un letto di molle indipendenti fra di loro reagenti solo a sforzo assiale di compressione. La rigidezza della singola molla è legata alla costante di sottofondo orizzontale del terreno (*costante di Winkler*). La costante di sottofondo,  $k$ , è definita come la pressione unitaria che occorre applicare per ottenere uno spostamento unitario. Dimensionalmente è espressa quindi come rapporto fra una pressione ed uno spostamento al cubo  $[F/L^3]$ . È evidente che i risultati sono tanto migliori quanto più è elevato il numero delle molle che schematizzano il terreno. Se ( $m$  è l'interasse fra le molle (in cm) e  $b$  è la larghezza della paratia in direzione longitudinale ( $b=100$  cm) occorre ricavare l'area equivalente,  $A_m$ , della molla (a cui si assegna una lunghezza pari a 100 cm). Indicato con  $E_m$  il modulo elastico del materiale costituente la paratia (in  $Kg/cm^2$ ), l'equivalenza, in termini di rigidezza, si esprime come

$$A_m = 10000 \times \frac{k \Delta_m}{E_m}$$

Per le molle di estremità, in corrispondenza della linea di fondo scavo ed in corrispondenza dell'estremità inferiore della paratia, si assume una area equivalente dimezzata. Inoltre, tutte le molle hanno, ovviamente, rigidezza flessionale e tagliante nulla e sono vincolate all'estremità alla traslazione. Quindi la matrice di rigidezza di tutto il sistema paratia-terreno sarà data dall'assemblaggio delle matrici di rigidezza degli elementi della paratia (elementi a rigidezza flessionale, tagliante ed assiale), delle matrici di rigidezza dei tiranti (solo rigidezza assiale) e delle molle (rigidezza assiale).

## Modalità di analisi e comportamento elasto-plastico del terreno



A questo punto vediamo come è effettuata l'analisi. Un tipo di analisi molto semplice e veloce sarebbe l'analisi elastica (peraltro disponibile nel programma **PAC**). Ma si intuisce che considerare il terreno con un comportamento infinitamente elastico è una approssimazione alquanto grossolana. Occorre quindi introdurre qualche correttivo che meglio ci aiuti a modellare il terreno. Fra le varie soluzioni possibili una delle più praticabili e che fornisce risultati soddisfacenti è quella di considerare il terreno con comportamento elasto-plastico perfetto. Si assume cioè che la curva sforzi-deformazioni del terreno abbia andamento bilatero. Rimane da scegliere il criterio di plasticizzazione del terreno (molle). Si può fare riferimento ad un criterio di tipo cinematico: la resistenza della molla cresce con la deformazione fino a quando lo spostamento non raggiunge il valore  $X_{\max}$ ; una volta superato tale spostamento limite non si ha più incremento di resistenza all'aumentare degli spostamenti. Un altro criterio può essere di tipo statico: si assume che la molla abbia una resistenza crescente fino al raggiungimento di una pressione  $p_{\max}$ . Tale pressione  $p_{\max}$  può essere imposta pari al valore della pressione passiva in corrispondenza della quota della molla. D'altronde un ulteriore criterio si può ottenere dalla combinazione dei due descritti precedentemente: plasticizzazione o per raggiungimento dello spostamento limite o per raggiungimento della pressione passiva. Dal punto di vista strettamente numerico è chiaro che l'introduzione di criteri di plasticizzazione porta ad analisi di tipo non lineare (non linearità meccaniche). Questo comporta un aggravio computazionale non indifferente. L'entità di tale aggravio dipende poi dalla particolare tecnica adottata per la soluzione. Nel caso di analisi elastica lineare il problema si risolve immediatamente con la soluzione del sistema fondamentale ( $K$  matrice di rigidezza,  $u$  vettore degli spostamenti nodali,  $p$  vettore dei carichi nodali)

$$Ku=p$$

Un sistema non lineare, invece, deve essere risolto mediante un'analisi al passo per tener conto della plasticizzazione delle molle. Quindi si procede per passi di carico, a partire da un carico iniziale  $p_0$ , fino a raggiungere il carico totale  $p$ . Ogni volta che si incrementa il carico si controllano eventuali plasticizzazioni delle molle. Se si hanno nuove plasticizzazioni la matrice globale andrà riassemblata escludendo il contributo delle molle plasticizzate. Il procedimento descritto se fosse applicato in questo modo sarebbe particolarmente gravoso (la fase di decomposizione della matrice di rigidezza è particolarmente onerosa). Si ricorre pertanto a soluzioni più sofisticate che escludono il riassemblaggio e la decomposizione della matrice, ma usano la matrice elastica iniziale (*metodo di Riks*).

Senza addentrarci troppo nei dettagli diremo che si tratta di un metodo di Newton-Raphson modificato e ottimizzato. L'analisi condotta secondo questa tecnica offre dei vantaggi immediati. Essa restituisce l'effettiva deformazione della paratia e le relative sollecitazioni; dà informazioni dettagliate circa la deformazione e la pressione sul terreno. Infatti la deformazione è direttamente leggibile, mentre la pressione sarà data dallo sforzo nella molla diviso per l'area di influenza della molla stessa. Sappiamo quindi quale è la zona di terreno effettivamente plasticizzato. Inoltre dalle deformazioni ci si può rendere conto di un possibile meccanismo di rottura del terreno.



## Analisi per fasi di scavo

L'analisi della paratia per fasi di scavo consente di ottenere informazioni dettagliate sullo stato di sollecitazione e deformazione dell'opera durante la fase di realizzazione. In ogni fase lo stato di sollecitazione e di deformazione dipende dalla 'storia' dello scavo (soprattutto nel caso di paratie tirantate o vincolate).

Definite le varie altezze di scavo (in funzione della posizione di tiranti, vincoli, o altro) si procede per ogni fase al calcolo delle spinte inserendo gli elementi (tiranti, vincoli o carichi) attivi per quella fase, tenendo conto delle deformazioni dello stato precedente. Ad esempio, se sono presenti dei tiranti passivi si inserirà nell'analisi della fase la 'molla' che lo rappresenta. Indicando con  $u$  ed  $u_0$  gli spostamenti nella fase attuale e nella fase precedente, con  $s$  ed  $s_0$  gli sforzi nella fase attuale e nella fase precedente e con  $K$  la matrice di rigidezza della 'struttura' la relazione sforzi-deformazione è esprimibile nella forma

$$s = s_0 + K(u - u_0)$$

In sostanza analizzare la paratia per fasi di scavo oppure 'direttamente' porta a risultati abbastanza diversi sia per quanto riguarda lo stato di deformazione e sollecitazione dell'opera sia per quanto riguarda il tiro dei tiranti.

## Verifica alla stabilità globale

La verifica alla stabilità globale del complesso paratia+terreno deve fornire un coefficiente di sicurezza non inferiore a 1.30.

È usata la tecnica della suddivisione a strisce della superficie di scorrimento da analizzare. La superficie di scorrimento è supposta circolare.

In particolare il programma esamina, per un dato centro 3 cerchi differenti: un cerchio passante per la linea di fondo scavo, un cerchio passante per il piede della paratia ed un cerchio passante per il punto medio della parte interrata. Si determina il minimo coefficiente di sicurezza su una maglia di centri di dimensioni 6x6 posta in prossimità della sommità della paratia. Il numero di strisce è pari a 50.

Il coefficiente di sicurezza fornito da Fellenius si esprime secondo la seguente formula:

$$\eta = \frac{\sum_i \left( \frac{c_i b_i}{\cos \alpha_i} + [W_i \cos \alpha_i - u_i l_i] \tan \phi_i \right)}{\sum_i W_i \sin \alpha_i}$$

dove  $n$  è il numero delle strisce considerate,  $b_i$  e  $\alpha_i$  sono la larghezza e l'inclinazione della base della striscia  $i$ -esima rispetto all'orizzontale,  $W_i$  è il peso della striscia  $i$ -esima e  $c_i$  e  $\phi_i$  sono le caratteristiche del terreno (coesione ed angolo di attrito) lungo la base della striscia.

Inoltre  $u_i$  ed  $l_i$  rappresentano la pressione neutra lungo la base della striscia e la lunghezza della base della striscia ( $l_i = b_i / \cos \alpha_i$ ).



Quindi, assunto un cerchio di tentativo si suddivide in  $n$  strisce e dalla formula precedente si ricava  $\eta$ . Questo procedimento è eseguito per il numero di centri prefissato e è assunto come coefficiente di sicurezza della scarpata il minimo dei coefficienti così determinati.

## Geometria paratia

### Tipo paratia: **Paratia di pali**

Altezza fuori terra	9.10	[m]
Profondità di infissione	9.00	[m]
Altezza totale della paratia	18.10	[m]
Lunghezza paratia	19.10	[m]

Numero di file di pali	1	
Interasse fra i pali della fila	0.60	[m]
Diametro dei pali	60.00	[cm]
Numero totale di pali	31	
Numero di pali per metro lineare	1.62	

## Geometria cordoli

### *Simbologia adottata*

$n^\circ$	numero d'ordine del cordolo
Y	posizione del cordolo sull'asse della paratia espresso in [m]

#### Cordoli in calcestruzzo

B	Base della sezione del cordolo espresso in [cm]
H	Altezza della sezione del cordolo espresso in [cm]

#### Cordoli in acciaio

A	Area della sezione in acciaio del cordolo espresso in [cmq]
W	Modulo di resistenza della sezione del cordolo espresso in [cm <sup>3</sup> ]

$n^\circ$	Y	Tipo	B	H	A	W
1	0.00	Calcestruzzo	60.00	80.00	--	--

## Geometria profilo terreno

### *Simbologia adottata e sistema di riferimento*

(Sistema di riferimento con origine in testa alla paratia, ascissa X positiva verso monte, ordinata Y positiva verso l'alto)

N	numero ordine del punto
X	ascissa del punto espressa in [m]
Y	ordinata del punto espressa in [m]
A	inclinazione del tratto espressa in [°]

### **Profilo di monte**

N	X	Y	A
2	10.00	0.00	0.00

### **Profilo di valle**

N	X	Y	A
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1	-10.00	-9.10	0.00
2	0.00	-9.10	0.00

## Descrizione terreni

### *Simbologia adottata*

n°	numero d'ordine dello strato a partire dalla sommità della paratia
Descrizione	Descrizione del terreno
$\gamma$	peso di volume del terreno espresso in [kg/mc]
$\gamma_s$	peso di volume saturo del terreno espresso [kg/mc]
$\phi$	angolo d'attrito interno del terreno espresso in [°]
$\delta$	angolo d'attrito terreno/paratia espresso in [°]
c	coesione del terreno espressa in [kg/cm <sup>2</sup> ]

n°	Descrizione	$\gamma$	$\gamma_s$	$\phi$	$\delta$	c
1	Limo sabbiosi e cineriti	1800.00	1900.00	29.00	0.00	0.000
2	tufo	1600.00	2000.00	45.00	0.00	0.000

## Descrizione stratigrafia

### *Simbologia adottata*

n°	numero d'ordine dello strato a partire dalla sommità della paratia
sp	spessore dello strato in corrispondenza dell'asse della paratia espresso in [m]
kw	costante di Winkler orizzontale espressa in Kg/cm <sup>2</sup> /cm
$\alpha$	inclinazione dello strato espressa in GRADI(°)
Terreno	Terreno associato allo strato

n°	sp	$\alpha$	kw	Terreno
1	11.00	0.00	1.67	Limo sabbiosi e cineriti
2	15.00	0.00	11.99	tufo

## Falda

Profondità della falda a monte rispetto alla sommità della paratia	9.00	[m]
Profondità della falda a valle rispetto alla sommità della paratia	9.00	[m]
Regime delle pressioni neutre:	<b>Idrostatico</b>	

## Caratteristiche materiali utilizzati

### *Calcestruzzo*

Peso specifico	2500	[kg/mc]
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Classe di Resistenza	C25/30	
Resistenza caratteristica a compressione $R_{bk}$	306	[kg/cm <sup>2</sup> ]
Tensione di progetto a compressione $\sigma_c$	99	[kg/cm <sup>2</sup> ]
Tensione tangenziale ammissibile $\tau_{c0}$	6.1	[kg/cm <sup>2</sup> ]
Tensione tangenziale ammissibile $\tau_{c1}$	18.5	[kg/cm <sup>2</sup> ]

#### **Acciaio**

Tipo	B450C	
Tensione ammissibile $\sigma_{fa}$	4589	[kg/cm <sup>2</sup> ]
Tensione di snervamento $f_{yk}$	4589	[kg/cm <sup>2</sup> ]

#### **Caratteristiche acciaio cordoli in c.a.**

Tipo	B450C	
Tensione ammissibile $\sigma_{fa}$	4589	[kg/cm <sup>2</sup> ]
Tensione di snervamento $f_{yk}$	4589	[kg/cm <sup>2</sup> ]

### Condizioni di carico

#### *Simbologia e convenzioni adottate*

Le ascisse dei punti di applicazione del carico sono espresse in [m] rispetto alla testa della paratia

Le ordinate dei punti di applicazione del carico sono espresse in [m] rispetto alla testa della paratia

$F_x$  Forza orizzontale espressa in [kg], positiva da monte verso valle

$F_y$  Forza verticale espressa in [kg], positiva verso il basso

$M$  Momento espresso in [kgm], positivo ribaltante

$Q_i, Q_f$  Intensità dei carichi distribuiti sul profilo espresse in [kg/mq]

$V_i, V_s$  Intensità dei carichi distribuiti sulla paratia espresse in [kg/mq], positivi da monte verso valle

$R$  Risultante carico distribuito sulla paratia espressa in [kg]

#### Condizione n° 1

Carico distribuito sul profilo       $X_i = 1.00$        $X_f = 5.00$        $Q_i = 500$        $Q_f = 500$

### Vincoli lungo l'altezza della paratia

#### *Simbologia adottata*

$n^\circ$  numero d'ordine del vincolo

$Y$  ordinata del vincolo rispetto alla testa della paratia espressa in [m]

$V_x$  Vincolo in direzione orizzontale

$K_x$  Rigidezza vincolo in direzione orizzontale espressa in [Kg/cm]

$V_r$  Vincolo alla rotazione

$K_r$  Rigidezza vincolo alla rotazione espressa in [Kgm/°]

$n^\circ$	$Y$	$V_x$	$K_x$	$V_r$	$K_r$
1	9.00	V. RIGIDO	--	LIBERO	--
2	0.00	V. RIGIDO	--	LIBERO	--



## Combinazioni di carico

Nella tabella sono riportate le condizioni di carico di ogni combinazione con il relativo coefficiente di partecipazione.

### Combinazione n° 1

Spinta terreno

### Combinazione n° 2

Spinta terreno

Condizione 1 (folla addensata) x 1.00

### Combinazione n° 3

Spinta terreno

### Combinazione n° 4

Spinta terreno

Condizione 1 (folla addensata) x 1.00

## Impostazioni di progetto

### Spinte e verifiche secondo :

- D.M. 11/03/1988

- D.M. 16/01/1996

### Verifica materiali

Tensioni ammissibili

Impostazioni di analisi

## **Analisi per Combinazioni di Carico.**

Rottura del terreno: Pressione passiva

Influenza  $\delta$  (angolo di attrito terreno-paratia): Nel calcolo del coefficiente di spinta attiva  $K_a$  e nell'inclinazione della spinta attiva (non viene considerato per la spinta passiva)

Stabilità globale: Metodo di Fellenius



## Impostazioni analisi sismica

Coefficiente di intensità sismica (percento) 7.00

Forma del diagramma di incremento sismico triangolare con vertice in basso sulla parte fuori terra

Influenza sisma nella spinta attiva da monte

## Analisi della paratia

### L'analisi è stata eseguita per combinazioni di carico

La paratia è analizzata con il metodo degli elementi finiti.

Essa è discretizzata in 182 elementi fuori terra e 180 elementi al di sotto della linea di fondo scavo.

Le molle che simulano il terreno hanno un comportamento elastoplastico: una volta raggiunta la pressione passiva non reagiscono ad ulteriori incremento di carico.

Altezza fuori terra della paratia	9.10	[m]
Profondità di infissione	9.00	[m]
Altezza totale della paratia	18.10	[m]

## Forze agenti sulla paratia

Tutte le forze si intendono positive se dirette da monte verso valle. Esse sono riferite ad un metro di larghezza della paratia. Le Y hanno come origine la testa della paratia, e sono espresse in [m]

### Simbologia adottata

n°	Indice della Combinazione/Fase
Tipo	Tipo della Combinazione/Fase
Pa	Spinta attiva, espressa in [kg]
Is	Incremento sismico della spinta, espressa in [kg]
Pw	Spinta della falda, espressa in [kg]
Pp	Resistenza passiva, espressa in [kg]
Pc	Controspinta, espressa in [kg]

n°	Pa	Y <sub>Pa</sub>	Is	Y <sub>Is</sub>	Pw	Y <sub>Pw</sub>	Pp	Y <sub>Pp</sub>	Pc	Y <sub>Pc</sub>
1	33389	6.93	--	--	0	0.00	-561	16.52	7450	11.81
2	34649	6.87	--	--	0	0.00	-598	16.52	7945	11.81
3	33572	7.03	4686	3.03	0	0.00	-668	16.52	8904	11.81
4	34831	6.97	4675	3.03	0	0.00	-704	16.53	9396	11.81

### Simbologia adottata

n°	Indice della Combinazione/Fase
Tipo	Tipo della Combinazione/Fase
Rc	Risultante carichi esterni applicati, espressa in [kg]
Rt	Risultante delle reazioni dei tiranti (componente orizzontale), espressa in [kg]
Rv	Risultante delle reazioni dei vincoli, espressa in [kg]
Rp	Risultante delle reazioni dei puntoni, espressa in [kg]

n°	Rc	Y <sub>Rc</sub>	Rt	Y <sub>Rt</sub>	Rv	Y <sub>Rv</sub>	Rp	Y <sub>Rp</sub>
1	0	0.00	--	---	40278	7.70	--	--



2	0	0.00	--	---41996	7.67	--	--
3	0	0.00	--	---46494	7.41	--	--
4	0	0.00	--	---48198	7.39	--	--

### *Simbologia adottata*

n°	Indice della Combinazione/Fase
P <sub>NUL</sub>	Punto di nullo del diagramma, espresso in [m]
P <sub>INV</sub>	Punto di inversione del diagramma, espresso in [m]
C <sub>ROT</sub>	Punto Centro di rotazione, espresso in [m]
MP	Percentuale molle plasticizzate, espressa in [%]
R/R <sub>MAX</sub>	Rapporto tra lo sforzo reale nelle molle e lo sforzo che le molle sarebbero in grado di esprimere, espresso in [%]
Pp	Portanza di punta, espressa in [kg]

n°	P <sub>NUL</sub>	P <sub>INV</sub>	C <sub>ROT</sub>	MP	R/R <sub>MAX</sub>	Pp
1	10.99	16.25	14.73	0.00	1.23	477537
2	10.99	16.25	14.73	0.00	1.31	477537
3	10.99	16.30	14.74	0.00	1.48	477537
4	10.99	16.30	14.74	0.00	1.55	477537

### Risultati vincoli

### *Simbologia adottata*

n°	Indice del vincolo
Y	posizione del vincolo rispetto alla testa della paratia espressa in [m]
R <sub>x</sub> /ml	reazione in direzione orizzontale a metro lineare, positiva verso valle, espressa in [kg]
R <sub>θ</sub> /ml	reazione momento a metro lineare, positiva antioraria, espressa in [kgm]
u	spostamento orizzontale, positivo verso valle, espresso in [cm]

### **Combinazione n° 1**

n°	Y	R <sub>x</sub>	R <sub>θ</sub>	u
1	9.00	-34441.60	--	0.00
2	0.00	-5835.91	--	0.00

### **Combinazione n° 2**

n°	Y	R <sub>x</sub>	R <sub>θ</sub>	u
1	9.00	-35774.14	--	0.00
2	0.00	-6222.15	--	0.00

### **Combinazione n° 3**

n°	Y	R <sub>x</sub>	R <sub>θ</sub>	u
1	9.00	-38273.07	--	0.00
2	0.00	-8220.59	--	0.00

### **Combinazione n° 4**



<b>n°</b>	<b>Y</b>	<b>R<sub>x</sub></b>	<b>R<sub>θ</sub></b>	<b>u</b>
1	9.00	-39597.01	--	0.00
2	0.00	-8601.47	--	0.00

Valori massimi e minimi sollecitazioni per metro di paratia

#### *Simbologia adottata*

n°	Indice della combinazione/fase
Tipo	Tipo della combinazione/fase
Y	ordinata della sezione rispetto alla testa espressa in [m]
M	momento flettente massimo e minimo espresso in [kgm]
N	sforzo normale massimo e minimo espresso in [kg] (positivo di compressione)
T	taglio massimo e minimo espresso in [kg]

<b>n°</b>	<b>M</b>	<b>Y<sub>M</sub></b>	<b>T</b>	<b>Y<sub>T</sub></b>	<b>N</b>	<b>Y<sub>N</sub></b>	
1	23361	9.00	19458	9.00	20765	18.10	MAX
--	-16818	4.30	-14983	9.00	0	0.00	MIN
2	24556	9.00	20279	9.00	20765	18.10	MAX
--	-17848	4.30	-15495	9.00	0	0.00	MIN
3	26993	9.00	21604	9.00	20765	18.10	MAX
--	-20261	4.15	-16669	9.00	0	0.00	MIN
4	28180	9.00	22420	9.00	20765	18.10	MAX
--	-21292	4.15	-17177	9.00	0	0.00	MIN

Spostamenti massimi e minimi della paratia

#### *Simbologia adottata*

n°	Indice della combinazione/fase
Tipo	Tipo della combinazione/fase
Y	ordinata della sezione rispetto alla testa della paratia espressa in [m]
U	spostamento orizzontale massimo e minimo espresso in [cm] positivo verso valle
V	spostamento verticale massimo e minimo espresso in [cm] positivo verso il basso

<b>n°</b>	<b>U</b>	<b>Y<sub>U</sub></b>	<b>V</b>	<b>Y<sub>V</sub></b>	
1	0.3761	4.30	0.0130	0.00	MAX
--	-0.0382	10.45	0.0000	0.00	MIN
2	0.3989	4.25	0.0130	0.00	MAX
--	-0.0407	10.45	0.0000	0.00	MIN
3	0.4531	4.20	0.0130	0.00	MAX
--	-0.0455	10.45	0.0000	0.00	MIN
4	0.4757	4.20	0.0130	0.00	MAX
--	-0.0479	10.45	0.0000	0.00	MIN



## Stabilità globale

### Metodo di Fellenius

Numero di cerchi analizzati 100

#### Simbologia adottata

n°	Indice della combinazione/fase
Tipo	Tipo della combinazione/fase
(X <sub>C</sub> ; Y <sub>C</sub> )	Coordinate centro cerchio superficie di scorrimento, espresse in [m]
R	Raggio cerchio superficie di scorrimento, espresso in [m]
(X <sub>V</sub> ; Y <sub>V</sub> )	Coordinate intersezione del cerchio con il pendio a valle, espresse in [m]
(X <sub>M</sub> ; Y <sub>M</sub> )	Coordinate intersezione del cerchio con il pendio a monte, espresse in [m]
FS	Coefficiente di sicurezza

n°	(X <sub>C</sub> , Y <sub>C</sub> )	R	(X <sub>V</sub> , Y <sub>V</sub> )	(X <sub>M</sub> , Y <sub>M</sub> )	FS
1	(-5.43; 0.00)	18.90	(-22.00; -9.08)	(13.47; 0.00)	2.31
2	(-5.43; 0.00)	18.90	(-22.00; -9.08)	(13.47; 0.00)	2.31
3	(-5.43; 0.00)	18.90	(-22.00; -9.08)	(13.47; 0.00)	1.93
4	(-7.24; 0.00)	19.49	(-24.49; -9.08)	(12.25; 0.00)	1.93

### Combinazione n° 4

Numero di strisce 50

#### Simbologia adottata

Le ascisse X sono considerate positive verso monte	
Le ordinate Y sono considerate positive verso l'alto	
Origine in testa alla paratia (spigolo contro terra)	
Le strisce sono numerate da monte verso valle	
N°	numero d'ordine della striscia
W	peso della striscia espresso in [kg]
α	angolo fra la base della striscia e l'orizzontale espresso in gradi (positivo antiorario)
φ	angolo d'attrito del terreno lungo la base della striscia
c	coesione del terreno lungo la base della striscia espressa in [kg/cmq]
b	larghezza della striscia espressa in [m]
L	sviluppo della base della striscia espressa in [m] ( $L=b/\cos\alpha$ )
u	pressione neutra lungo la base della striscia espressa in [kg/cmq]
Ctn, Ctt	contributo alla striscia normale e tangenziale del tirante espresse in [kg]

### Caratteristiche delle strisce

N°	W	α(°)	Wsinα	L	φ	c	u	(Ctn; Ctt)
1	957.23	-60.05	-829.38	1.49	29.00	0.000	0.073	(0; 0)
2	2645.67	-55.92	-2191.19	1.32	37.00	0.000	0.192	(0; 0)
3	4155.86	-52.19	-3283.33	1.21	45.00	0.000	0.295	(0; 0)
4	5493.69	-48.76	-4130.79	1.13	45.00	0.000	0.385	(0; 0)
5	6683.09	-45.54	-4770.37	1.06	45.00	0.000	0.465	(0; 0)
6	7749.15	-42.51	-5236.04	1.01	45.00	0.000	0.537	(0; 0)
7	8709.72	-39.61	-5553.26	0.96	45.00	0.000	0.601	(0; 0)
8	9578.01	-36.83	-5742.03	0.93	45.00	0.000	0.660	(0; 0)
9	10364.12	-34.15	-5818.55	0.90	45.00	0.000	0.713	(0; 0)
10	11075.94	-31.56	-5796.34	0.87	45.00	0.000	0.761	(0; 0)



11	11719.78	-29.03	-5686.95	0.85	45.00	0.000	0.804	(0; 0)
12	12300.72	-26.56	-5500.42	0.83	45.00	0.000	0.843	(0; 0)
13	12822.92	-24.15	-5245.64	0.81	45.00	0.000	0.878	(0; 0)
14	13289.83	-21.78	-4930.59	0.80	45.00	0.000	0.910	(0; 0)
15	13704.29	-19.45	-4562.52	0.79	45.00	0.000	0.938	(0; 0)
16	14068.66	-17.15	-4148.14	0.78	45.00	0.000	0.962	(0; 0)
17	14384.91	-14.88	-3693.66	0.77	45.00	0.000	0.984	(0; 0)
18	14654.65	-12.63	-3204.94	0.76	45.00	0.000	1.002	(0; 0)
19	14879.21	-10.41	-2687.52	0.75	45.00	0.000	1.017	(0; 0)
20	15059.66	-8.20	-2146.72	0.75	45.00	0.000	1.029	(0; 0)
21	15196.82	-6.00	-1587.65	0.75	45.00	0.000	1.038	(0; 0)
22	15291.32	-3.81	-1015.31	0.74	45.00	0.000	1.045	(0; 0)
23	15343.57	-1.62	-434.59	0.74	45.00	0.000	1.048	(0; 0)
24	15353.81	0.56	149.71	0.74	45.00	0.000	1.049	(0; 0)
25	15322.07	2.74	732.78	0.74	45.00	0.000	1.047	(0; 0)
26	15248.22	4.93	1309.82	0.74	45.00	0.000	1.042	(0; 0)
27	15131.93	7.12	1875.97	0.75	45.00	0.000	1.034	(0; 0)
28	14972.69	9.33	2426.31	0.75	45.00	0.000	1.023	(0; 0)
29	14769.76	11.54	2955.79	0.76	45.00	0.000	1.010	(0; 0)
30	14522.21	13.78	3459.19	0.76	45.00	0.000	0.993	(0; 0)
31	14228.83	16.04	3931.09	0.77	45.00	0.000	0.973	(0; 0)
32	13888.16	18.32	4365.78	0.78	45.00	0.000	0.950	(0; 0)
33	13498.40	20.64	4757.24	0.79	45.00	0.000	0.924	(0; 0)
34	24432.71	22.95	9527.73	0.78	45.00	0.000	0.895	(0; 0)
35	24188.18	25.27	10327.03	0.80	45.00	0.000	0.862	(0; 0)
36	23810.31	27.64	11046.42	0.81	45.00	0.000	0.827	(0; 0)
37	23237.44	30.06	11640.21	0.83	45.00	0.000	0.787	(0; 0)
38	22605.14	32.54	12159.68	0.86	45.00	0.000	0.743	(0; 0)
39	21908.48	35.09	12595.43	0.88	45.00	0.000	0.695	(0; 0)
40	21118.43	37.73	12922.55	0.91	45.00	0.000	0.641	(0; 0)
41	19935.80	40.46	12936.54	0.95	45.00	0.000	0.583	(0; 0)
42	19002.85	43.31	13034.38	0.99	45.00	0.000	0.518	(0; 0)
43	17969.38	46.30	12990.62	1.04	45.00	0.000	0.446	(0; 0)
44	16818.16	49.46	12781.07	1.11	45.00	0.000	0.367	(0; 0)
45	15524.95	52.84	12373.38	1.19	45.00	0.000	0.277	(0; 0)
46	14074.65	56.52	11739.27	1.31	37.00	0.000	0.175	(0; 0)
47	12449.64	60.60	10846.11	1.47	29.00	0.000	0.056	(0; 0)
48	10562.62	65.29	9595.58	1.72	29.00	0.000	0.000	(0; 0)
49	8180.50	71.10	7739.38	2.23	29.00	0.000	0.000	(0; 0)
50	3407.36	82.19	3375.72	5.30	29.00	0.000	0.000	(0; 0)

Resistenza a taglio paratia= 0.00 [kg]

$\Sigma W_i = 696291.51$  [kg]

$\Sigma W_i \sin \alpha_i = 125398.86$  [kg]

$\Sigma W_i \cos \alpha_i \tan \phi_i = 583543.66$  [kg]

$\Sigma c_i b_i / \cos \alpha_i = 0.00$  [kg]



## Descrizione armatura pali e caratteristiche sezione

Diametro del palo	60.00	[cm]
Area della sezione trasversale	2827.43	[cmq]
Copriferro	3.00	[cm]

L'armatura del palo è costituita da 15 $\phi$ 20( $A_f=47.12$  cmq) longitudinali e staffe  $\phi$ 12/20.0 cm.

## Verifica armatura paratia (Sezioni critiche)

### Simbologia adottata

$n^\circ$	Indice della combinazione/fase
$Y$	ordinata della sezione rispetto alla testa della paratia espressa in [m]
$\sigma_c$	tensione nel calcestruzzo, espressa in [kg/cmq]
$\sigma_f$	tensione nell'armatura longitudinale del palo, espressa in [kg/cmq]
$\tau_c$	tensione tangenziale nel calcestruzzo, espresso in [kg/cmq]
$\sigma_{st}$	tensione nell'armatura trasversale, espresso in [kg/cmq]

$n^\circ$	$\sigma_c$	$Y(\sigma_c)$	$\sigma_f$	$Y(\sigma_f)$	$\tau_c$	$Y(\tau_c)$	$\sigma_{st}$	$Y(\sigma_{st})$
1	79.52	9.001885.76	9.00	9.00	5.58	9.001973.19	9.00	9.00
2	83.57	9.001989.81	9.00	9.00	5.81	9.002056.03	9.00	9.00
3	91.80	9.002201.92	9.00	9.00	6.19	9.002189.72	9.00	9.00
4	95.81	9.002305.28	9.00	9.00	6.42	9.002272.14	9.00	9.00

## Verifica armatura paratia (Inviluppo)

### Simbologia adottata

$n^\circ$	Indice della combinazione/fase
$Y$	ordinata della sezione, espressa in [m]
$\sigma_c$	tensione massima nel calcestruzzo, espressa in [kg/cmq]
$\sigma_f$	tensione massima nei ferri longitudinali, espressa in [kg/cmq]
$\sigma_{st}$	tensione massima nei ferri trasversali, espressa in [kg/cmq]

$Y$	$\sigma_c$	$n^\circ$	$\sigma_f$	$n^\circ$	$\tau_c$	$n^\circ$	$\sigma_{st}$	$n^\circ$
0.00	0.00	1	0.00	1	1.87	4	662.92	4
0.05	1.45	4	36.54	4	2.45	4	866.28	4
0.10	2.90	4	72.88	4	2.44	4	861.77	4
0.15	4.34	4	109.03	4	2.42	4	857.12	4
0.20	5.77	4	144.97	4	2.41	4	852.33	4
0.25	7.19	4	180.71	4	2.40	4	847.41	4
0.30	8.60	4	216.23	4	2.38	4	842.35	4
0.35	10.01	4	251.53	4	2.37	4	837.15	4
0.40	11.40	4	286.60	4	2.35	4	831.81	4
0.45	12.79	4	321.44	4	2.34	4	826.33	4
0.50	14.17	4	356.04	4	2.32	4	820.71	4
0.55	15.53	4	390.40	4	2.30	4	814.96	4
0.60	16.89	4	424.51	4	2.29	4	809.06	4



0.65	18.24	4	458.36	4	2.27	4	803.03	4
0.70	19.58	4	491.94	4	2.25	4	796.86	4
0.75	20.91	4	525.26	4	2.24	4	790.55	4
0.80	22.23	4	558.31	4	2.22	4	784.10	4
0.85	23.53	4	591.07	4	2.20	4	777.52	4
0.90	24.83	4	623.55	4	2.18	4	770.79	4
0.95	26.11	4	655.73	4	2.16	4	763.93	4
1.00	27.38	4	687.62	4	2.14	4	756.93	4
1.05	28.64	4	719.20	4	2.12	4	749.79	4
1.10	29.89	4	750.47	4	2.10	4	742.51	4
1.15	31.13	4	781.43	4	2.08	4	735.09	4
1.20	32.35	4	812.06	4	2.06	4	727.54	4
1.25	33.56	4	842.37	4	2.04	4	719.84	4
1.30	34.76	4	872.34	4	2.01	4	712.01	4
1.35	35.95	4	901.97	4	1.99	4	704.00	4
1.40	37.12	4	931.25	4	1.97	4	695.78	4
1.45	38.28	4	960.17	4	1.94	4	687.30	4
1.50	39.42	4	988.72	4	1.92	4	678.50	4
1.55	40.55	4	1016.89	4	1.89	4	669.43	4
1.60	41.66	4	1044.66	4	1.87	4	660.12	4
1.65	42.76	4	1072.03	4	1.84	4	650.61	4
1.70	43.84	4	1098.98	4	1.81	4	640.96	4
1.75	44.90	4	1125.51	4	1.78	4	631.15	4
1.80	45.95	4	1151.62	4	1.76	4	621.19	4
1.85	46.98	4	1177.30	4	1.73	4	611.09	4
1.90	48.00	4	1202.54	4	1.70	4	600.84	4
1.95	49.00	4	1227.34	4	1.67	4	590.45	4
2.00	49.98	4	1251.68	4	1.64	4	579.91	4
2.05	50.94	4	1275.57	4	1.61	4	569.22	4
2.10	51.88	4	1299.00	4	1.58	4	558.39	4
2.15	52.81	4	1321.95	4	1.55	4	547.42	4
2.20	53.72	4	1344.43	4	1.52	4	536.30	4
2.25	54.61	4	1366.43	4	1.48	4	525.04	4
2.30	55.48	4	1387.95	4	1.45	4	513.64	4
2.35	56.33	4	1408.97	4	1.42	4	502.09	4
2.40	57.16	4	1429.48	4	1.39	4	490.41	4
2.45	57.97	4	1449.50	4	1.35	4	478.58	4
2.50	58.76	4	1469.00	4	1.32	4	466.60	4
2.55	59.53	4	1487.98	4	1.29	4	454.49	4
2.60	60.29	4	1506.44	4	1.25	4	442.24	4
2.65	61.02	4	1524.37	4	1.22	4	429.84	4
2.70	61.73	4	1541.76	4	1.18	4	417.30	4
2.75	62.42	4	1558.61	4	1.14	4	404.62	4
2.80	63.08	4	1574.91	4	1.11	4	391.80	4
2.85	63.73	4	1590.65	4	1.07	4	378.84	4
2.90	64.36	4	1605.84	4	1.03	4	365.74	4
2.95	64.96	4	1620.46	4	1.00	4	352.50	4
3.00	65.54	4	1634.50	4	0.96	4	339.12	4
3.05	66.10	4	1647.97	4	0.92	4	325.60	4
3.10	66.63	4	1660.85	4	0.88	4	311.94	4
3.15	67.14	4	1673.15	4	0.84	4	298.14	4
3.20	67.63	4	1684.84	4	0.80	4	284.20	4



3.25	68.10	4	1695.93	4	0.76	4	270.11	4
3.30	68.54	4	1706.42	4	0.73	2	256.45	2
3.35	68.96	4	1716.29	4	0.69	2	245.09	2
3.40	69.36	4	1725.53	4	0.66	2	233.57	2
3.45	69.73	4	1734.15	4	0.63	2	221.89	2
3.50	70.07	4	1742.14	4	0.59	2	210.05	2
3.55	70.39	4	1749.49	4	0.56	2	198.05	2
3.60	70.69	4	1756.20	4	0.53	2	185.89	2
3.65	70.96	4	1762.25	4	0.49	2	173.58	2
3.70	71.20	4	1767.65	4	0.46	2	161.10	2
3.75	71.42	4	1772.38	4	0.42	2	148.47	2
3.80	71.62	4	1776.45	4	0.38	2	135.67	2
3.85	71.78	4	1779.84	4	0.35	2	122.72	2
3.90	71.92	4	1782.55	4	0.31	1	110.01	1
3.95	72.04	4	1784.57	4	0.28	1	97.60	1
4.00	72.12	4	1785.90	4	0.24	1	85.02	1
4.05	72.18	4	1786.53	4	0.20	1	72.30	1
4.10	72.22	4	1786.46	4	0.17	1	59.41	1
4.15	72.22	4	1785.67	4	0.13	1	46.36	1
4.20	72.20	4	1784.17	4	0.09	1	33.16	1
4.25	72.15	4	1781.95	4	0.12	4	40.85	4
4.30	72.07	4	1779.00	4	0.16	4	57.86	4
4.35	71.96	4	1775.31	4	0.21	4	75.01	4
4.40	71.83	4	1770.89	4	0.26	4	92.31	4
4.45	71.66	4	1765.71	4	0.31	4	109.74	4
4.50	71.47	4	1759.79	4	0.36	4	127.31	4
4.55	71.24	4	1753.10	4	0.41	4	145.02	4
4.60	70.99	4	1745.66	4	0.46	4	162.87	4
4.65	70.71	4	1737.44	4	0.51	4	180.86	4
4.70	70.39	4	1728.44	4	0.56	4	198.99	4
4.75	70.05	4	1718.67	4	0.61	4	217.26	4
4.80	69.67	4	1708.10	4	0.67	4	235.67	4
4.85	69.27	4	1696.74	4	0.72	4	254.22	4
4.90	68.83	4	1684.58	4	0.77	4	272.92	4
4.95	68.37	4	1671.62	4	0.82	4	291.75	4
5.00	67.87	4	1657.84	4	0.88	4	310.72	4
5.05	67.34	4	1643.24	4	0.93	4	329.83	4
5.10	66.77	4	1627.83	4	0.99	4	349.08	4
5.15	66.18	4	1611.58	4	1.04	4	368.48	4
5.20	65.55	4	1594.49	4	1.10	4	388.01	4
5.25	64.89	4	1576.57	4	1.15	4	407.69	4
5.30	64.20	4	1557.79	4	1.21	4	427.50	4
5.35	63.47	4	1538.17	4	1.27	4	447.46	4
5.40	62.71	4	1517.68	4	1.32	4	467.57	4
5.45	61.92	4	1496.33	4	1.38	4	487.81	4
5.50	61.09	4	1474.11	4	1.44	4	508.20	4
5.55	60.23	4	1451.01	4	1.49	4	528.73	4
5.60	59.33	4	1427.02	4	1.55	4	549.40	4
5.65	58.40	4	1402.15	4	1.61	4	570.22	4
5.70	57.44	4	1376.39	4	1.67	4	591.19	4
5.75	56.44	4	1349.72	4	1.73	4	612.30	4
5.80	55.40	4	1322.15	4	1.79	4	633.56	4



5.85	54.33	4	1293.66	4	1.85	4	654.96	4
5.90	53.22	4	1264.26	4	1.91	4	676.52	4
5.95	52.08	4	1233.93	4	1.97	4	698.23	4
6.00	50.90	4	1202.68	4	2.04	4	720.09	4
6.05	49.68	4	1170.49	4	2.10	4	742.10	4
6.10	48.43	4	1137.36	4	2.16	4	764.28	4
6.15	47.14	4	1103.28	4	2.22	4	786.61	4
6.20	45.82	4	1068.25	4	2.29	4	809.11	4
6.25	44.45	4	1032.26	4	2.35	4	831.78	4
6.30	43.05	4	995.32	4	2.42	4	854.62	4
6.35	41.61	4	957.40	4	2.48	4	877.65	4
6.40	40.13	4	918.51	4	2.55	4	900.87	4
6.45	38.61	4	878.64	4	2.61	4	924.28	4
6.50	37.06	4	837.79	4	2.68	4	947.92	4
6.55	35.46	4	795.96	4	2.75	4	971.79	4
6.60	33.83	4	753.13	4	2.82	4	995.91	4
6.65	32.16	4	709.31	4	2.88	4	1020.33	4
6.70	30.44	4	664.50	4	2.95	4	1045.08	4
6.75	28.69	4	618.68	4	3.03	4	1070.21	4
6.80	26.89	4	571.87	4	3.10	4	1095.82	4
6.85	25.05	4	524.07	4	3.17	4	1122.01	4
6.90	23.17	4	475.27	4	3.25	4	1148.97	4
6.95	21.25	4	425.50	4	3.33	4	1176.94	4
7.00	19.28	4	374.78	4	3.41	4	1206.34	4
7.05	17.27	4	323.14	4	3.50	4	1237.85	4
7.10	15.21	4	270.66	4	3.60	4	1272.63	4
7.15	13.13	2	218.14	2	3.71	4	1312.77	4
7.20	11.27	2	171.76	2	3.85	4	1362.24	4
7.25	9.37	2	125.25	2	4.04	4	1428.30	4
7.30	7.41	2	93.12	2	4.29	4	1517.02	4
7.35	5.46	2	70.52	2	4.38	4	1549.18	4
7.40	3.73	1	49.99	1	3.88	4	1371.05	4
7.45	2.43	1	34.03	1	3.95	4	1396.56	4
7.50	3.36	4	45.61	4	4.22	4	1493.07	4
7.55	5.45	4	70.63	4	4.78	4	1691.23	4
7.60	7.93	4	99.32	4	4.69	4	1657.84	4
7.65	10.49	4	146.64	4	4.60	4	1627.18	4
7.70	13.09	4	209.04	4	4.58	4	1618.88	4
7.75	15.73	4	273.53	4	4.59	4	1624.12	4
7.80	18.40	4	339.67	4	4.63	4	1637.03	4
7.85	21.11	4	407.25	4	4.68	4	1654.51	4
7.90	23.86	4	476.16	4	4.74	4	1674.84	4
7.95	26.65	4	546.36	4	4.80	4	1697.09	4
8.00	29.48	4	617.81	4	4.87	4	1720.66	4
8.05	32.36	4	690.50	4	4.93	4	1745.20	4
8.10	35.28	4	764.42	4	5.01	4	1770.48	4
8.15	38.25	4	839.56	4	5.08	4	1796.34	4
8.20	41.26	4	915.92	4	5.15	4	1822.67	4
8.25	44.32	4	993.50	4	5.23	4	1849.39	4
8.30	47.42	4	1072.31	4	5.31	4	1876.45	4
8.35	50.57	4	1152.34	4	5.38	4	1903.79	4
8.40	53.76	4	1233.61	4	5.46	4	1931.36	4



8.45	57.01	4	1316.10	4	5.54	4	1959.13	4
8.50	60.30	4	1399.82	4	5.62	4	1987.06	4
8.55	63.63	4	1484.78	4	5.70	4	2015.12	4
8.60	67.02	4	1570.98	4	5.78	4	2043.29	4
8.65	70.45	4	1658.41	4	5.86	4	2071.57	4
8.70	73.93	4	1747.09	4	5.94	4	2099.95	4
8.75	77.46	4	1837.00	4	6.02	4	2128.42	4
8.80	81.03	4	1928.16	4	6.10	4	2156.99	4
8.85	84.65	4	2020.56	4	6.18	4	2185.64	4
8.90	88.33	4	2114.22	4	6.26	4	2214.37	4
8.95	92.05	4	2209.12	4	6.34	4	2243.21	4
9.00	95.81	4	2305.28	4	6.42	4	2272.14	4
9.05	92.94	4	2230.30	4	4.84	4	1711.53	4
9.10	90.11	4	2156.60	4	4.75	4	1681.60	4
9.15	87.34	4	2084.20	4	4.67	4	1651.02	4
9.20	84.61	4	2013.11	4	4.58	4	1620.49	4
9.25	81.94	4	1943.35	4	4.50	4	1590.04	4
9.30	79.31	4	1874.90	4	4.41	4	1559.69	4
9.35	76.74	4	1807.76	4	4.32	4	1529.49	4
9.40	74.22	4	1741.92	4	4.24	4	1499.47	4
9.45	71.74	4	1677.38	4	4.16	4	1469.64	4
9.50	69.32	4	1614.13	4	4.07	4	1440.05	4
9.55	66.94	4	1552.16	4	3.99	4	1410.72	4
9.60	64.62	4	1491.46	4	3.91	4	1381.68	4
9.65	62.34	4	1432.02	4	3.83	4	1352.95	4
9.70	60.11	4	1373.82	4	3.75	4	1324.56	4
9.75	57.93	4	1316.86	4	3.67	4	1296.53	4
9.80	55.79	4	1261.11	4	3.59	4	1268.90	4
9.85	53.70	4	1206.57	4	3.51	4	1241.68	4
9.90	51.66	4	1153.21	4	3.44	4	1214.90	4
9.95	49.66	4	1101.03	4	3.36	4	1188.59	4
10.00	47.70	4	1050.00	4	3.29	4	1162.76	4
10.05	45.79	4	1000.10	4	3.22	4	1137.44	4
10.10	43.92	4	951.32	4	3.15	4	1112.65	4
10.15	42.09	4	903.64	4	3.08	4	1088.42	4
10.20	40.30	4	857.03	4	3.01	4	1064.77	4
10.25	38.55	4	811.47	4	2.95	4	1041.73	4
10.30	36.84	4	766.96	4	2.88	4	1019.31	4
10.35	35.17	4	723.46	4	2.82	4	997.55	4
10.40	33.54	4	680.95	4	2.76	4	976.48	4
10.45	31.94	4	639.41	4	2.70	4	956.12	4
10.50	30.37	4	598.83	4	2.65	4	936.50	4
10.55	28.84	4	559.17	4	2.59	4	917.67	4
10.60	27.34	4	520.43	4	2.54	4	899.67	4
10.65	25.87	4	482.58	4	2.50	4	882.54	4
10.70	24.43	4	445.60	4	2.45	4	866.33	4
10.75	23.02	4	409.48	4	2.41	4	851.11	4
10.80	21.64	4	374.21	4	2.37	4	836.95	4
10.85	20.28	4	339.78	4	2.33	4	823.93	4
10.90	18.95	4	306.19	4	2.30	4	812.13	4
10.95	17.65	4	273.43	4	2.27	4	801.66	4
11.00	16.36	4	241.40	4	2.23	4	789.84	4



11.05	15.09	4	210.30	4	2.17	4	768.81	4
11.10	13.87	4	180.69	4	2.12	4	748.76	4
11.15	12.69	4	157.84	4	2.06	4	729.61	4
11.20	11.56	4	144.97	4	2.01	4	711.11	4
11.25	10.48	4	132.58	4	1.96	4	692.68	4
11.30	9.44	4	120.71	4	1.90	4	673.24	4
11.35	8.47	4	109.44	4	1.84	4	651.04	4
11.40	7.57	4	98.87	4	1.76	4	623.72	4
11.45	6.75	4	89.15	4	1.67	4	589.12	4
11.50	6.02	4	80.43	4	1.55	4	546.76	4
11.55	5.39	4	72.78	4	1.41	4	499.12	4
11.60	4.85	4	66.19	4	1.28	4	452.03	4
11.65	4.38	4	60.35	4	1.20	4	424.15	4
11.70	3.93	4	54.82	4	1.14	4	403.56	4
11.75	3.51	4	49.57	4	1.08	4	383.49	4
11.80	3.10	4	44.59	4	1.03	4	363.92	4
11.85	2.72	4	39.87	4	0.98	4	344.86	4
11.90	2.47	1	36.80	1	0.92	4	326.31	4
11.95	2.77	4	40.51	4	0.87	4	308.28	4
12.00	3.11	4	44.79	4	0.82	4	290.75	4
12.05	3.43	4	48.83	4	0.77	4	273.73	4
12.10	3.74	4	52.64	4	0.73	4	257.22	4
12.15	4.03	4	56.23	4	0.68	4	241.22	4
12.20	4.30	4	59.61	4	0.64	4	225.72	4
12.25	4.55	4	62.78	4	0.60	4	210.71	4
12.30	4.79	4	65.75	4	0.55	4	196.19	4
12.35	5.01	4	68.53	4	0.52	4	182.71	4
12.40	5.22	4	71.16	4	0.49	4	171.68	4
12.45	5.42	4	73.66	4	0.46	4	160.93	4
12.50	5.61	4	76.05	4	0.42	4	150.10	4
12.55	5.79	4	78.30	4	0.39	4	139.16	4
12.60	5.96	4	80.41	4	0.36	4	128.17	4
12.65	6.12	4	82.38	4	0.33	4	117.20	4
12.70	6.27	4	84.20	4	0.30	4	106.33	4
12.75	6.40	4	85.88	4	0.27	4	95.62	4
12.80	6.53	4	87.40	4	0.24	4	85.15	4
12.85	6.64	4	88.77	4	0.21	4	74.94	4
12.90	6.73	4	90.00	4	0.18	4	65.04	4
12.95	6.82	4	91.07	4	0.16	4	55.47	4
13.00	6.90	4	92.01	4	0.13	4	46.26	4
13.05	6.96	4	92.81	4	0.11	4	37.42	4
13.10	7.01	4	93.48	4	0.08	4	28.96	4
13.15	7.05	4	94.02	4	0.06	4	20.88	4
13.20	7.09	4	94.44	4	0.04	4	13.19	4
13.25	7.11	4	94.75	4	0.02	4	5.88	4
13.30	7.12	4	94.94	4	0.01	1	1.98	1
13.35	7.13	4	95.04	4	0.02	4	7.58	4
13.40	7.12	4	95.03	4	0.04	4	13.74	4
13.45	7.11	4	94.93	4	0.06	4	19.53	4
13.50	7.10	4	94.75	4	0.07	4	24.96	4
13.55	7.07	4	94.50	4	0.08	4	30.02	4
13.60	7.04	4	94.16	4	0.10	4	34.73	4



13.65	7.01	4	93.77	4	0.11	4	39.10	4
13.70	6.96	4	93.31	4	0.12	4	43.13	4
13.75	6.92	4	92.80	4	0.13	4	46.83	4
13.80	6.87	4	92.23	4	0.14	4	50.21	4
13.85	6.82	4	91.63	4	0.15	4	53.29	4
13.90	6.76	4	90.98	4	0.16	4	56.05	4
13.95	6.71	4	90.30	4	0.17	4	58.53	4
14.00	6.64	4	89.59	4	0.17	4	60.73	4
14.05	6.58	4	88.86	4	0.18	4	62.66	4
14.10	6.52	4	88.11	4	0.18	4	64.34	4
14.15	6.45	4	87.34	4	0.19	4	65.77	4
14.20	6.39	4	86.56	4	0.19	4	66.97	4
14.25	6.32	4	85.77	4	0.19	4	67.95	4
14.30	6.25	4	84.97	4	0.19	4	68.74	4
14.35	6.19	4	84.17	4	0.20	4	69.34	4
14.40	6.12	4	83.37	4	0.20	4	69.77	4
14.45	6.05	4	82.58	4	0.20	4	70.05	4
14.50	5.99	4	81.78	4	0.20	4	70.21	4
14.55	5.92	4	80.99	4	0.20	4	70.28	4
14.60	5.86	4	80.20	4	0.20	4	70.34	4
14.65	5.79	4	79.41	4	0.20	4	70.53	4
14.70	5.72	4	78.61	4	0.20	4	70.62	4
14.75	5.66	4	77.82	4	0.20	4	70.60	4
14.80	5.59	4	77.02	4	0.20	4	70.47	4
14.85	5.52	4	76.23	4	0.20	4	70.25	4
14.90	5.46	4	75.44	4	0.20	4	69.93	4
14.95	5.39	4	74.65	4	0.20	4	69.52	4
15.00	5.33	4	73.87	4	0.20	4	69.03	4
15.05	5.26	4	73.10	4	0.19	4	68.47	4
15.10	5.20	4	72.33	4	0.19	4	67.82	4
15.15	5.14	4	71.57	4	0.19	4	67.11	4
15.20	5.07	4	70.83	4	0.19	4	66.34	4
15.25	5.01	4	70.09	4	0.19	4	65.50	4
15.30	4.95	4	69.36	4	0.18	4	64.61	4
15.35	4.89	4	68.65	4	0.18	4	63.67	4
15.40	4.83	4	67.95	4	0.18	4	62.68	4
15.45	4.78	4	67.26	4	0.17	4	61.64	4
15.50	4.72	4	66.58	4	0.17	4	60.57	4
15.55	4.66	4	65.92	4	0.17	4	59.45	4
15.60	4.61	4	65.28	4	0.16	4	58.31	4
15.65	4.56	4	64.65	4	0.16	4	57.13	4
15.70	4.51	4	64.03	4	0.16	4	55.93	4
15.75	4.46	4	63.43	4	0.15	4	54.70	4
15.80	4.41	4	62.85	4	0.15	4	53.45	4
15.85	4.36	4	62.29	4	0.15	4	52.18	4
15.90	4.31	4	61.74	4	0.14	4	50.89	4
15.95	4.27	4	61.21	4	0.14	4	49.59	4
16.00	4.22	4	60.69	4	0.14	4	48.28	4
16.05	4.18	4	60.20	4	0.13	4	46.95	4
16.10	4.14	4	59.72	4	0.13	4	45.63	4
16.15	4.10	4	59.26	4	0.13	4	44.29	4
16.20	4.06	4	58.82	4	0.12	4	42.95	4



16.25	4.03	4	58.39	4	0.12	4	41.61	4
16.30	3.99	4	57.98	4	0.11	4	40.27	4
16.35	3.96	4	57.59	4	0.11	4	38.93	4
16.40	3.93	4	57.22	4	0.11	4	37.59	4
16.45	3.90	4	56.87	4	0.10	4	36.26	4
16.50	3.87	4	56.54	4	0.10	4	34.93	4
16.55	3.84	4	56.22	4	0.10	4	33.60	4
16.60	3.81	4	55.92	4	0.09	4	32.29	4
16.65	3.79	4	55.64	4	0.09	4	30.99	4
16.70	3.77	4	55.37	4	0.08	4	29.69	4
16.75	3.74	4	55.12	4	0.08	4	28.40	4
16.80	3.72	4	54.89	4	0.08	4	27.13	4
16.85	3.70	4	54.68	4	0.07	4	25.87	4
16.90	3.69	4	54.49	4	0.07	4	24.62	4
16.95	3.67	4	54.31	4	0.07	4	23.39	4
17.00	3.65	4	54.14	4	0.06	4	22.17	4
17.05	3.64	4	54.00	4	0.06	4	20.96	4
17.10	3.63	4	53.87	4	0.06	4	19.77	4
17.15	3.62	4	53.75	4	0.05	4	18.60	4
17.20	3.61	4	53.65	4	0.05	4	17.44	4
17.25	3.60	4	53.57	4	0.05	4	16.29	4
17.30	3.59	4	53.50	4	0.04	4	15.17	4
17.35	3.58	4	53.45	4	0.04	4	14.06	4
17.40	3.58	4	53.41	4	0.04	4	12.97	4
17.45	3.57	4	53.39	4	0.03	4	11.90	4
17.50	3.57	4	53.38	4	0.03	4	10.84	4
17.55	3.57	4	53.38	4	0.03	4	9.80	4
17.60	3.57	4	53.40	4	0.02	4	8.78	4
17.65	3.57	4	53.43	4	0.02	4	7.78	4
17.70	3.57	4	53.48	4	0.02	4	6.80	4
17.75	3.57	4	53.54	4	0.02	4	5.83	4
17.80	3.58	4	53.61	4	0.01	4	4.88	4
17.85	3.58	4	53.70	4	0.01	4	3.95	4
17.90	3.59	4	53.79	4	0.01	4	3.04	4
17.95	3.59	4	53.90	4	0.01	4	2.15	4
18.00	3.60	4	54.02	4	0.00	4	1.27	4
18.05	3.61	4	54.16	4	0.00	4	0.42	4



## Verifica sezione cordoli

### *Simbologia adottata*

$M_h$	momento flettente espresso in [kgm] nel piano orizzontale
$T_h$	taglio espresso in [kg] nel piano orizzontale
$M_v$	momento flettente espresso in [kgm] nel piano verticale
$T_v$	taglio espresso in [kg] nel piano verticale

### **Cordolo N° 1 (X=0.00 m) (Cordolo in c.a.)**

$B=60.00$ [cm]	$H=80.00$ [cm]		
$A_{fv}=8.04$ [cmq]	$A_{fh}=8.04$ [cmq]	Staffe $\phi 10/12$	$N_{bh}=2 - N_{bv}=2$
$M_h=14222$ [kgm]	$T_h=28445$ [kg]	$M_v=216$ [kgm]	$T_v=720$ [kg]
$\sigma_c = 51.33$ [kg/cmq]	$\sigma_f = 3304.85$ [kg/cmq]	$\tau_c = 6.97$ [kg/cmq]	$\sigma_{staffe} = 4260.80$ [kg/cmq]

### Computo delle quantità e dei costi

Numero di pali	31
----------------	----

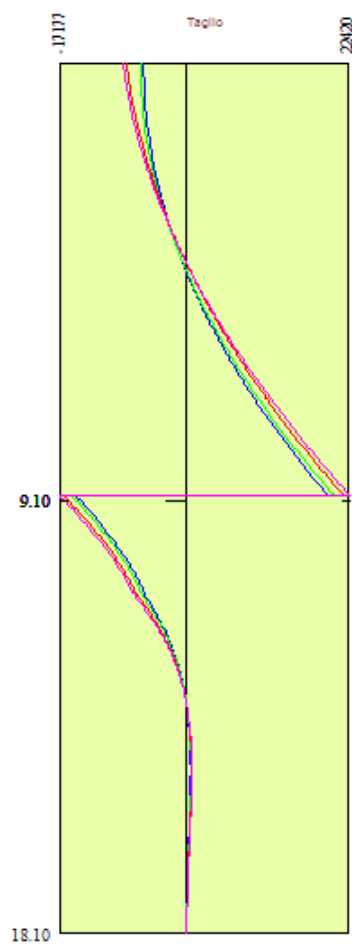
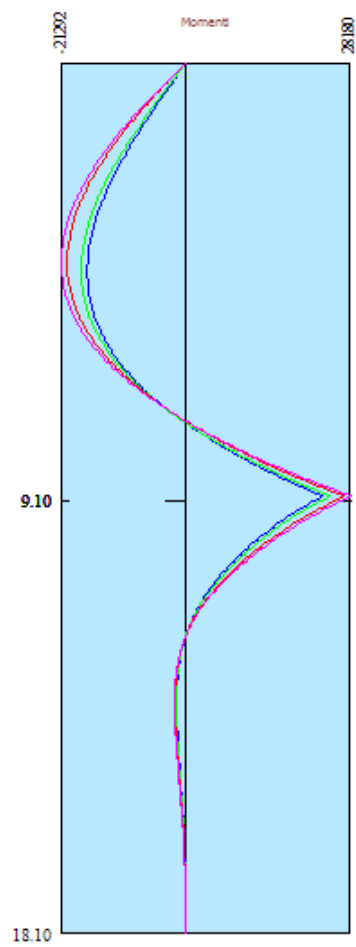
### **Quantità per il singolo palo**

Perforazione	[m]	18.10
Diametro perforazione	[m]	0.60
Volume calcestruzzo	[mc]	5.12
Quantità acciaio	[kg]	821.16

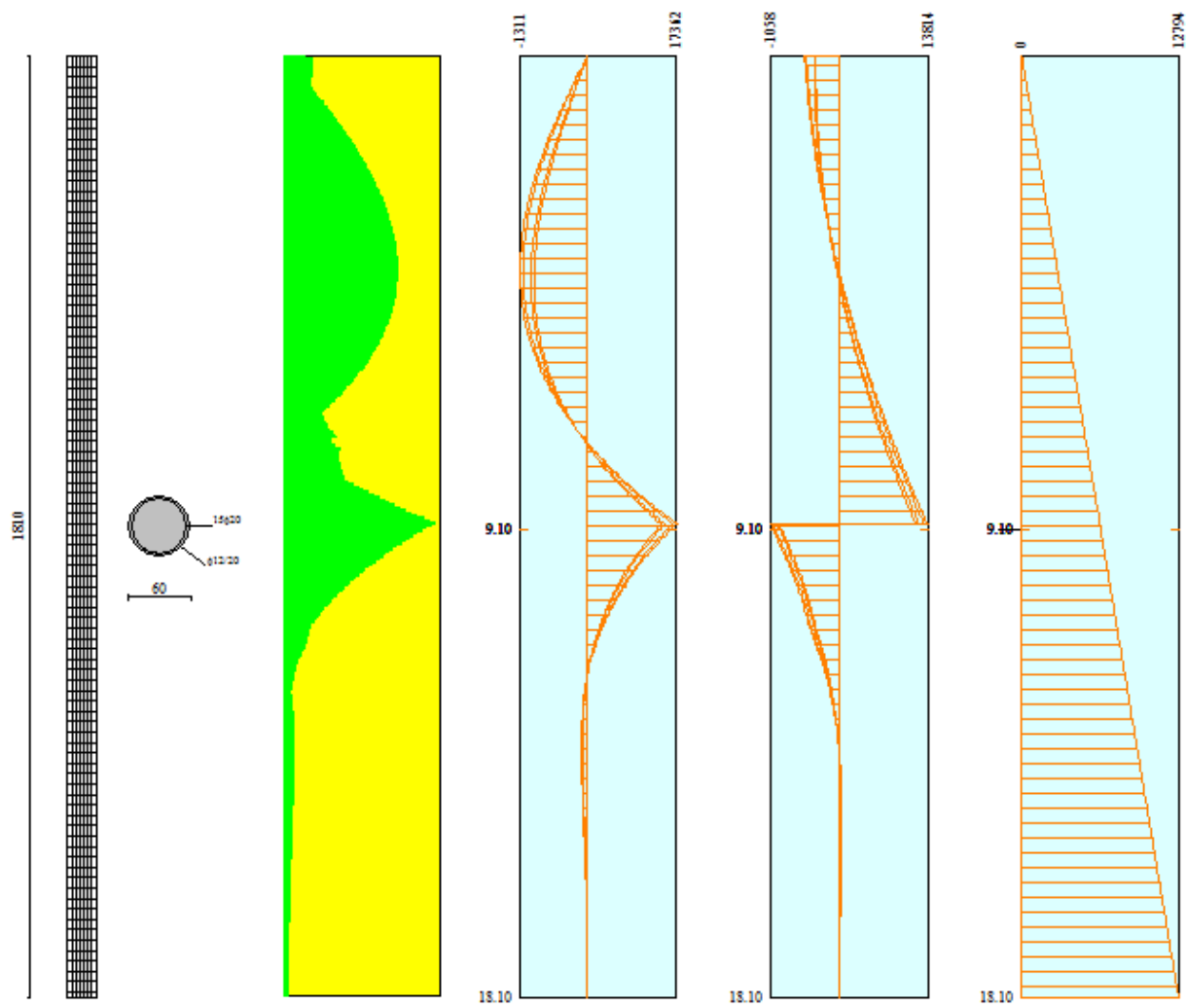
### *Quantità acciaio per diametro*

<b>Diametro(mm)</b>	<b>Quantita(Kg)</b>
12	151.60
20	669.56











# PALIFICATA TIPO – B -

## Geometria paratia

### Tipo paratia: **Paratia di pali**

Altezza fuori terra	5.20	[m]
Profondità di infissione	8.80	[m]
Altezza totale della paratia	14.00	[m]
Lunghezza paratia	19.10	[m]

Numero di file di pali	1	
Interasse fra i pali della fila	0.60	[m]
Diametro dei pali	60.00	[cm]
Numero totale di pali	31	
Numero di pali per metro lineare	1.62	

## Geometria cordoli

### *Simbologia adottata*

n°	numero d'ordine del cordolo
Y	posizione del cordolo sull'asse della paratia espresso in [m]

#### Cordoli in calcestruzzo

B	Base della sezione del cordolo espresso in [cm]
H	Altezza della sezione del cordolo espresso in [cm]

#### Cordoli in acciaio

A	Area della sezione in acciaio del cordolo espresso in [cmq]
W	Modulo di resistenza della sezione del cordolo espresso in [cm^3]

n°	Y	Tipo	B	H	A	W
1	0.00	Calcestruzzo	60.00	80.00	--	--

## Geometria profilo terreno

### *Simbologia adottata e sistema di riferimento*

(Sistema di riferimento con origine in testa alla paratia, ascissa X positiva verso monte, ordinata Y positiva verso l'alto)

N	numero ordine del punto
X	ascissa del punto espressa in [m]
Y	ordinata del punto espressa in [m]
A	inclinazione del tratto espressa in [°]

### **Profilo di monte**

N	X	Y	A
2	10.00	0.00	0.00

### **Profilo di valle**

N	X	Y	A
1	-10.00	-5.20	0.00



2	0.00	-5.20	0.00
---	------	-------	------

## Descrizione terreni

### Simbologia adottata

n°	numero d'ordine dello strato a partire dalla sommità della paratia
Descrizione	Descrizione del terreno
$\gamma$	peso di volume del terreno espresso in [kg/mc]
$\gamma_s$	peso di volume saturo del terreno espresso [kg/mc]
$\phi$	angolo d'attrito interno del terreno espresso in [°]
$\delta$	angolo d'attrito terreno/paratia espresso in [°]
c	coesione del terreno espressa in [kg/cm <sup>2</sup> ]

n°	Descrizione	$\gamma$	$\gamma_s$	$\phi$	$\delta$	c
1	Limo sabbiosi e cineriti	1800.00	1900.00	29.00	0.00	0.000
2	tufo	1600.00	2000.00	45.00	0.00	0.000

## Descrizione stratigrafia

### Simbologia adottata

n°	numero d'ordine dello strato a partire dalla sommità della paratia
sp	spessore dello strato in corrispondenza dell'asse della paratia espresso in [m]
kw	costante di Winkler orizzontale espressa in Kg/cm <sup>2</sup> /cm
$\alpha$	inclinazione dello strato espressa in GRADI(°)
Terreno	Terreno associato allo strato

n°	sp	$\alpha$	kw	Terreno
1	6.60	0.00	1.00	Limo sabbiosi e cineriti
2	15.00	0.00	9.01	tufo

## Falda

Profondità della falda a monte rispetto alla sommità della paratia 4.60 [m]  
 Profondità della falda a valle rispetto alla sommità della paratia 4.60 [m]  
 Regime delle pressioni neutre: **Idrostatico**

## Caratteristiche materiali utilizzati

### Calcestruzzo

Peso specifico 2500 [kg/mc]  
 Classe di Resistenza C25/30



Resistenza caratteristica a compressione $R_{bk}$	306	[kg/cm <sup>2</sup> ]
Tensione di progetto a compressione $\sigma_c$	99	[kg/cm <sup>2</sup> ]
Tensione tangenziale ammissibile $\tau_{c0}$	6.1	[kg/cm <sup>2</sup> ]
Tensione tangenziale ammissibile $\tau_{c1}$	18.5	[kg/cm <sup>2</sup> ]

#### **Acciaio**

Tipo	B450C	
Tensione ammissibile $\sigma_{fa}$	4589	[kg/cm <sup>2</sup> ]
Tensione di snervamento $f_{yk}$	4589	[kg/cm <sup>2</sup> ]

#### **Caratteristiche acciaio cordoli in c.a.**

Tipo	B450C	
Tensione ammissibile $\sigma_{fa}$	4589	[kg/cm <sup>2</sup> ]
Tensione di snervamento $f_{yk}$	4589	[kg/cm <sup>2</sup> ]

### Condizioni di carico

#### *Simbologia e convenzioni adottate*

Le ascisse dei punti di applicazione del carico sono espresse in [m] rispetto alla testa della paratia

Le ordinate dei punti di applicazione del carico sono espresse in [m] rispetto alla testa della paratia

$F_x$	Forza orizzontale espressa in [kg], positiva da monte verso valle
$F_y$	Forza verticale espressa in [kg], positiva verso il basso
$M$	Momento espresso in [kgm], positivo ribaltante
$Q_i, Q_f$	Intensità dei carichi distribuiti sul profilo espresse in [kg/mq]
$V_i, V_s$	Intensità dei carichi distribuiti sulla paratia espresse in [kg/mq], positivi da monte verso valle
$R$	Risultante carico distribuito sulla paratia espressa in [kg]

#### Condizione n° 1

Carico distribuito sul profilo	$X_i = 1.00$	$X_f = 5.00$	$Q_i = 500$	$Q_f = 500$
Carico distribuito sul profilo	$X_i = 5.00$	$X_f = 10.00$	$Q_i = 8000$	$Q_f = 8000$

### Vincoli lungo l'altezza della paratia

#### *Simbologia adottata*

$n^\circ$	numero d'ordine del vincolo
$Y$	ordinata del vincolo rispetto alla testa della paratia espressa in [m]
$V_x$	Vincolo in direzione orizzontale
$K_x$	Rigidezza vincolo in direzione orizzontale espresso in [Kg/cm]
$V_r$	Vincolo alla rotazione
$K_r$	Rigidezza vincolo alla rotazione espresso in [Kgm/°]

$n^\circ$	$Y$	$V_x$	$K_x$	$V_r$	$K_r$
1	5.00	V. RIGIDO	--	LIBERO	--
2	0.00	V. RIGIDO	--	LIBERO	--



## Combinazioni di carico

Nella tabella sono riportate le condizioni di carico di ogni combinazione con il relativo coefficiente di partecipazione.

### Combinazione n° 1

Spinta terreno

### Combinazione n° 2

Spinta terreno

Condizione 1 (terreno) x 1.00

### Combinazione n° 3

Spinta terreno

### Combinazione n° 4

Spinta terreno

Condizione 1 (terreno) x 1.00

## Impostazioni di progetto

### Spinte e verifiche secondo :

- D.M. 11/03/1988

- D.M. 16/01/1996

### Verifica materiali

Tensioni ammissibili

Impostazioni di analisi

## **Analisi per Combinazioni di Carico.**

Rottura del terreno: Pressione passiva

Influenza  $\delta$  (angolo di attrito terreno-paratia): Nel calcolo del coefficiente di spinta attiva  $K_a$  e nell'inclinazione della spinta attiva (non viene considerato per la spinta passiva)

Stabilità globale: Metodo di Fellenius



## Impostazioni analisi sismica

Coefficiente di intensità sismica (percento) 7.00

Forma del diagramma di incremento sismico triangolare con vertice in basso sulla parte fuori terra

Influenza sisma nella spinta attiva da monte



## Analisi della paratia

### L'analisi è stata eseguita per combinazioni di carico

La paratia è analizzata con il metodo degli elementi finiti.

Essa è discretizzata in 104 elementi fuori terra e 176 elementi al di sotto della linea di fondo scavo.

Le molle che simulano il terreno hanno un comportamento elastoplastico: una volta raggiunta la pressione passiva non reagiscono ad ulteriori incremento di carico.

Altezza fuori terra della paratia	5.20	[m]
Profondità di infissione	8.80	[m]
Altezza totale della paratia	14.00	[m]

### Forze agenti sulla paratia

Tutte le forze si intendono positive se dirette da monte verso valle. Esse sono riferite ad un metro di larghezza della paratia. Le Y hanno come origine la testa della paratia, e sono espresse in [m]

#### Simbologia adottata

n°	Indice della Combinazione/Fase
Tipo	Tipo della Combinazione/Fase
Pa	Spinta attiva, espressa in [kg]
Is	Incremento sismico della spinta, espressa in [kg]
Pw	Spinta della falda, espressa in [kg]
Pp	Resistenza passiva, espressa in [kg]
Pc	Controspinta, espressa in [kg]

n°	Pa	Y <sub>Pa</sub>	Is	Y <sub>Is</sub>	Pw	Y <sub>Pw</sub>	Pp	Y <sub>Pp</sub>	Pc	Y <sub>Pc</sub>
1	10496	3.90	--	--	0	0.00	-61	12.83	927	7.78
2	12427	4.11	--	--	0	0.00	-41	12.62	555	7.65
3	10509	3.97	1556	1.73	0	0.00	-74	12.83	1140	7.78
4	12456	4.26	3722	1.73	0	0.00	-73	12.74	1063	7.72

#### Simbologia adottata

n°	Indice della Combinazione/Fase
Tipo	Tipo della Combinazione/Fase
Rc	Risultante carichi esterni applicati, espressa in [kg]
Rt	Risultante delle reazioni dei tiranti (componente orizzontale), espressa in [kg]
Rv	Risultante delle reazioni dei vincoli, espressa in [kg]
Rp	Risultante delle reazioni dei puntoni, espressa in [kg]

n°	Rc	Y <sub>Rc</sub>	Rt	Y <sub>Rt</sub>	Rv	Y <sub>Rv</sub>	Rp	Y <sub>Rp</sub>
1	0	0.00	--	---11363	4.17	--	--	--
2	0	0.00	--	---12941	4.24	--	--	--
3	0	0.00	--	---13130	3.99	--	--	--
4	0	0.00	--	---17167	3.89	--	--	--

#### Simbologia adottata



n°	Indice della Combinazione/Fase
P <sub>NUL</sub>	Punto di nullo del diagramma, espresso in [m]
P <sub>INV</sub>	Punto di inversione del diagramma, espresso in [m]
C <sub>ROT</sub>	Punto Centro di rotazione, espresso in [m]
MP	Percentuale molle plasticizzate, espressa in [%]
R/R <sub>MAX</sub>	Rapporto tra lo sforzo reale nelle molle e lo sforzo che le molle sarebbero in grado di esplicare, espresso in [%]
Pp	Portanza di punta, espressa in [kg]

<b>n°</b>	<b>P<sub>NUL</sub></b>	<b>P<sub>INV</sub></b>	<b>C<sub>ROT</sub></b>	<b>MP</b>	<b>R/R<sub>MAX</sub></b>	<b>Pp</b>
1	6.55	5.20	11.09	0.00	0.21	470188
2	6.59	12.80	10.79	0.00	0.12	470188
3	6.55	5.20	11.10	0.00	0.26	470188
4	6.59	5.20	10.96	0.00	0.21	470188



## Risultati vincoli

### *Simbologia adottata*

n°	Indice del vincolo
Y	posizione del vincolo rispetto alla testa della paratia espressa in [m]
R <sub>x</sub> /ml	reazione in direzione orizzontale a metro lineare, positiva verso valle, espressa in [kg]
R <sub>θ</sub> /ml	reazione momento a metro lineare, positiva antioraria, espressa in [kgm]
u	spostamento orizzontale, positivo verso valle, espresso in [cm]

### **Combinazione n° 1**

n°	Y	R <sub>x</sub>	R <sub>θ</sub>	u
1	5.00	-9470.10	--	0.00
2	0.00	-1892.43	--	0.00

### **Combinazione n° 2**

n°	Y	R <sub>x</sub>	R <sub>θ</sub>	u
1	5.00	-10964.72	--	0.00
2	0.00	-1976.24	--	0.00

### **Combinazione n° 3**

n°	Y	R <sub>x</sub>	R <sub>θ</sub>	u
1	5.00	-10464.38	--	0.00
2	0.00	-2665.23	--	0.00

### **Combinazione n° 4**

n°	Y	R <sub>x</sub>	R <sub>θ</sub>	u
1	5.00	-13345.86	--	0.00
2	0.00	-3820.94	--	0.00



## Valori massimi e minimi sollecitazioni per metro di paratia

### *Simbologia adottata*

n°	Indice della combinazione/fase
Tipo	Tipo della combinazione/fase
Y	ordinata della sezione rispetto alla testa espressa in [m]
M	momento flettente massimo e minimo espresso in [kgm]
N	sforzo normale massimo e minimo espresso in [kg] (positivo di compressione)
T	taglio massimo e minimo espresso in [kg]

<b>n°</b>	<b>M</b>	<b>Y<sub>M</sub></b>	<b>T</b>	<b>Y<sub>T</sub></b>	<b>N</b>	<b>Y<sub>N</sub></b>	
1	3546	5.00	5889	5.00	16062	14.00	MAX
--	-3105	2.45	-3581	5.00	0	0.00	MIN
2	4121	5.00	6383	5.00	16062	14.00	MAX
--	-3239	2.40	-4582	5.00	0	0.00	MIN
3	4095	5.00	6582	5.00	16062	14.00	MAX
--	-3762	2.35	-3883	5.00	0	0.00	MIN
4	5434	5.00	8041	5.00	16062	14.00	MAX
--	-4836	2.25	-5305	5.00	0	0.00	MIN



## Spostamenti massimi e minimi della paratia

### *Simbologia adottata*

n°	Indice della combinazione/fase
Tipo	Tipo della combinazione/fase
Y	ordinata della sezione rispetto alla testa della paratia espressa in [m]
U	spostamento orizzontale massimo e minimo espresso in [cm] positivo verso valle
V	spostamento verticale massimo e minimo espresso in [cm] positivo verso il basso

<b>n°</b>	<b>U</b>	<b>Y<sub>U</sub></b>	<b>V</b>	<b>Y<sub>V</sub></b>	
1	0.0221	2.40	0.0078	0.00	MAX
--	-0.0049	6.50	0.0000	0.00	MIN
2	0.0226	2.40	0.0078	0.00	MAX
--	-0.0034	6.20	0.0000	0.00	MIN
3	0.0268	2.40	0.0078	0.00	MAX
--	-0.0060	6.50	0.0000	0.00	MIN
4	0.0339	2.35	0.0078	0.00	MAX
--	-0.0059	6.35	0.0000	0.00	MIN



## Stabilità globale

### Metodo di Fellenius

Numero di cerchi analizzati 100

#### Simbologia adottata

n°	Indice della combinazione/fase
Tipo	Tipo della combinazione/fase
(X <sub>C</sub> ; Y <sub>C</sub> )	Coordinate centro cerchio superficie di scorrimento, espresse in [m]
R	Raggio cerchio superficie di scorrimento, espresso in [m]
(X <sub>V</sub> ; Y <sub>V</sub> )	Coordinate intersezione del cerchio con il pendio a valle, espresse in [m]
(X <sub>M</sub> ; Y <sub>M</sub> )	Coordinate intersezione del cerchio con il pendio a monte, espresse in [m]
FS	Coefficiente di sicurezza

n°	(X <sub>C</sub> , Y <sub>C</sub> )	R	(X <sub>V</sub> , Y <sub>V</sub> )	(X <sub>M</sub> , Y <sub>M</sub> )	FS
1	(-2.80; 0.00)	14.28	(-16.11; -5.17)	(11.48; 0.00)	3.00
2	(-4.20; 0.00)	14.62	(-17.87; -5.18)	(10.42; 0.00)	2.16
3	(-4.20; 0.00)	14.62	(-17.87; -5.18)	(10.42; 0.00)	2.29
4	(-5.60; 0.00)	15.08	(-19.76; -5.17)	(9.48; 0.00)	1.77

### Combinazione n° 4

Numero di strisce 50

#### Simbologia adottata

Le ascisse X sono considerate positive verso monte	
Le ordinate Y sono considerate positive verso l'alto	
Origine in testa alla paratia (spigolo contro terra)	
Le strisce sono numerate da monte verso valle	
N°	numero d'ordine della striscia
W	peso della striscia espresso in [kg]
α	angolo fra la base della striscia e l'orizzontale espresso in gradi (positivo antiorario)
φ	angolo d'attrito del terreno lungo la base della striscia
c	coesione del terreno lungo la base della striscia espressa in [kg/cm <sup>2</sup> ]
b	larghezza della striscia espressa in [m]
L	sviluppo della base della striscia espressa in [m] (L=b/cosα)
u	pressione neutra lungo la base della striscia espressa in [kg/cm <sup>2</sup> ]
Ctn, Ctt	contributo alla striscia normale e tangenziale del tirante espresse in [kg]

### Caratteristiche delle strisce

N°	W	α(°)	Wsinα	L	φ	c	u	(Ctn; Ctt)
1	1078.39	-67.10	-993.38	1.49	29.00	0.000	0.126	(0; 0)
2	2468.44	-61.91	-2177.73	1.23	45.00	0.000	0.249	(0; 0)
3	3632.08	-57.51	-3063.61	1.08	45.00	0.000	0.349	(0; 0)
4	4620.83	-53.59	-3718.92	0.98	45.00	0.000	0.434	(0; 0)
5	5481.85	-50.01	-4200.12	0.90	45.00	0.000	0.509	(0; 0)
6	6243.06	-46.68	-4542.31	0.85	45.00	0.000	0.574	(0; 0)
7	6922.61	-43.55	-4769.57	0.80	45.00	0.000	0.632	(0; 0)
8	7533.12	-40.57	-4899.54	0.77	45.00	0.000	0.685	(0; 0)
9	8083.78	-37.72	-4945.84	0.73	45.00	0.000	0.732	(0; 0)
10	8581.52	-34.98	-4919.34	0.71	45.00	0.000	0.775	(0; 0)



11	9031.69	-32.32	-4829.06	0.69	45.00	0.000	0.814	(0; 0)
12	9438.54	-29.74	-4682.57	0.67	45.00	0.000	0.849	(0; 0)
13	9805.46	-27.23	-4486.46	0.65	45.00	0.000	0.880	(0; 0)
14	10135.24	-24.77	-4246.50	0.64	45.00	0.000	0.909	(0; 0)
15	10430.14	-22.36	-3967.85	0.63	45.00	0.000	0.934	(0; 0)
16	10692.05	-19.99	-3655.19	0.62	45.00	0.000	0.957	(0; 0)
17	10922.51	-17.66	-3312.80	0.61	45.00	0.000	0.977	(0; 0)
18	11122.82	-15.35	-2944.67	0.60	45.00	0.000	0.994	(0; 0)
19	11294.04	-13.07	-2554.51	0.60	45.00	0.000	1.008	(0; 0)
20	11437.03	-10.81	-2145.86	0.59	45.00	0.000	1.021	(0; 0)
21	11552.51	-8.57	-1722.09	0.59	45.00	0.000	1.031	(0; 0)
22	11641.02	-6.34	-1286.43	0.58	45.00	0.000	1.038	(0; 0)
23	11702.96	-4.13	-842.03	0.58	45.00	0.000	1.044	(0; 0)
24	11738.62	-1.91	-391.99	0.58	45.00	0.000	1.047	(0; 0)
25	11748.17	0.30	60.67	0.58	45.00	0.000	1.048	(0; 0)
26	11731.64	2.51	512.93	0.58	45.00	0.000	1.046	(0; 0)
27	11688.95	4.72	961.76	0.58	45.00	0.000	1.042	(0; 0)
28	11619.93	6.94	1404.12	0.59	45.00	0.000	1.037	(0; 0)
29	11524.24	9.17	1836.90	0.59	45.00	0.000	1.028	(0; 0)
30	11401.45	11.42	2256.95	0.59	45.00	0.000	1.018	(0; 0)
31	11250.97	13.68	2660.98	0.60	45.00	0.000	1.005	(0; 0)
32	11072.05	15.97	3045.59	0.60	45.00	0.000	0.989	(0; 0)
33	10863.78	18.28	3407.21	0.61	45.00	0.000	0.971	(0; 0)
34	10625.03	20.62	3742.03	0.62	45.00	0.000	0.951	(0; 0)
35	15774.67	23.02	6169.85	0.64	45.00	0.000	0.927	(0; 0)
36	15550.58	25.49	6693.36	0.66	45.00	0.000	0.901	(0; 0)
37	15400.30	28.02	7233.94	0.67	45.00	0.000	0.871	(0; 0)
38	15006.03	30.60	7638.54	0.69	45.00	0.000	0.838	(0; 0)
39	14568.38	33.25	7988.40	0.71	45.00	0.000	0.801	(0; 0)
40	14083.38	35.99	8276.07	0.73	45.00	0.000	0.760	(0; 0)
41	13546.06	38.83	8492.87	0.76	45.00	0.000	0.714	(0; 0)
42	12950.06	41.78	8628.40	0.79	45.00	0.000	0.664	(0; 0)
43	14774.29	44.88	10424.90	0.84	45.00	0.000	0.608	(0; 0)
44	15988.72	48.15	11910.80	0.89	45.00	0.000	0.545	(0; 0)
45	15153.15	51.66	11884.75	0.95	45.00	0.000	0.475	(0; 0)
46	14199.67	55.46	11696.24	1.04	45.00	0.000	0.394	(0; 0)
47	13089.99	59.67	11298.56	1.17	45.00	0.000	0.301	(0; 0)
48	11766.83	64.52	10622.17	1.38	37.00	0.000	0.188	(0; 0)
49	10122.29	70.51	9542.32	1.78	29.00	0.000	0.042	(0; 0)
50	6970.51	81.94	6901.71	4.23	29.00	0.000	0.000	(0; 0)

Resistenza a taglio paratia= 0.00 [kg]

$\Sigma W_i = 538061.43$  [kg]

$\Sigma W_i \sin \alpha_i = 85993.65$  [kg]

$\Sigma W_i \cos \alpha_i \tan \phi_i = 442591.02$  [kg]

$\Sigma c_i b_i / \cos \alpha_i = 0.00$  [kg]



#### Descrizione armatura pali e caratteristiche sezione

Diametro del palo	60.00	[cm]
Area della sezione trasversale	2827.43	[cmq]
Copriferro	3.00	[cm]

L'armatura del palo è costituita da 6 $\phi$ 16( $A_f=12.06$  cmq) longitudinali e staffe  $\phi$ 10/25.0 cm.



## Verifica armatura paratia (Sezioni critiche)

### *Simbologia adottata*

$n^{\circ}$	Indice della combinazione/fase
$Y$	ordinata della sezione rispetto alla testa della paratia espressa in [m]
$\sigma_c$	tensione nel calcestruzzo, espressa in [kg/cm <sup>2</sup> ]
$\sigma_f$	tensione nell'armatura longitudinale del palo, espressa in [kg/cm <sup>2</sup> ]
$\tau_c$	tensione tangenziale nel calcestruzzo, espresso in [kg/cm <sup>2</sup> ]
$\sigma_{st}$	tensione nell'armatura trasversale, espresso in [kg/cm <sup>2</sup> ]

$n^{\circ}$	$\sigma_c$	$Y(\sigma_c)$	$\sigma_f$	$Y(\sigma_f)$	$\tau_c$	$Y(\tau_c)$	$\sigma_{st}$	$Y(\sigma_{st})$
1	22.51	5.00764.72	2.30	1.94	5.001234.02	5.00		
2	26.49	5.00891.89	5.00	2.07	5.001319.98	5.00		
3	26.32	5.00966.68	2.25	2.14	5.001361.75	5.00		
4	35.54	5.001294.10	2.15	2.57	5.001636.35	5.00		



## Verifica armatura paratia (Inviluppo)

### Simbologia adottata

$n^\circ$	Indice della combinazione/fase
$Y$	ordinata della sezione, espressa in [m]
$\sigma_c$	tensione massima nel calcestruzzo, espressa in [kg/cm <sup>2</sup> ]
$\sigma_f$	tensione massima nei ferri longitudinali, espressa in [kg/cm <sup>2</sup> ]
$\sigma_{st}$	tensione massima nei ferri trasversali, espressa in [kg/cm <sup>2</sup> ]

$Y$	$\sigma_c$	$n^\circ$	$\sigma_f$	$n^\circ$	$\tau_c$	$n^\circ$	$\sigma_{st}$	$n^\circ$
0.00	0.00	1	0.00	1	0.83	4	530.06	4
0.05	1.28	4	53.28	4	1.18	4	750.97	4
0.10	2.54	4	105.71	4	1.16	4	739.40	4
0.15	3.78	4	157.25	4	1.14	4	727.60	4
0.20	5.00	4	207.90	4	1.12	4	715.58	4
0.25	6.19	4	257.64	4	1.10	4	703.33	4
0.30	7.37	4	306.45	4	1.09	4	690.86	4
0.35	8.53	4	354.31	4	1.07	4	678.15	4
0.40	9.66	4	401.22	4	1.04	4	665.23	4
0.45	10.77	4	447.14	4	1.02	4	652.07	4
0.50	11.86	4	492.06	4	1.00	4	638.69	4
0.55	12.92	4	535.97	4	0.98	4	625.09	4
0.60	13.97	4	578.85	4	0.96	4	611.26	4
0.65	14.98	4	620.68	4	0.94	4	597.20	4
0.70	15.98	4	661.45	4	0.92	4	582.91	4
0.75	16.95	4	701.14	4	0.89	4	568.40	4
0.80	17.89	4	739.73	4	0.87	4	553.66	4
0.85	18.81	4	777.20	4	0.85	4	538.69	4
0.90	19.70	4	813.54	4	0.82	4	523.50	4
0.95	20.57	4	848.73	4	0.80	4	508.08	4
1.00	21.41	4	882.75	4	0.77	4	492.43	4
1.05	22.22	4	915.59	4	0.75	4	476.56	4
1.10	23.01	4	947.23	4	0.72	4	460.46	4
1.15	23.77	4	977.66	4	0.70	4	444.13	4
1.20	24.50	4	1006.85	4	0.67	4	427.58	4
1.25	25.20	4	1034.78	4	0.65	4	410.80	4
1.30	25.87	4	1061.46	4	0.62	4	393.79	4
1.35	26.52	4	1086.84	4	0.59	4	376.48	4
1.40	27.13	4	1110.91	4	0.56	4	358.79	4
1.45	27.71	4	1133.63	4	0.54	4	340.63	4
1.50	28.27	4	1154.98	4	0.51	4	321.91	4
1.55	28.78	4	1174.90	4	0.48	4	302.69	4
1.60	29.27	4	1193.36	4	0.44	4	283.03	4
1.65	29.72	4	1210.33	4	0.41	4	263.03	4
1.70	30.14	4	1225.80	4	0.38	4	242.77	4
1.75	30.52	4	1239.74	4	0.35	4	222.27	4
1.80	30.87	4	1252.13	4	0.32	4	201.52	4
1.85	31.18	4	1262.96	4	0.28	4	180.51	4
1.90	31.46	4	1272.21	4	0.25	4	159.27	4
1.95	31.70	4	1279.86	4	0.23	2	144.53	2



2.00	31.90	4	1285.89	4	0.21	2	130.64	2
2.05	32.06	4	1290.29	4	0.18	1	116.92	1
2.10	32.19	4	1293.03	4	0.16	1	103.90	1
2.15	32.28	4	1294.10	4	0.14	1	90.56	1
2.20	32.33	4	1293.48	4	0.12	1	76.89	1
2.25	32.34	4	1291.16	4	0.10	1	62.90	1
2.30	32.31	4	1287.12	4	0.08	1	48.58	1
2.35	32.25	4	1281.33	4	0.07	4	43.03	4
2.40	32.14	4	1273.79	4	0.10	4	66.74	4
2.45	31.99	4	1264.47	4	0.14	4	90.70	4
2.50	31.80	4	1253.36	4	0.18	4	114.91	4
2.55	31.57	4	1240.44	4	0.22	4	139.38	4
2.60	31.29	4	1225.70	4	0.26	4	164.11	4
2.65	30.98	4	1209.11	4	0.30	4	189.10	4
2.70	30.62	4	1190.67	4	0.34	4	214.36	4
2.75	30.22	4	1170.35	4	0.38	4	239.88	4
2.80	29.77	4	1148.13	4	0.42	4	265.68	4
2.85	29.28	4	1124.01	4	0.46	4	291.77	4
2.90	28.75	4	1097.97	4	0.50	4	318.15	4
2.95	28.17	4	1069.99	4	0.54	4	344.83	4
3.00	27.55	4	1040.05	4	0.58	4	371.83	4
3.05	26.88	4	1008.14	4	0.63	4	399.17	4
3.10	26.16	4	974.25	4	0.67	4	426.87	4
3.15	25.40	4	938.36	4	0.71	4	454.95	4
3.20	24.59	4	900.46	4	0.76	4	483.44	4
3.25	23.73	4	860.54	4	0.80	4	512.41	4
3.30	22.82	4	818.59	4	0.85	4	541.89	4
3.35	21.86	4	774.59	4	0.90	4	571.97	4
3.40	20.85	4	728.55	4	0.95	4	602.76	4
3.45	19.79	4	680.46	4	1.00	4	634.39	4
3.50	18.68	4	630.33	4	1.05	4	667.07	4
3.55	17.52	4	578.16	4	1.10	4	701.08	4
3.60	16.30	4	523.99	4	1.16	4	736.82	4
3.65	15.03	4	467.85	4	1.22	4	774.94	4
3.70	13.70	4	409.83	4	1.28	4	816.38	4
3.75	12.31	4	350.07	4	1.36	4	862.69	4
3.80	10.85	4	288.82	4	1.44	4	916.39	4
3.85	9.33	4	226.57	4	1.54	4	981.63	4
3.90	7.75	4	164.35	4	1.67	4	1064.61	4
3.95	6.16	3	106.45	3	1.84	4	1168.96	4
4.00	4.88	3	64.37	3	1.98	4	1259.35	4
4.05	3.69	3	47.82	3	1.88	4	1193.85	4
4.10	2.73	3	36.51	3	1.53	4	974.93	4
4.15	2.08	1	28.54	1	1.50	4	953.03	4
4.20	1.61	1	22.72	1	1.54	4	982.30	4
4.25	1.96	4	27.03	4	1.59	4	1011.77	4
4.30	2.88	4	38.56	4	2.05	4	1302.43	4
4.35	4.39	4	56.27	4	2.43	4	1548.69	4
4.40	6.36	4	101.89	4	2.45	4	1557.11	4
4.45	8.52	4	175.68	4	2.36	4	1501.17	4
4.50	10.74	4	258.16	4	2.30	4	1464.22	4
4.55	13.00	4	346.11	4	2.28	4	1449.62	4



4.60	15.31	4	438.14	4	2.28	4	1450.27	4
4.65	17.66	4	533.60	4	2.29	4	1460.73	4
4.70	20.06	4	632.18	4	2.32	4	1477.58	4
4.75	22.51	4	733.67	4	2.35	4	1498.74	4
4.80	25.01	4	837.99	4	2.39	4	1522.90	4
4.85	27.56	4	945.05	4	2.43	4	1549.22	4
4.90	30.17	4	1054.82	4	2.48	4	1577.14	4
4.95	32.83	4	1167.26	4	2.52	4	1606.27	4
5.00	35.54	4	1282.36	4	2.57	4	1636.35	4
5.05	33.73	4	1201.28	4	1.65	4	1047.30	4
5.10	31.98	4	1122.85	4	1.59	4	1015.13	4
5.15	30.28	4	1047.09	4	1.54	4	983.06	4
5.20	28.63	4	974.02	4	1.49	4	951.11	4
5.25	27.05	4	903.63	4	1.44	4	919.61	4
5.30	25.52	4	835.89	4	1.40	4	889.69	4
5.35	24.04	4	770.73	4	1.35	4	861.29	4
5.40	22.61	4	708.09	4	1.31	4	834.48	4
5.45	21.24	4	647.90	4	1.27	4	809.32	4
5.50	19.91	4	590.10	4	1.23	4	785.90	4
5.55	18.62	4	534.64	4	1.20	4	764.29	4
5.60	17.37	4	481.49	4	1.17	4	744.59	4
5.65	16.17	4	430.62	4	1.14	4	726.91	4
5.70	15.00	4	382.01	4	1.12	4	711.34	4
5.75	13.87	4	335.71	4	1.09	4	696.97	4
5.80	12.78	4	291.85	4	1.07	4	682.71	4
5.85	11.73	4	250.64	4	1.05	4	667.07	4
5.90	10.73	4	212.42	4	1.02	4	648.15	4
5.95	9.78	4	177.50	4	0.98	4	625.92	4
6.00	8.89	4	146.16	4	0.94	4	600.13	4
6.05	8.07	4	118.59	4	0.90	4	570.64	4
6.10	7.33	4	94.84	4	0.84	4	537.59	4
6.15	6.85	3	86.88	3	0.79	4	500.47	4
6.20	6.45	3	82.38	3	0.72	4	459.68	4
6.25	6.07	3	78.18	3	0.65	4	416.60	4
6.30	5.73	3	74.29	3	0.59	4	373.10	4
6.35	5.42	3	70.70	3	0.52	4	331.03	4
6.40	5.13	3	67.39	3	0.46	4	291.70	4
6.45	4.87	3	64.34	3	0.40	4	255.80	4
6.50	4.63	3	61.53	3	0.38	3	239.39	3
6.55	4.41	3	58.94	3	0.36	3	230.04	3
6.60	4.21	3	56.56	3	0.34	3	219.03	3
6.65	4.03	3	54.37	3	0.32	3	206.12	3
6.70	3.87	3	52.40	3	0.30	3	193.93	3
6.75	3.72	3	50.62	3	0.29	3	182.54	3
6.80	3.59	3	49.02	3	0.27	3	171.99	3
6.85	3.47	3	47.56	3	0.25	3	162.34	3
6.90	3.36	3	46.23	3	0.24	3	153.71	3
6.95	3.26	3	45.00	3	0.23	3	146.81	3
7.00	3.17	3	43.83	3	0.22	3	142.15	3
7.05	3.07	3	42.71	3	0.22	3	137.54	3
7.10	2.99	3	41.62	3	0.21	3	132.98	3
7.15	2.90	3	40.58	3	0.20	3	128.48	3



7.20	2.82	3	39.58	3	0.19	3	124.04	3
7.25	2.74	3	38.62	3	0.19	3	119.67	3
7.30	2.67	3	37.70	3	0.18	3	115.35	3
7.35	2.59	3	36.82	3	0.17	3	111.11	3
7.40	2.52	3	35.98	3	0.17	3	106.93	3
7.45	2.46	3	35.18	3	0.16	3	102.82	3
7.50	2.40	3	34.41	3	0.16	3	98.79	3
7.55	2.34	3	33.68	3	0.15	3	94.83	3
7.60	2.28	3	32.99	3	0.14	3	90.95	3
7.65	2.22	3	32.34	3	0.14	3	87.14	3
7.70	2.17	3	31.71	3	0.13	3	83.42	3
7.75	2.12	3	31.13	3	0.13	3	79.77	3
7.80	2.08	3	30.57	3	0.12	3	76.20	3
7.85	2.03	3	30.05	3	0.11	3	72.71	3
7.90	1.99	3	29.56	3	0.11	3	69.30	3
7.95	1.97	2	29.30	2	0.10	3	65.97	3
8.00	2.00	2	29.72	2	0.10	3	62.72	3
8.05	2.03	2	30.12	2	0.09	3	59.56	3
8.10	2.06	4	30.58	4	0.09	3	56.47	3
8.15	2.11	4	31.20	4	0.08	3	53.47	3
8.20	2.16	4	31.79	4	0.08	3	50.54	3
8.25	2.20	4	32.36	4	0.07	3	47.70	3
8.30	2.24	4	32.90	4	0.07	3	44.94	3
8.35	2.28	4	33.42	4	0.07	3	42.25	3
8.40	2.32	4	33.92	4	0.06	3	39.65	3
8.45	2.35	4	34.39	4	0.06	3	37.12	3
8.50	2.39	4	34.84	4	0.05	3	34.68	3
8.55	2.42	4	35.28	4	0.05	3	32.31	3
8.60	2.45	4	35.69	4	0.05	3	30.01	3
8.65	2.48	4	36.09	4	0.04	3	27.79	3
8.70	2.50	4	36.46	4	0.04	3	25.64	3
8.75	2.53	4	36.82	4	0.04	3	23.57	3
8.80	2.56	4	37.16	4	0.03	3	21.57	3
8.85	2.58	4	37.49	4	0.03	3	19.64	3
8.90	2.60	4	37.80	4	0.03	3	17.79	3
8.95	2.62	4	38.09	4	0.03	3	16.00	3
9.00	2.64	4	38.37	4	0.02	3	14.27	3
9.05	2.66	4	38.64	4	0.02	3	12.62	3
9.10	2.68	4	38.89	4	0.02	3	11.03	3
9.15	2.70	4	39.13	4	0.01	3	9.50	3
9.20	2.71	4	39.36	4	0.01	3	8.04	3
9.25	2.73	4	39.58	4	0.01	3	6.64	3
9.30	2.74	4	39.78	4	0.01	3	5.30	3
9.35	2.75	4	39.97	4	0.01	3	4.02	3
9.40	2.77	4	40.16	4	0.00	3	2.79	3
9.45	2.78	4	40.33	4	0.00	2	2.42	2
9.50	2.79	3	40.51	3	0.00	2	2.87	2
9.55	2.80	3	40.69	3	0.01	2	3.29	2
9.60	2.81	3	40.86	3	0.01	4	4.00	4
9.65	2.82	3	41.02	3	0.01	4	4.81	4
9.70	2.83	3	41.17	3	0.01	4	5.58	4
9.75	2.84	3	41.32	3	0.01	4	6.30	4



9.80	2.85	3	41.45	3	0.01	4	6.98	4
9.85	2.86	3	41.58	3	0.01	4	7.61	4
9.90	2.87	3	41.71	3	0.01	4	8.21	4
9.95	2.87	3	41.82	3	0.01	4	8.77	4
10.00	2.88	3	41.93	3	0.01	4	9.28	4
10.05	2.89	3	42.04	3	0.02	4	9.76	4
10.10	2.89	3	42.14	3	0.02	4	10.21	4
10.15	2.90	3	42.23	3	0.02	4	10.62	4
10.20	2.90	3	42.32	3	0.02	4	11.00	4
10.25	2.91	3	42.40	3	0.02	4	11.34	4
10.30	2.91	3	42.48	3	0.02	4	11.66	4
10.35	2.91	3	42.56	3	0.02	4	11.94	4
10.40	2.92	3	42.63	3	0.02	4	12.20	4
10.45	2.92	3	42.70	3	0.02	4	12.42	4
10.50	2.92	3	42.77	3	0.02	4	12.62	4
10.55	2.93	3	42.83	3	0.02	4	12.80	4
10.60	2.93	3	42.90	3	0.02	4	12.95	4
10.65	2.93	3	42.96	3	0.02	4	13.08	4
10.70	2.94	3	43.02	3	0.02	4	13.18	4
10.75	2.94	3	43.07	3	0.02	4	13.26	4
10.80	2.94	3	43.13	3	0.02	4	13.32	4
10.85	2.94	3	43.18	3	0.02	3	13.41	3
10.90	2.94	3	43.24	3	0.02	3	13.49	3
10.95	2.95	3	43.29	3	0.02	3	13.55	3
11.00	2.95	3	43.34	3	0.02	3	13.59	3
11.05	2.95	3	43.39	3	0.02	3	13.61	3
11.10	2.95	3	43.44	3	0.02	3	13.61	3
11.15	2.95	3	43.50	3	0.02	3	13.59	3
11.20	2.95	3	43.55	3	0.02	3	13.56	3
11.25	2.96	3	43.60	3	0.02	3	13.51	3
11.30	2.96	3	43.65	3	0.02	3	13.45	3
11.35	2.96	3	43.70	3	0.02	3	13.37	3
11.40	2.96	3	43.76	3	0.02	3	13.27	3
11.45	2.96	3	43.81	3	0.02	3	13.17	3
11.50	2.97	3	43.87	3	0.02	3	13.05	3
11.55	2.97	3	43.93	3	0.02	3	12.92	3
11.60	2.97	3	43.98	3	0.02	3	12.77	3
11.65	2.97	3	44.04	3	0.02	3	12.62	3
11.70	2.98	3	44.10	3	0.02	3	12.46	3
11.75	2.98	3	44.17	3	0.02	3	12.29	3
11.80	2.98	3	44.23	3	0.02	3	12.10	3
11.85	2.99	3	44.29	3	0.02	3	11.91	3
11.90	2.99	3	44.36	3	0.02	3	11.72	3
11.95	2.99	3	44.43	3	0.02	3	11.51	3
12.00	2.99	3	44.50	3	0.02	3	11.30	3
12.05	3.00	3	44.57	3	0.02	3	11.08	3
12.10	3.00	3	44.65	3	0.02	3	10.85	3
12.15	3.01	3	44.73	3	0.02	3	10.62	3
12.20	3.01	3	44.81	3	0.02	3	10.38	3
12.25	3.01	3	44.89	3	0.02	3	10.14	3
12.30	3.02	3	44.97	3	0.02	3	9.89	3
12.35	3.02	3	45.06	3	0.02	3	9.63	3



12.40	3.03	3	45.14	3	0.01	3	9.38	3
12.45	3.03	3	45.23	3	0.01	3	9.12	3
12.50	3.04	3	45.33	3	0.01	3	8.85	3
12.55	3.04	3	45.42	3	0.01	3	8.58	3
12.60	3.05	3	45.52	3	0.01	3	8.31	3
12.65	3.05	3	45.62	3	0.01	3	8.03	3
12.70	3.06	3	45.72	3	0.01	3	7.76	3
12.75	3.07	3	45.83	3	0.01	3	7.47	3
12.80	3.07	3	45.93	3	0.01	3	7.19	3
12.85	3.08	3	46.05	3	0.01	3	6.90	3
12.90	3.09	3	46.16	3	0.01	3	6.62	3
12.95	3.09	3	46.27	3	0.01	3	6.32	3
13.00	3.10	3	46.39	3	0.01	3	6.03	3
13.05	3.11	3	46.51	3	0.01	3	5.74	3
13.10	3.12	3	46.64	3	0.01	3	5.44	3
13.15	3.12	3	46.76	3	0.01	3	5.14	3
13.20	3.13	3	46.89	3	0.01	3	4.84	3
13.25	3.14	3	47.02	3	0.01	3	4.54	3
13.30	3.15	3	47.16	3	0.01	3	4.24	3
13.35	3.16	3	47.30	3	0.01	3	3.93	3
13.40	3.17	3	47.44	3	0.01	3	3.62	3
13.45	3.17	3	47.58	3	0.01	3	3.32	3
13.50	3.18	3	47.73	3	0.00	3	3.01	3
13.55	3.19	3	47.87	3	0.00	3	2.70	3
13.60	3.20	3	48.03	3	0.00	3	2.38	3
13.65	3.21	3	48.18	3	0.00	3	2.07	3
13.70	3.22	3	48.34	3	0.00	3	1.75	3
13.75	3.23	3	48.50	3	0.00	3	1.44	3
13.80	3.24	3	48.66	3	0.00	3	1.12	3
13.85	3.26	3	48.83	3	0.00	3	0.80	3
13.90	3.27	3	49.00	3	0.00	3	0.48	3
13.95	3.28	3	49.17	3	0.00	3	0.16	3



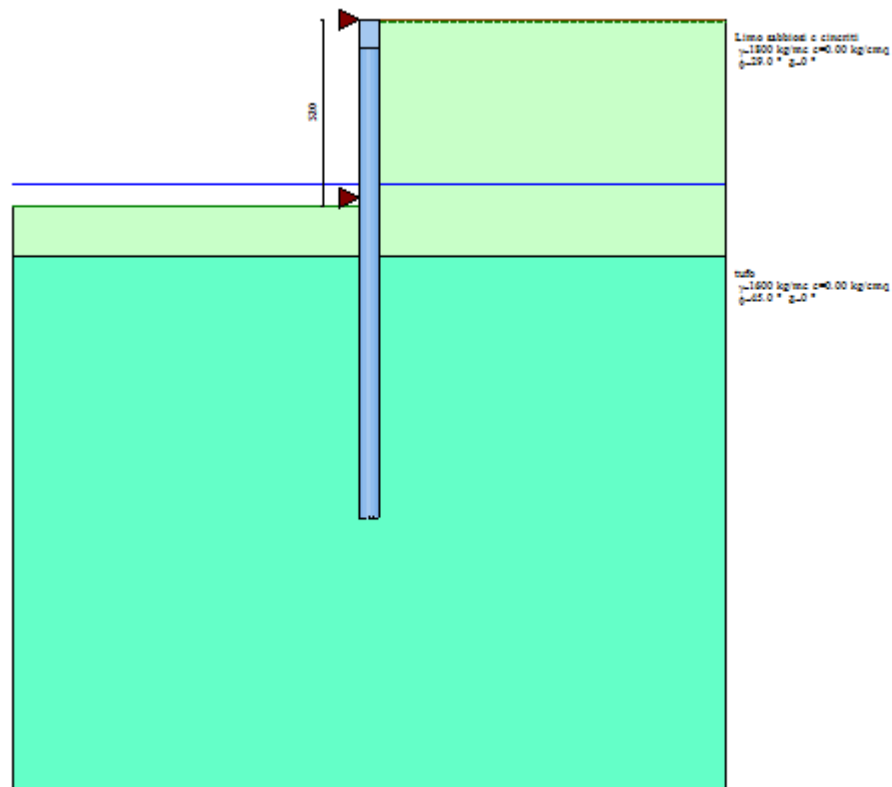
## Verifica sezione cordoli

### *Simbologia adottata*

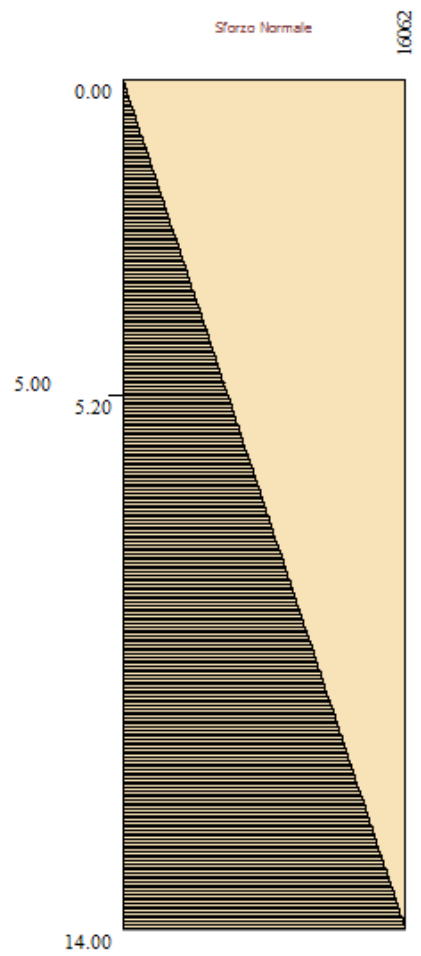
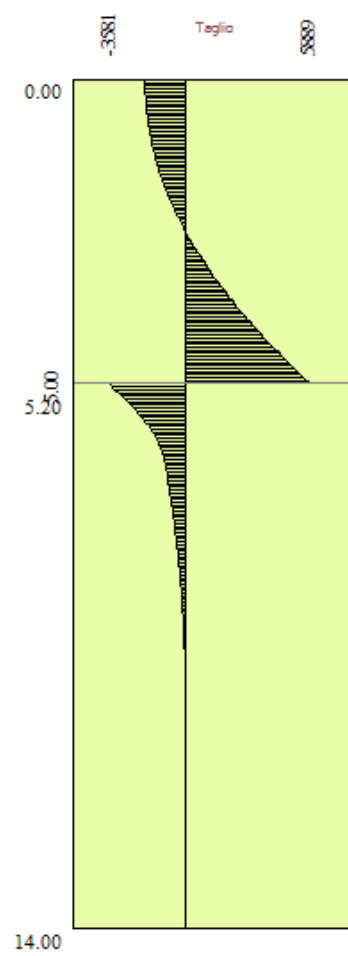
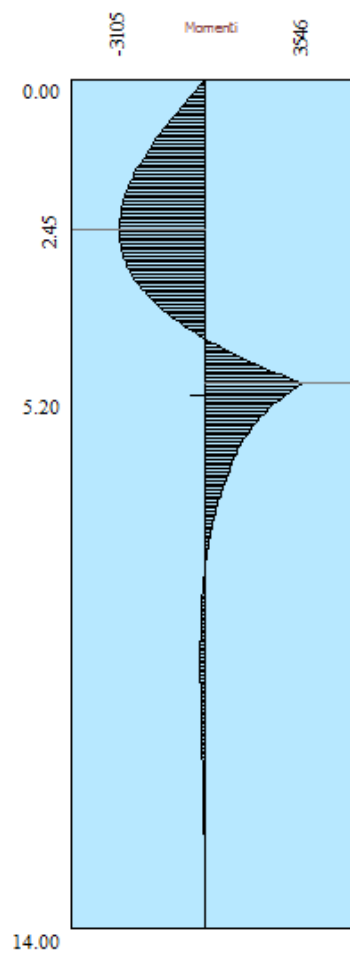
$M_h$	momento flettente espresso in [kgm] nel piano orizzontale
$T_h$	taglio espresso in [kg] nel piano orizzontale
$M_v$	momento flettente espresso in [kgm] nel piano verticale
$T_v$	taglio espresso in [kg] nel piano verticale

### **Cordolo N° 1 (X=0.00 m) (Cordolo in c.a.)**

$B=60.00$ [cm]	$H=80.00$ [cm]		
$A_{fv}=8.04$ [cmq]	$A_{fh}=8.04$ [cmq]	Staffe $\phi 10/25$	$N_{bh}=2 - N_{bv}=2$
$M_h=5824$ [kgm]	$T_h=11648$ [kg]	$M_v=216$ [kgm]	$T_v=720$ [kg]
$\sigma_c = 21.02$ [kg/cmq]	$\sigma_f = 1353.29$ [kg/cmq]	$\tau_c = 2.85$ [kg/cmq]	$\sigma_{staffe} = 3634.86$ [kg/cmq]









# PALIFICATA TIPO – C -

## Geometria paratia

Tipo paratia: **Paratia di pali**

Altezza fuori terra	4.85	[m]
Profondità di infissione	6.45	[m]
Altezza totale della paratia	11.30	[m]
Lunghezza paratia	19.10	[m]

Numero di file di pali	1	
Interasse fra i pali della fila	0.60	[m]
Diametro dei pali	60.00	[cm]
Numero totale di pali	31	
Numero di pali per metro lineare	1.62	

## Geometria cordoli

### *Simbologia adottata*

n°	numero d'ordine del cordolo
Y	posizione del cordolo sull'asse della paratia espresso in [m]

#### Cordoli in calcestruzzo

B	Base della sezione del cordolo espresso in [cm]
H	Altezza della sezione del cordolo espresso in [cm]

#### Cordoli in acciaio

A	Area della sezione in acciaio del cordolo espresso in [cmq]
W	Modulo di resistenza della sezione del cordolo espresso in [cm^3]

n°	Y	Tipo	B	H	A	W
1	0.00	Calcestruzzo	60.00	80.00	--	--

## Geometria profilo terreno

### *Simbologia adottata e sistema di riferimento*

(Sistema di riferimento con origine in testa alla paratia, ascissa X positiva verso monte, ordinata Y positiva verso l'alto)

N	numero ordine del punto
X	ascissa del punto espressa in [m]
Y	ordinata del punto espressa in [m]
A	inclinazione del tratto espressa in [°]

#### **Profilo di monte**

N	X	Y	A
2	10.00	0.00	0.00

#### **Profilo di valle**

N	X	Y	A
1	-10.00	-4.85	0.00
2	0.00	-4.85	0.00



## Descrizione terreni

### *Simbologia adottata*

n°	numero d'ordine dello strato a partire dalla sommità della paratia
Descrizione	Descrizione del terreno
$\gamma$	peso di volume del terreno espresso in [kg/mc]
$\gamma_s$	peso di volume saturo del terreno espresso [kg/mc]
$\phi$	angolo d'attrito interno del terreno espresso in [°]
$\delta$	angolo d'attrito terreno/paratia espresso in [°]
c	coesione del terreno espressa in [kg/cm <sup>2</sup> ]

n°	Descrizione	$\gamma$	$\gamma_s$	$\phi$	$\delta$	c
1	Limo sabbiosi e cineriti	1800.00	1900.00	29.00	0.00	0.000
2	tufo	1600.00	2000.00	45.00	0.00	0.000

## Descrizione stratigrafia

### *Simbologia adottata*

n°	numero d'ordine dello strato a partire dalla sommità della paratia
sp	spessore dello strato in corrispondenza dell'asse della paratia espresso in [m]
kw	costante di Winkler orizzontale espressa in Kg/cm <sup>2</sup> /cm
$\alpha$	inclinazione dello strato espressa in GRADI(°)
Terreno	Terreno associato allo strato

n°	sp	$\alpha$	kw	Terreno
1	11.00	0.00	1.67	Limo sabbiosi e cineriti
2	15.00	0.00	11.99	tufo

## Falda

Profondità della falda a monte rispetto alla sommità della paratia	9.00	[m]
Profondità della falda a valle rispetto alla sommità della paratia	9.00	[m]
Regime delle pressioni neutre:	<b>Idrostatico</b>	

## Caratteristiche materiali utilizzati

### *Calcestruzzo*

Peso specifico	2500	[kg/mc]
Classe di Resistenza	C25/30	
Resistenza caratteristica a compressione $R_{bk}$	306	[kg/cm <sup>2</sup> ]



Tensione di progetto a compressione $\sigma_c$	99	[kg/cm <sup>2</sup> ]
Tensione tangenziale ammissibile $\tau_{c0}$	6.1	[kg/cm <sup>2</sup> ]
Tensione tangenziale ammissibile $\tau_{c1}$	18.5	[kg/cm <sup>2</sup> ]

#### **Acciaio**

Tipo	B450C	
Tensione ammissibile $\sigma_{fa}$	4589	[kg/cm <sup>2</sup> ]
Tensione di snervamento $f_{yk}$	4589	[kg/cm <sup>2</sup> ]

#### **Caratteristiche acciaio cordoli in c.a.**

Tipo	B450C	
Tensione ammissibile $\sigma_{fa}$	4589	[kg/cm <sup>2</sup> ]
Tensione di snervamento $f_{yk}$	4589	[kg/cm <sup>2</sup> ]

### Condizioni di carico

#### **Simbologia e convenzioni adottate**

Le ascisse dei punti di applicazione del carico sono espresse in [m] rispetto alla testa della paratia

Le ordinate dei punti di applicazione del carico sono espresse in [m] rispetto alla testa della paratia

$F_x$	Forza orizzontale espressa in [kg], positiva da monte verso valle
$F_y$	Forza verticale espressa in [kg], positiva verso il basso
$M$	Momento espresso in [kgm], positivo ribaltante
$Q_i, Q_f$	Intensità dei carichi distribuiti sul profilo espresse in [kg/mq]
$V_i, V_s$	Intensità dei carichi distribuiti sulla paratia espresse in [kg/mq], positivi da monte verso valle
$R$	Risultante carico distribuito sulla paratia espressa in [kg]

#### **Condizione n° 1**

Carico distribuito sul profilo	$X_i = 1.00$	$X_f = 5.00$	$Q_i = 500$	$Q_f = 500$
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### Vincoli lungo l'altezza della paratia

#### **Simbologia adottata**

$n^\circ$	numero d'ordine del vincolo
$Y$	ordinata del vincolo rispetto alla testa della paratia espressa in [m]
$V_x$	Vincolo in direzione orizzontale
$K_x$	Rigidezza vincolo in direzione orizzontale espressa in [Kg/cm]
$V_r$	Vincolo alla rotazione
$K_r$	Rigidezza vincolo alla rotazione espressa in [Kg/m°]

$n^\circ$	$Y$	$V_x$	$K_x$	$V_r$	$K_r$
1	4.50	V. RIGIDO	--	LIBERO	--
2	0.00	V. RIGIDO	--	LIBERO	--



## Combinazioni di carico

Nella tabella sono riportate le condizioni di carico di ogni combinazione con il relativo coefficiente di partecipazione.

### Combinazione n° 1

Spinta terreno

### Combinazione n° 2

Spinta terreno

Condizione 1 (folla addensata) x 1.00

### Combinazione n° 3

Spinta terreno

### Combinazione n° 4

Spinta terreno

Condizione 1 (folla addensata) x 1.00

## Impostazioni di progetto

### Spinte e verifiche secondo :

- D.M. 11/03/1988

- D.M. 16/01/1996

### Verifica materiali

Tensioni ammissibili

Impostazioni di analisi

## **Analisi per Combinazioni di Carico.**

Rottura del terreno: Pressione passiva

Influenza  $\delta$  (angolo di attrito terreno-paratia): Nel calcolo del coefficiente di spinta attiva  $K_a$  e nell'inclinazione della spinta attiva (non viene considerato per la spinta passiva)

Stabilità globale: Metodo di Fellenius



## Impostazioni analisi sismica

Coefficiente di intensità sismica (percento) 7.00

Forma del diagramma di incremento sismico triangolare con vertice in basso sulla parte fuori terra

Influenza sisma nella spinta attiva da monte



## Analisi della paratia

### L'analisi è stata eseguita per combinazioni di carico

La paratia è analizzata con il metodo degli elementi finiti.

Essa è discretizzata in 97 elementi fuori terra e 129 elementi al di sotto della linea di fondo scavo.

Le molle che simulano il terreno hanno un comportamento elastoplastico: una volta raggiunta la pressione passiva non reagiscono ad ulteriori incremento di carico.

Altezza fuori terra della paratia	4.85	[m]
Profondità di infissione	6.45	[m]
Altezza totale della paratia	11.30	[m]

### Forze agenti sulla paratia

Tutte le forze si intendono positive se dirette da monte verso valle. Esse sono riferite ad un metro di larghezza della paratia. Le Y hanno come origine la testa della paratia, e sono espresse in [m]

#### Simbologia adottata

n°	Indice della Combinazione/Fase
Tipo	Tipo della Combinazione/Fase
Pa	Spinta attiva, espressa in [kg]
Is	Incremento sismico della spinta, espressa in [kg]
Pw	Spinta della falda, espressa in [kg]
Pp	Resistenza passiva, espressa in [kg]
Pc	Controspinta, espressa in [kg]

n°	Pa	Y <sub>Pa</sub>	Is	Y <sub>Is</sub>	Pw	Y <sub>Pw</sub>	Pp	Y <sub>Pp</sub>	Pc	Y <sub>Pc</sub>
1	8398	3.46	--	--	0	0.00	0	0.00	468	7.56
2	9076	3.47	--	--	0	0.00	0	0.00	502	7.56
3	8407	3.50	1118	1.62	0	0.00	0	0.00	559	7.56
4	9087	3.51	1281	1.62	0	0.00	0	0.00	604	7.56

#### Simbologia adottata

n°	Indice della Combinazione/Fase
Tipo	Tipo della Combinazione/Fase
Rc	Risultante carichi esterni applicati, espressa in [kg]
Rt	Risultante delle reazioni dei tiranti (componente orizzontale), espressa in [kg]
Rv	Risultante delle reazioni dei vincoli, espressa in [kg]
Rp	Risultante delle reazioni dei puntoni, espressa in [kg]

n°	Rc	Y <sub>Rc</sub>	Rt	Y <sub>Rt</sub>	Rv	Y <sub>Rv</sub>	Rp	Y <sub>Rp</sub>
1	0	0.00	--	--	-8867	3.68	--	--
2	0	0.00	--	--	-9579	3.69	--	--
3	0	0.00	--	--	-10084	3.51	--	--
4	0	0.00	--	--	-10972	3.51	--	--

#### Simbologia adottata

n°	Indice della Combinazione/Fase
P <sub>NUL</sub>	Punto di nullo del diagramma, espresso in [m]



$P_{INV}$	Punto di inversione del diagramma, espresso in [m]
$C_{ROT}$	Punto Centro di rotazione, espresso in [m]
$MP$	Percentuale molle plasticizzate, espressa in [%]
$R/R_{MAX}$	Rapporto tra lo sforzo reale nelle molle e lo sforzo che le molle sarebbero in grado di esplicare, espresso in [%]
$Pp$	Portanza di punta, espressa in [kg]

$n^{\circ}$	$P_{NUL}$	$P_{INV}$	$C_{ROT}$	$MP$	$R/R_{MAX}$	$Pp$
1	5.51	4.85	-1.60	0.00	0.17	514774
2	5.55	4.85	-1.60	0.00	0.19	514774
3	5.51	4.85	-1.60	0.00	0.21	514774
4	5.55	4.85	-1.60	0.00	0.23	514774



## Risultati vincoli

### *Simbologia adottata*

n°	Indice del vincolo
Y	posizione del vincolo rispetto alla testa della paratia espressa in [m]
R <sub>x</sub> /ml	reazione in direzione orizzontale a metro lineare, positiva verso valle, espressa in [kg]
R <sub>θ</sub> /ml	reazione momento a metro lineare, positiva antioraria, espressa in [kgm]
u	spostamento orizzontale, positivo verso valle, espresso in [cm]

#### **Combinazione n° 1**

n°	Y	R <sub>x</sub>	R <sub>θ</sub>	u
1	4.50	-7252.22	--	0.00
2	0.00	-1614.64	--	0.00

#### **Combinazione n° 2**

n°	Y	R <sub>x</sub>	R <sub>θ</sub>	u
1	4.50	-7847.29	--	0.00
2	0.00	-1731.29	--	0.00

#### **Combinazione n° 3**

n°	Y	R <sub>x</sub>	R <sub>θ</sub>	u
1	4.50	-7873.19	--	0.00
2	0.00	-2210.58	--	0.00

#### **Combinazione n° 4**

n°	Y	R <sub>x</sub>	R <sub>θ</sub>	u
1	4.50	-8566.66	--	0.00
2	0.00	-2405.77	--	0.00



## Valori massimi e minimi sollecitazioni per metro di paratia

### *Simbologia adottata*

n°	Indice della combinazione/fase
Tipo	Tipo della combinazione/fase
Y	ordinata della sezione rispetto alla testa espressa in [m]
M	momento flettente massimo e minimo espresso in [kgm]
N	sforzo normale massimo e minimo espresso in [kg] (positivo di compressione)
T	taglio massimo e minimo espresso in [kg]

<b>n°</b>	<b>M</b>	<b>Y<sub>M</sub></b>	<b>T</b>	<b>Y<sub>T</sub></b>	<b>N</b>	<b>Y<sub>N</sub></b>	
1	2220	4.50	4709	4.50	12964	11.30	MAX
--	-2447	2.25	-2543	4.50	0	0.00	MIN
2	2421	4.50	5085	4.50	12964	11.30	MAX
--	-2664	2.25	-2763	4.50	0	0.00	MIN
3	2517	4.50	5191	4.50	12964	11.30	MAX
--	-2908	2.20	-2682	4.50	0	0.00	MIN
4	2761	4.50	5639	4.50	12964	11.30	MAX
--	-3188	2.20	-2928	4.50	0	0.00	MIN



## Spostamenti massimi e minimi della paratia

### *Simbologia adottata*

n°	Indice della combinazione/fase
Tipo	Tipo della combinazione/fase
Y	ordinata della sezione rispetto alla testa della paratia espressa in [m]
U	spostamento orizzontale massimo e minimo espresso in [cm] positivo verso valle
V	spostamento verticale massimo e minimo espresso in [cm] positivo verso il basso

<b>n°</b>	<b>U</b>	<b>Y<sub>U</sub></b>	<b>V</b>	<b>Y<sub>V</sub></b>	
1	0.0144	2.20	0.0051	0.00	MAX
--	-0.0065	6.80	0.0000	0.00	MIN
2	0.0157	2.20	0.0051	0.00	MAX
--	-0.0070	6.80	0.0000	0.00	MIN
3	0.0172	2.20	0.0051	0.00	MAX
--	-0.0078	6.80	0.0000	0.00	MIN
4	0.0188	2.20	0.0051	0.00	MAX
--	-0.0084	6.80	0.0000	0.00	MIN



## Stabilità globale

### Metodo di Fellenius

Numero di cerchi analizzati 100

#### Simbologia adottata

n°	Indice della combinazione/fase
Tipo	Tipo della combinazione/fase
(X <sub>C</sub> ; Y <sub>C</sub> )	Coordinate centro cerchio superficie di scorrimento, espresse in [m]
R	Raggio cerchio superficie di scorrimento, espresso in [m]
(X <sub>V</sub> ; Y <sub>V</sub> )	Coordinate intersezione del cerchio con il pendio a valle, espresse in [m]
(X <sub>M</sub> ; Y <sub>M</sub> )	Coordinate intersezione del cerchio con il pendio a monte, espresse in [m]
FS	Coefficiente di sicurezza

n°	(X <sub>C</sub> , Y <sub>C</sub> )	R	(X <sub>V</sub> , Y <sub>V</sub> )	(X <sub>M</sub> , Y <sub>M</sub> )	FS
1	(-1.13; 0.00)	11.36	(-11.41; -4.83)	(10.23; 0.00)	3.10
2	(-1.13; 0.00)	11.36	(-11.41; -4.83)	(10.23; 0.00)	3.08
3	(-1.13; 1.13)	12.48	(-12.10; -4.83)	(11.31; 0.00)	2.56
4	(-2.26; 2.26)	13.75	(-14.04; -4.83)	(11.31; 0.00)	2.54

### Combinazione n° 4

Numero di strisce 50

#### Simbologia adottata

Le ascisse X sono considerate positive verso monte	
Le ordinate Y sono considerate positive verso l'alto	
Origine in testa alla paratia (spigolo contro terra)	
Le strisce sono numerate da monte verso valle	
N°	numero d'ordine della striscia
W	peso della striscia espresso in [kg]
α	angolo fra la base della striscia e l'orizzontale espresso in gradi (positivo antiorario)
φ	angolo d'attrito del terreno lungo la base della striscia
c	coesione del terreno lungo la base della striscia espressa in [kg/cm <sup>2</sup> ]
b	larghezza della striscia espressa in [m]
L	sviluppo della base della striscia espressa in [m] (L=b/cosα)
u	pressione neutra lungo la base della striscia espressa in [kg/cm <sup>2</sup> ]
Ctn, Ctt	contributo alla striscia normale e tangenziale del tirante espresse in [kg]

### Caratteristiche delle strisce

N°	W	α(°)	Wsinα	L	φ	c	u	(Ctn; Ctt)
1	331.54	-57.03	-278.14	0.92	29.00	0.000	0.000	(0; 0)
2	984.30	-53.36	-789.78	0.84	29.00	0.000	0.000	(0; 0)
3	1557.78	-49.98	-1193.00	0.78	29.00	0.000	0.000	(0; 0)
4	2068.29	-46.83	-1508.44	0.73	29.00	0.000	0.000	(0; 0)
5	2526.72	-43.85	-1750.54	0.70	29.00	0.000	0.000	(0; 0)
6	2940.79	-41.02	-1930.09	0.66	29.00	0.000	0.000	(0; 0)
7	3316.21	-38.30	-2055.47	0.64	29.00	0.000	0.000	(0; 0)
8	3657.80	-35.69	-2133.72	0.62	29.00	0.000	0.000	(0; 0)
9	3979.88	-33.15	-2176.40	0.60	29.00	0.000	0.025	(0; 0)
10	4277.52	-30.69	-2183.11	0.58	29.00	0.000	0.056	(0; 0)



11	4547.71	-28.29	-2155.10	0.57	29.00	0.000	0.084	(0; 0)
12	4792.33	-25.94	-2096.20	0.56	29.00	0.000	0.110	(0; 0)
13	5012.96	-23.64	-2009.84	0.55	29.00	0.000	0.133	(0; 0)
14	5210.89	-21.37	-1899.12	0.54	29.00	0.000	0.154	(0; 0)
15	5387.23	-19.15	-1766.88	0.53	29.00	0.000	0.172	(0; 0)
16	5542.88	-16.95	-1615.75	0.52	29.00	0.000	0.189	(0; 0)
17	5680.36	-14.78	-1448.63	0.52	37.00	0.000	0.203	(0; 0)
18	5802.69	-12.62	-1268.18	0.51	45.00	0.000	0.215	(0; 0)
19	5905.52	-10.49	-1075.25	0.51	45.00	0.000	0.225	(0; 0)
20	5989.04	-8.37	-872.01	0.51	45.00	0.000	0.234	(0; 0)
21	6053.62	-6.26	-660.61	0.50	45.00	0.000	0.240	(0; 0)
22	6099.52	-4.17	-443.15	0.50	45.00	0.000	0.245	(0; 0)
23	6126.93	-2.07	-221.67	0.50	45.00	0.000	0.248	(0; 0)
24	6135.95	0.02	1.81	0.50	45.00	0.000	0.248	(0; 0)
25	6126.63	2.11	225.26	0.50	45.00	0.000	0.248	(0; 0)
26	6098.92	4.20	446.70	0.50	45.00	0.000	0.245	(0; 0)
27	6052.73	6.30	664.08	0.50	45.00	0.000	0.240	(0; 0)
28	5987.84	8.41	875.36	0.51	45.00	0.000	0.234	(0; 0)
29	10538.30	10.55	1929.83	0.52	45.00	0.000	0.225	(0; 0)
30	10443.33	12.74	2302.96	0.53	45.00	0.000	0.215	(0; 0)
31	10556.57	14.95	2722.69	0.53	37.00	0.000	0.202	(0; 0)
32	10410.56	17.18	3074.33	0.54	29.00	0.000	0.187	(0; 0)
33	10244.46	19.43	3408.38	0.55	29.00	0.000	0.170	(0; 0)
34	10055.96	21.72	3721.72	0.55	29.00	0.000	0.151	(0; 0)
35	9844.01	24.05	4011.41	0.56	29.00	0.000	0.129	(0; 0)
36	9607.37	26.42	4274.28	0.57	29.00	0.000	0.105	(0; 0)
37	9344.55	28.84	4506.83	0.59	29.00	0.000	0.078	(0; 0)
38	8983.96	31.31	4668.94	0.60	29.00	0.000	0.048	(0; 0)
39	8475.80	33.86	4721.87	0.62	29.00	0.000	0.015	(0; 0)
40	8132.64	36.48	4834.91	0.64	29.00	0.000	0.000	(0; 0)
41	7763.03	39.19	4905.59	0.66	29.00	0.000	0.000	(0; 0)
42	7355.02	42.02	4922.94	0.69	29.00	0.000	0.000	(0; 0)
43	6903.35	44.97	4878.96	0.73	29.00	0.000	0.000	(0; 0)
44	6400.99	48.09	4763.51	0.77	29.00	0.000	0.000	(0; 0)
45	5838.21	51.41	4563.33	0.82	29.00	0.000	0.000	(0; 0)
46	5200.84	54.99	4260.01	0.90	29.00	0.000	0.000	(0; 0)
47	4466.68	58.94	3826.23	1.00	29.00	0.000	0.000	(0; 0)
48	3597.06	63.41	3216.56	1.15	29.00	0.000	0.000	(0; 0)
49	2510.50	68.76	2339.96	1.42	29.00	0.000	0.000	(0; 0)
50	949.43	75.94	921.00	2.12	29.00	0.000	0.000	(0; 0)

Resistenza a taglio paratia= 0.00 [kg]

$\Sigma W_i = 295817.18$  [kg]

$\Sigma W_i \sin \alpha_i = 51458.34$  [kg]

$\Sigma W_i \cos \alpha_i \tan \phi_i = 184887.81$  [kg]

$\Sigma c_i b_i / \cos \alpha_i = 0.00$  [kg]



#### Descrizione armatura pali e caratteristiche sezione

Diametro del palo	60.00	[cm]
Area della sezione trasversale	2827.43	[cmq]
Copriferro	3.00	[cm]

L'armatura del palo è costituita da 6 $\phi$ 16( $A_f=12.06$  cmq) longitudinali e staffe  $\phi$ 8/20.0 cm.



## Verifica armatura paratia (Sezioni critiche)

### *Simbologia adottata*

$n^{\circ}$	Indice della combinazione/fase
$Y$	ordinata della sezione rispetto alla testa della paratia espressa in [m]
$\sigma_c$	tensione nel calcestruzzo, espressa in [kg/cm <sup>2</sup> ]
$\sigma_f$	tensione nell'armatura longitudinale del palo, espressa in [kg/cm <sup>2</sup> ]
$\tau_c$	tensione tangenziale nel calcestruzzo, espresso in [kg/cm <sup>2</sup> ]
$\sigma_{st}$	tensione nell'armatura trasversale, espresso in [kg/cm <sup>2</sup> ]

$n^{\circ}$	$\sigma_c$	$Y(\sigma_c)$	$\sigma_f$	$Y(\sigma_f)$	$\tau_c$	$Y(\tau_c)$	$\sigma_{st}$	$Y(\sigma_{st})$
1	15.91	2.25580.15	2.10	2.10	1.65	4.251313.94	4.25	4.25
2	17.38	2.25644.19	2.10	2.10	1.75	4.201395.44	4.20	4.20
3	19.07	2.15722.08	2.05	2.05	1.79	4.201427.29	4.20	4.20
4	20.97	2.15805.28	2.05	2.05	1.92	4.151525.09	4.15	4.15



## Verifica armatura paratia (Inviluppo)

### *Simbologia adottata*

$n^\circ$	Indice della combinazione/fase
$Y$	ordinata della sezione, espressa in [m]
$\sigma_c$	tensione massima nel calcestruzzo, espressa in [kg/cm <sup>2</sup> ]
$\sigma_f$	tensione massima nei ferri longitudinali, espressa in [kg/cm <sup>2</sup> ]
$\sigma_{st}$	tensione massima nei ferri trasversali, espressa in [kg/cm <sup>2</sup> ]

$Y$	$\sigma_c$	$n^\circ$	$\sigma_f$	$n^\circ$	$\tau_c$	$n^\circ$	$\sigma_{st}$	$n^\circ$
0.00	0.00	1	0.00	1	0.52	4	417.18	4
0.05	0.80	4	32.28	4	0.75	4	593.24	4
0.10	1.59	4	64.20	4	0.74	4	587.11	4
0.15	2.37	4	95.74	4	0.73	4	580.64	4
0.20	3.14	4	126.88	4	0.72	4	573.83	4
0.25	3.90	4	157.60	4	0.71	4	566.68	4
0.30	4.65	4	187.89	4	0.70	4	559.19	4
0.35	5.39	4	217.71	4	0.69	4	551.37	4
0.40	6.12	4	247.05	4	0.68	4	543.20	4
0.45	6.84	4	275.88	4	0.67	4	534.70	4
0.50	7.55	4	304.20	4	0.66	4	525.86	4
0.55	8.24	4	331.98	4	0.65	4	516.69	4
0.60	8.92	4	359.19	4	0.64	4	507.17	4
0.65	9.59	4	385.82	4	0.62	4	497.31	4
0.70	10.25	4	411.85	4	0.61	4	487.12	4
0.75	10.89	4	437.25	4	0.60	4	476.59	4
0.80	11.51	4	462.02	4	0.59	4	465.72	4
0.85	12.13	4	486.11	4	0.57	4	454.51	4
0.90	12.72	4	509.53	4	0.56	4	442.96	4
0.95	13.30	4	532.24	4	0.54	4	431.07	4
1.00	13.86	4	554.23	4	0.53	4	418.85	4
1.05	14.41	4	575.47	4	0.51	4	406.28	4
1.10	14.94	4	595.95	4	0.49	4	393.37	4
1.15	15.45	4	615.64	4	0.48	4	380.13	4
1.20	15.94	4	634.52	4	0.46	4	366.54	4
1.25	16.42	4	652.59	4	0.44	4	352.61	4
1.30	16.87	4	669.80	4	0.43	4	338.34	4
1.35	17.31	4	686.15	4	0.41	4	323.68	4
1.40	17.72	4	701.60	4	0.39	4	308.43	4
1.45	18.12	4	716.12	4	0.37	4	292.56	4
1.50	18.49	4	729.66	4	0.35	4	275.92	4
1.55	18.83	4	742.19	4	0.32	4	258.56	4
1.60	19.16	4	753.66	4	0.30	4	240.66	4
1.65	19.46	4	764.05	4	0.28	4	222.25	4
1.70	19.73	4	773.32	4	0.26	4	203.47	4
1.75	19.98	4	781.46	4	0.23	2	184.34	2
1.80	20.20	4	788.44	4	0.21	2	168.66	2
1.85	20.40	4	794.25	4	0.19	2	152.55	2
1.90	20.56	4	798.86	4	0.17	2	136.02	2
1.95	20.70	4	802.25	4	0.15	2	119.07	2



2.00	20.82	4	804.39	4	0.13	2	101.69	2
2.05	20.90	4	805.28	4	0.11	2	83.90	2
2.10	20.95	4	804.89	4	0.08	2	65.68	2
2.15	20.97	4	803.19	4	0.06	2	47.03	2
2.20	20.97	4	800.17	4	0.04	2	27.95	2
2.25	20.93	4	795.80	4	0.03	4	27.63	4
2.30	20.86	4	790.07	4	0.06	4	50.89	4
2.35	20.76	4	782.96	4	0.09	4	74.54	4
2.40	20.63	4	774.44	4	0.12	4	98.58	4
2.45	20.46	4	764.50	4	0.15	4	123.01	4
2.50	20.26	4	753.11	4	0.19	4	147.85	4
2.55	20.03	4	740.27	4	0.22	4	173.11	4
2.60	19.76	4	725.93	4	0.25	4	198.80	4
2.65	19.46	4	710.10	4	0.28	4	224.92	4
2.70	19.12	4	692.75	4	0.32	4	251.51	4
2.75	18.74	4	673.86	4	0.35	4	278.57	4
2.80	18.33	4	653.42	4	0.38	4	306.14	4
2.85	17.88	4	631.40	4	0.42	4	334.25	4
2.90	17.40	4	607.80	4	0.46	4	362.94	4
2.95	16.87	4	582.60	4	0.49	4	392.27	4
3.00	16.31	4	555.79	4	0.53	4	422.31	4
3.05	15.71	4	527.35	4	0.57	4	453.15	4
3.10	15.06	4	497.28	4	0.61	4	484.91	4
3.15	14.37	4	465.57	4	0.65	4	517.76	4
3.20	13.65	4	432.24	4	0.69	4	551.93	4
3.25	12.87	4	397.29	4	0.74	4	587.74	4
3.30	12.06	4	360.75	4	0.79	4	625.62	4
3.35	11.19	4	322.66	4	0.84	4	666.24	4
3.40	10.28	4	283.12	4	0.89	4	710.56	4
3.45	9.32	4	242.27	4	0.96	4	760.01	4
3.50	8.31	4	200.38	4	1.03	4	816.71	4
3.55	7.25	4	157.92	4	1.11	4	883.51	4
3.60	6.14	4	115.82	4	1.21	4	962.91	4
3.65	4.99	4	75.91	4	1.32	4	1050.33	4
3.70	3.87	4	49.82	4	1.40	4	1111.32	4
3.75	2.90	4	38.41	4	1.35	4	1071.92	4
3.80	2.17	4	29.53	4	1.17	4	933.96	4
3.85	1.66	2	23.13	2	1.08	4	860.20	4
3.90	1.24	1	17.87	1	1.12	4	891.48	4
3.95	1.22	4	17.63	4	1.16	4	923.07	4
4.00	1.78	4	24.73	4	1.20	4	954.98	4
4.05	2.42	4	32.87	4	1.44	4	1147.93	4
4.10	3.39	4	44.68	4	1.77	4	1405.97	4
4.15	4.73	4	60.32	4	1.92	4	1525.09	4
4.20	6.31	4	105.98	4	1.91	4	1517.87	4
4.25	8.00	4	164.04	4	1.87	4	1484.95	4
4.30	9.75	4	228.25	4	1.84	4	1463.74	4
4.35	11.54	4	296.82	4	1.83	4	1457.58	4
4.40	13.37	4	368.89	4	1.84	4	1463.13	4
4.45	15.24	4	443.99	4	1.86	4	1477.06	4
4.50	17.16	4	521.89	4	1.88	4	1496.97	4
4.55	16.14	4	477.16	4	0.93	4	743.06	4



4.60	15.17	4	434.93	4	0.89	4	708.49	4
4.65	14.26	4	395.23	4	0.85	4	673.43	4
4.70	13.40	4	358.11	4	0.80	4	637.74	4
4.75	12.59	4	323.61	4	0.76	4	601.23	4
4.80	11.83	4	291.77	4	0.71	4	563.66	4
4.85	11.13	4	262.63	4	0.66	4	524.77	4
4.90	10.49	4	236.18	4	0.61	4	485.06	4
4.95	9.90	4	212.32	4	0.56	4	447.65	4
5.00	9.36	4	190.88	4	0.52	4	412.17	4
5.05	8.87	4	171.70	4	0.48	4	378.65	4
5.10	8.42	4	154.60	4	0.44	4	347.16	4
5.15	8.02	4	139.39	4	0.40	4	317.81	4
5.20	7.66	4	125.89	4	0.37	4	290.76	4
5.25	7.33	4	113.91	4	0.33	4	266.21	4
5.30	7.03	4	103.27	4	0.31	4	244.36	4
5.35	6.76	4	93.80	4	0.28	4	225.42	4
5.40	6.51	4	85.32	4	0.26	4	209.55	4
5.45	6.29	4	80.04	4	0.25	4	196.92	4
5.50	6.08	4	77.74	4	0.24	4	187.62	4
5.55	5.88	4	75.55	4	0.23	4	181.74	4
5.60	5.69	4	73.47	4	0.22	4	178.50	4
5.65	5.51	4	71.45	4	0.22	4	175.78	4
5.70	5.34	4	69.52	4	0.22	4	172.71	4
5.75	5.18	4	67.66	4	0.21	4	169.32	4
5.80	5.02	4	65.88	4	0.21	4	165.64	4
5.85	4.88	4	64.19	4	0.20	4	161.72	4
5.90	4.74	4	62.59	4	0.20	4	157.61	4
5.95	4.60	4	61.06	4	0.19	4	153.35	4
6.00	4.48	4	59.63	4	0.19	4	149.00	4
6.05	4.37	4	58.27	4	0.18	4	144.59	4
6.10	4.26	4	57.00	4	0.18	4	140.17	4
6.15	4.16	4	55.80	4	0.17	4	135.78	4
6.20	4.06	4	54.68	4	0.17	4	131.43	4
6.25	3.97	4	53.63	4	0.16	4	127.17	4
6.30	3.89	4	52.64	4	0.15	4	123.01	4
6.35	3.81	4	51.72	4	0.15	4	118.96	4
6.40	3.74	4	50.86	4	0.14	4	115.03	4
6.45	3.67	4	50.05	4	0.14	4	111.24	4
6.50	3.61	4	49.30	4	0.14	4	107.60	4
6.55	3.55	4	48.59	4	0.13	4	104.09	4
6.60	3.50	4	47.93	4	0.13	4	100.73	4
6.65	3.44	4	47.32	4	0.12	4	97.53	4
6.70	3.40	4	46.74	4	0.12	4	94.48	4
6.75	3.35	4	46.20	4	0.12	4	91.59	4
6.80	3.31	4	45.68	4	0.11	4	88.90	4
6.85	3.27	4	45.20	4	0.11	4	86.45	4
6.90	3.23	4	44.74	4	0.11	4	84.48	4
6.95	3.19	4	44.29	4	0.10	4	82.88	4
7.00	3.16	4	43.86	4	0.10	4	81.28	4
7.05	3.12	4	43.43	4	0.10	4	79.68	4
7.10	3.09	4	43.02	4	0.10	4	78.09	4
7.15	3.05	4	42.62	4	0.10	4	76.50	4



7.20	3.02	4	42.23	4	0.09	4	74.92	4
7.25	2.99	4	41.86	4	0.09	4	73.34	4
7.30	2.96	4	41.49	4	0.09	4	71.77	4
7.35	2.93	4	41.14	4	0.09	4	70.22	4
7.40	2.90	4	40.80	4	0.09	4	68.66	4
7.45	2.87	4	40.47	4	0.08	4	67.12	4
7.50	2.84	4	40.15	4	0.08	4	65.59	4
7.55	2.82	4	39.84	4	0.08	4	64.07	4
7.60	2.79	4	39.54	4	0.08	4	62.56	4
7.65	2.77	4	39.26	4	0.08	4	61.06	4
7.70	2.74	4	38.98	4	0.07	4	59.58	4
7.75	2.72	4	38.72	4	0.07	4	58.10	4
7.80	2.70	4	38.47	4	0.07	4	56.64	4
7.85	2.68	4	38.22	4	0.07	4	55.20	4
7.90	2.66	4	37.99	4	0.07	4	53.77	4
7.95	2.64	4	37.77	4	0.07	4	52.35	4
8.00	2.62	4	37.56	4	0.06	4	50.95	4
8.05	2.60	4	37.36	4	0.06	4	49.56	4
8.10	2.58	4	37.17	4	0.06	4	48.19	4
8.15	2.57	4	36.99	4	0.06	4	46.83	4
8.20	2.55	4	36.82	4	0.06	4	45.49	4
8.25	2.54	4	36.66	4	0.06	4	44.17	4
8.30	2.52	4	36.52	4	0.05	4	42.87	4
8.35	2.51	4	36.37	4	0.05	4	41.58	4
8.40	2.50	4	36.24	4	0.05	4	40.31	4
8.45	2.48	4	36.12	4	0.05	4	39.06	4
8.50	2.47	4	36.01	4	0.05	4	37.83	4
8.55	2.46	4	35.91	4	0.05	4	36.62	4
8.60	2.45	4	35.81	4	0.04	4	35.42	4
8.65	2.45	4	35.73	4	0.04	4	34.25	4
8.70	2.44	4	35.65	4	0.04	4	33.09	4
8.75	2.43	4	35.58	4	0.04	4	31.96	4
8.80	2.42	4	35.52	4	0.04	4	30.84	4
8.85	2.42	4	35.47	4	0.04	4	29.75	4
8.90	2.41	4	35.43	4	0.04	4	28.67	4
8.95	2.41	4	35.39	4	0.03	4	27.61	4
9.00	2.40	4	35.37	4	0.03	4	26.58	4
9.05	2.40	4	35.35	4	0.03	4	25.57	4
9.10	2.40	4	35.33	4	0.03	4	24.57	4
9.15	2.39	4	35.33	4	0.03	4	23.60	4
9.20	2.39	4	35.33	4	0.03	4	22.65	4
9.25	2.39	4	35.34	4	0.03	4	21.72	4
9.30	2.39	4	35.36	4	0.03	4	20.81	4
9.35	2.39	4	35.38	4	0.03	4	19.92	4
9.40	2.39	4	35.41	4	0.02	4	19.06	4
9.45	2.39	4	35.44	4	0.02	4	18.22	4
9.50	2.39	4	35.49	4	0.02	4	17.40	4
9.55	2.39	4	35.53	4	0.02	4	16.60	4
9.60	2.39	4	35.59	4	0.02	4	15.82	4
9.65	2.40	4	35.65	4	0.02	4	15.06	4
9.70	2.40	4	35.71	4	0.02	4	14.33	4
9.75	2.40	4	35.78	4	0.02	4	13.62	4



9.80	2.41	4	35.86	4	0.02	4	12.93	4
9.85	2.41	4	35.94	4	0.02	4	12.26	4
9.90	2.42	4	36.02	4	0.01	4	11.62	4
9.95	2.42	4	36.12	4	0.01	4	11.00	4
10.00	2.43	4	36.21	4	0.01	4	10.40	4
10.05	2.43	4	36.31	4	0.01	4	9.82	4
10.10	2.44	4	36.41	4	0.01	4	9.27	4
10.15	2.44	4	36.52	4	0.01	4	8.74	4
10.20	2.45	4	36.63	4	0.01	4	8.23	4
10.25	2.46	4	36.75	4	0.01	4	7.74	4
10.30	2.46	4	36.87	4	0.01	4	7.28	4
10.35	2.47	4	36.99	4	0.01	4	6.84	4
10.40	2.48	4	37.12	4	0.01	4	6.42	4
10.45	2.49	4	37.24	4	0.01	4	6.02	4
10.50	2.50	4	37.38	4	0.01	4	5.65	4
10.55	2.50	4	37.51	4	0.01	4	5.30	4
10.60	2.51	4	37.65	4	0.01	4	4.97	4
10.65	2.52	4	37.79	4	0.01	4	4.67	4
10.70	2.53	4	37.93	4	0.01	4	4.39	4
10.75	2.54	4	38.07	4	0.01	4	4.13	4
10.80	2.55	4	38.22	4	0.00	4	3.89	4
10.85	2.56	4	38.37	4	0.00	4	3.68	4
10.90	2.57	4	38.52	4	0.00	4	3.49	4
10.95	2.58	4	38.67	4	0.00	4	3.32	4
11.00	2.59	4	38.82	4	0.00	4	2.73	4
11.05	2.60	4	38.97	4	0.00	4	1.86	4
11.10	2.61	4	39.14	4	0.00	4	1.16	4
11.15	2.62	4	39.30	4	0.00	4	0.62	4
11.20	2.63	4	39.48	4	0.00	4	0.24	4
11.25	2.64	4	39.65	4	0.00	4	0.03	4



## Verifica sezione cordoli

### Simbologia adottata

$M_h$	momento flettente espresso in [kgm] nel piano orizzontale
$T_h$	taglio espresso in [kg] nel piano orizzontale
$M_v$	momento flettente espresso in [kgm] nel piano verticale
$T_v$	taglio espresso in [kg] nel piano verticale

### **Cordolo N° 1 (X=0.00 m) (Cordolo in c.a.)**

$B=60.00$  [cm]       $H=80.00$  [cm]

$A_{fv}=8.04$  [cmq]       $A_{fh}=8.04$  [cmq]

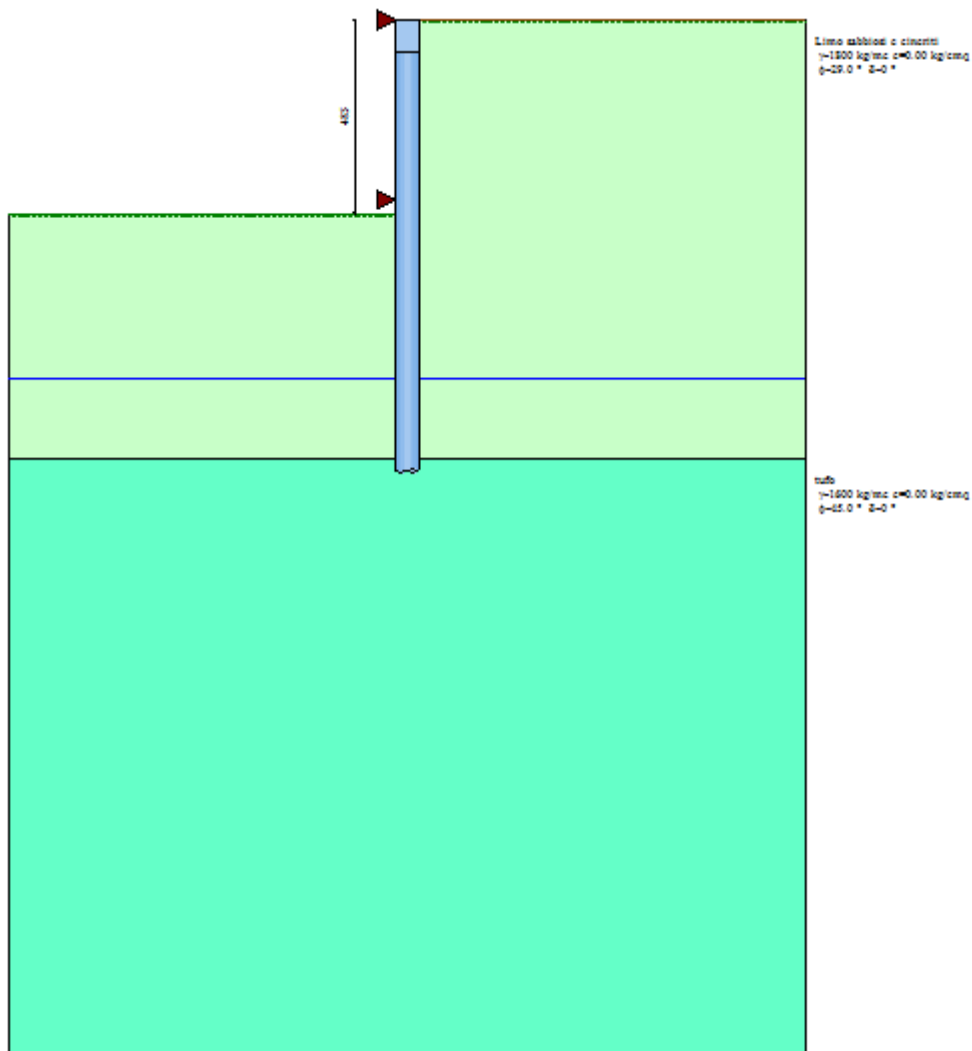
$M_h=3733$  [kgm]       $T_h=7465$  [kg]      Staffe  $\phi 10/25$

$N_{bh}=2$  -  $N_{bv}=2$

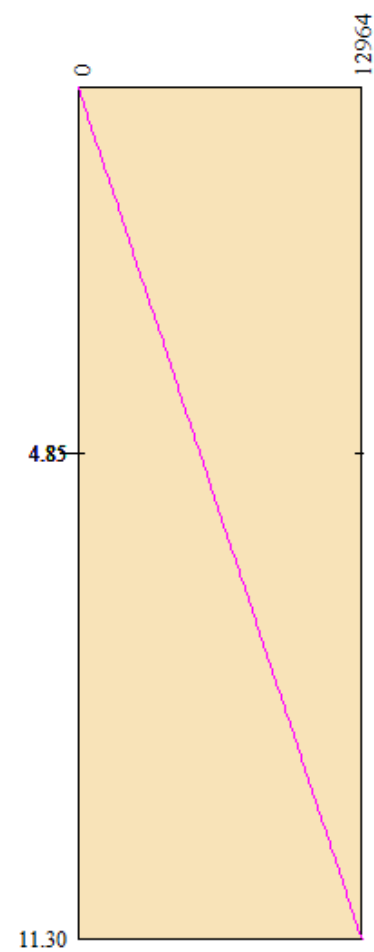
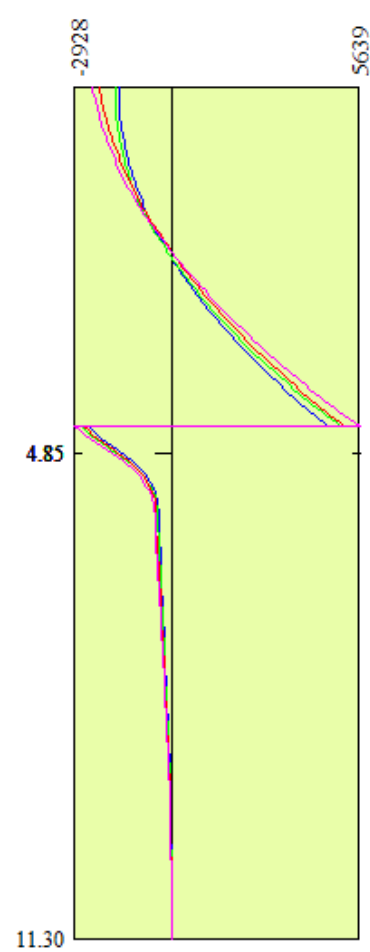
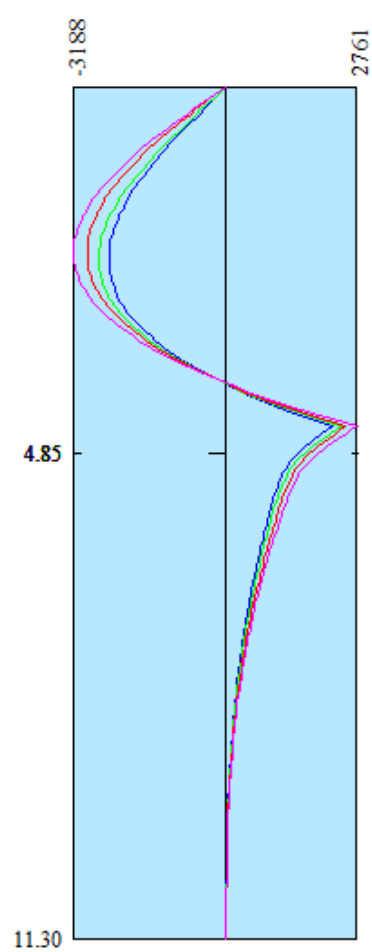
$T_v=720$  [kg]

$\sigma_c = 13.47$  [kg/cmq]       $\sigma_f = 867.35$  [kg/cmq]       $\tau_c = 1.83$  [kg/cmq]

$\sigma_{staffe} = 2329.67$  [kg/cmq]









## 4 – ILLUSTRAZIONE SINTETICA DEI RISULTATI

Il presente documento riporta gli **elaborati grafici sintetici** in conformità a quanto previsto nel par. 10.2 del D.M. 14 gennaio 2008.

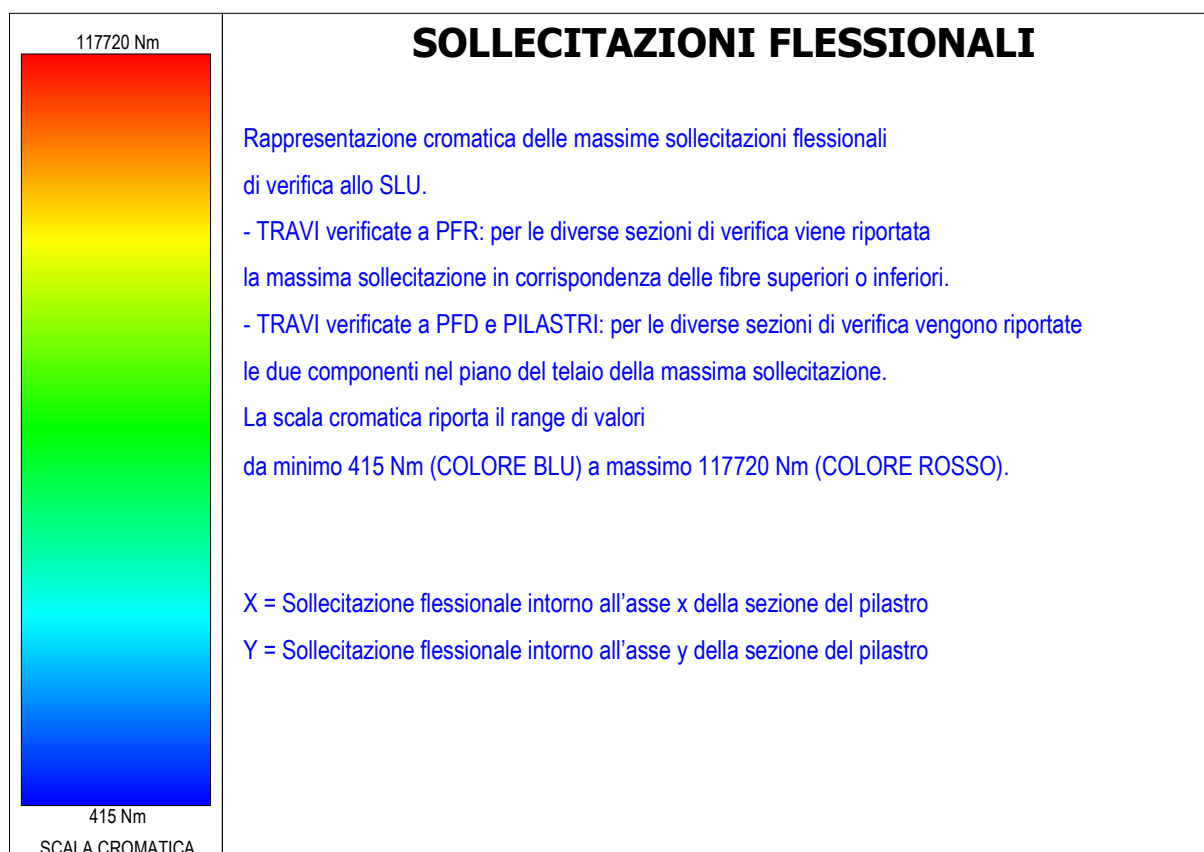
Tali elaborati hanno lo scopo di riassumere il comportamento della struttura relativamente al tipo di analisi svolta e possono riportare informazioni sintetiche e schemi relativi a carichi, sollecitazioni e sforzi, spostamenti, tensioni sul terreno, etc.

Al fine delle verifiche della misura della sicurezza, si riportano delle rappresentazioni che ne sintetizzano i valori numerici dei coefficienti di sicurezza nelle sezioni significative della struttura stessa.

Per ogni singolo elaborato grafico, contenente un telaio, una parte della struttura o la struttura nel suo insieme, si riportano indicazioni sulle convenzioni adottate e sulle unità di misura, nonché disegni, schemi grafici e mappature cromatiche che schematizzano il comportamento complessivo della struttura.

Grazie alle mappature a colori, per ciascun tipo di risultato, si fornisce un quadro chiaro e sintetico: è possibile rilevare agevolmente il valore delle diverse grandezze in base al colore assunto dagli elementi della struttura. Ogni colore rappresenta un determinato valore, dal blu (corrispondente generalmente al valore minimo) al rosso (generalmente valore massimo), passando attraverso le varie sfumature di colore corrispondenti ai valori intermedi.

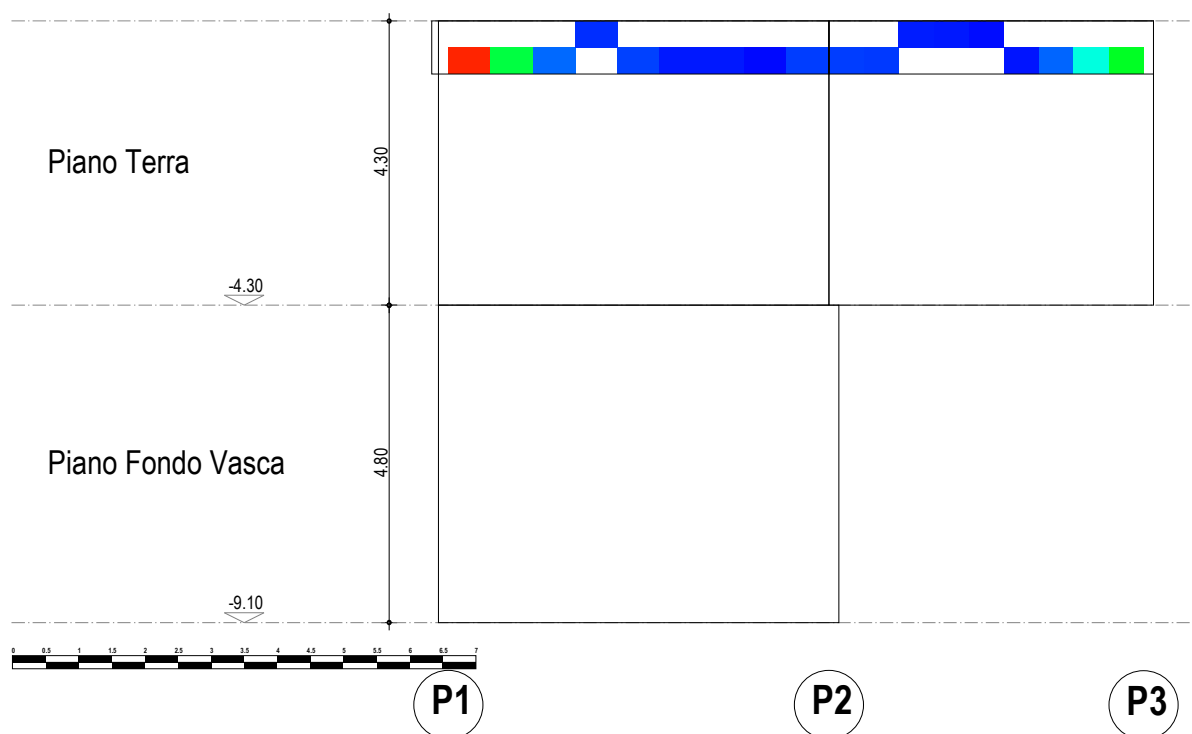
Prima di ogni tipologia di risultato è riportata la scala cromatica con l'indicazione numerica del valore minimo e massimo.





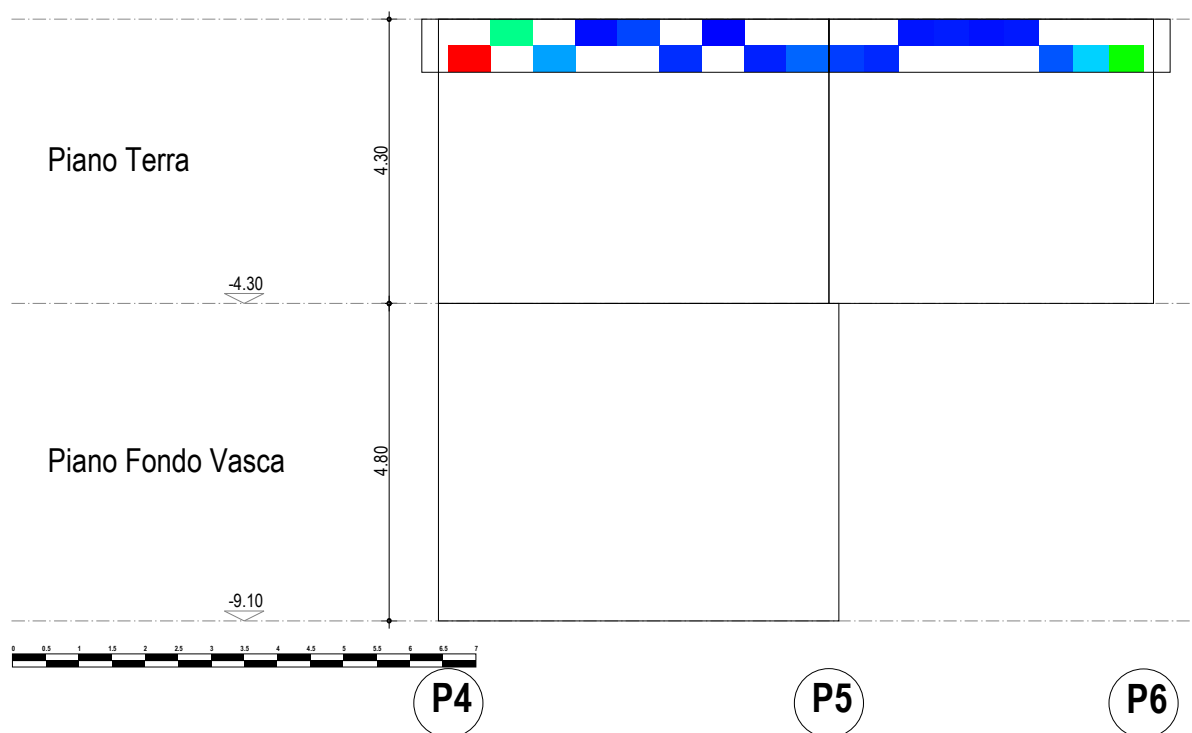
## Telaio P1-P2-P3

SOLLECITAZIONI FLESSIONALI



## Telaio P4-P5-P6

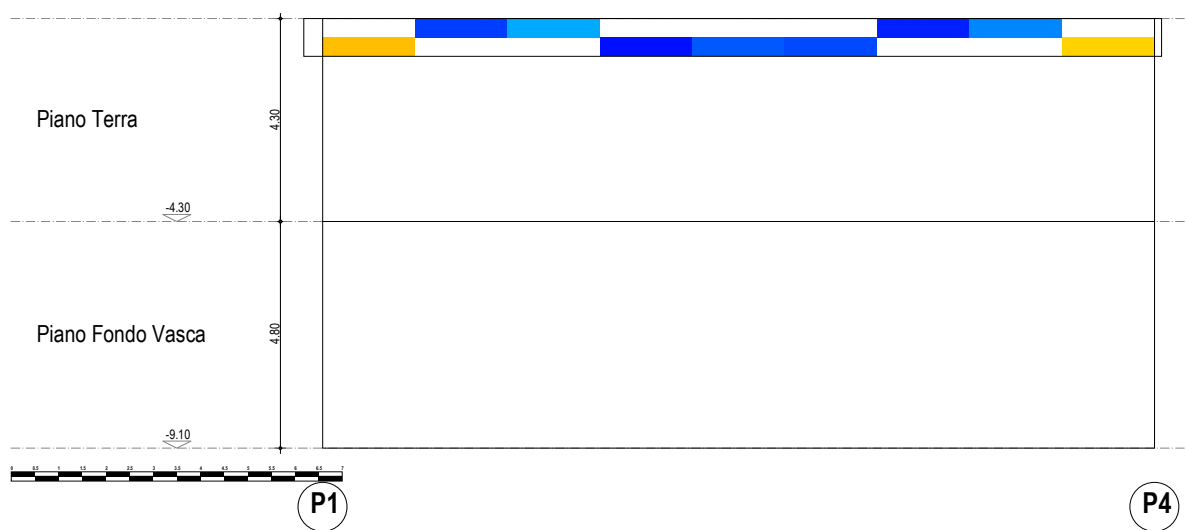
SOLLECITAZIONI FLESSIONALI





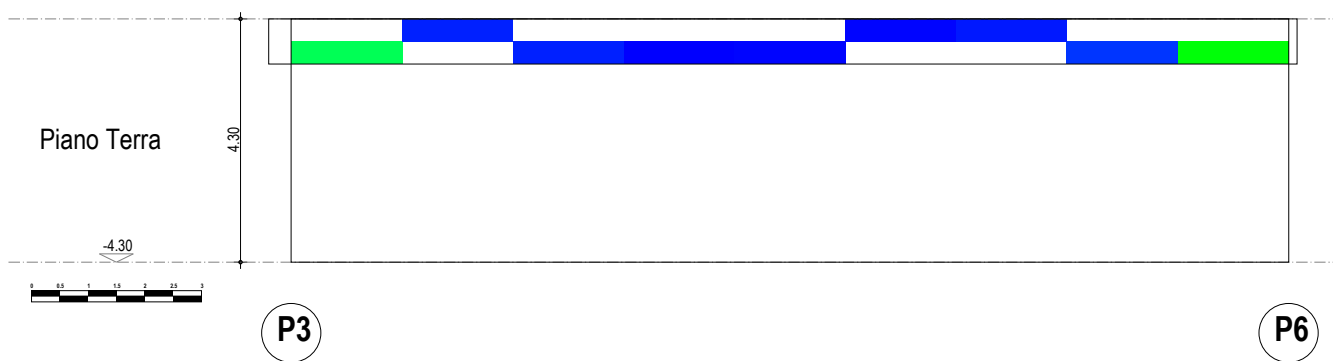
### Telaio P1-P4

SOLLECITAZIONI FLESSIONALI



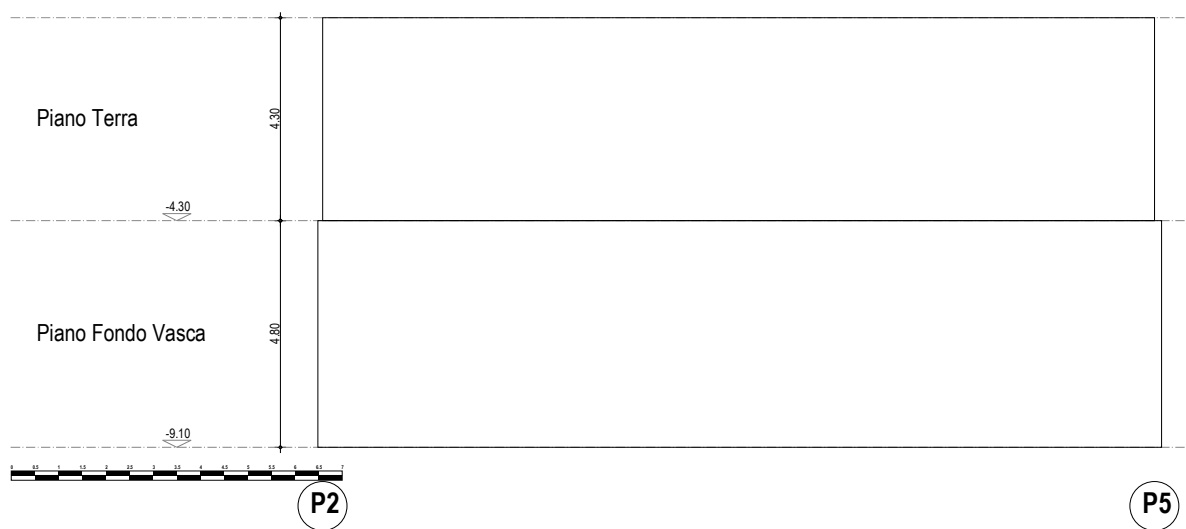
### Telaio P3-P6

SOLLECITAZIONI FLESSIONALI

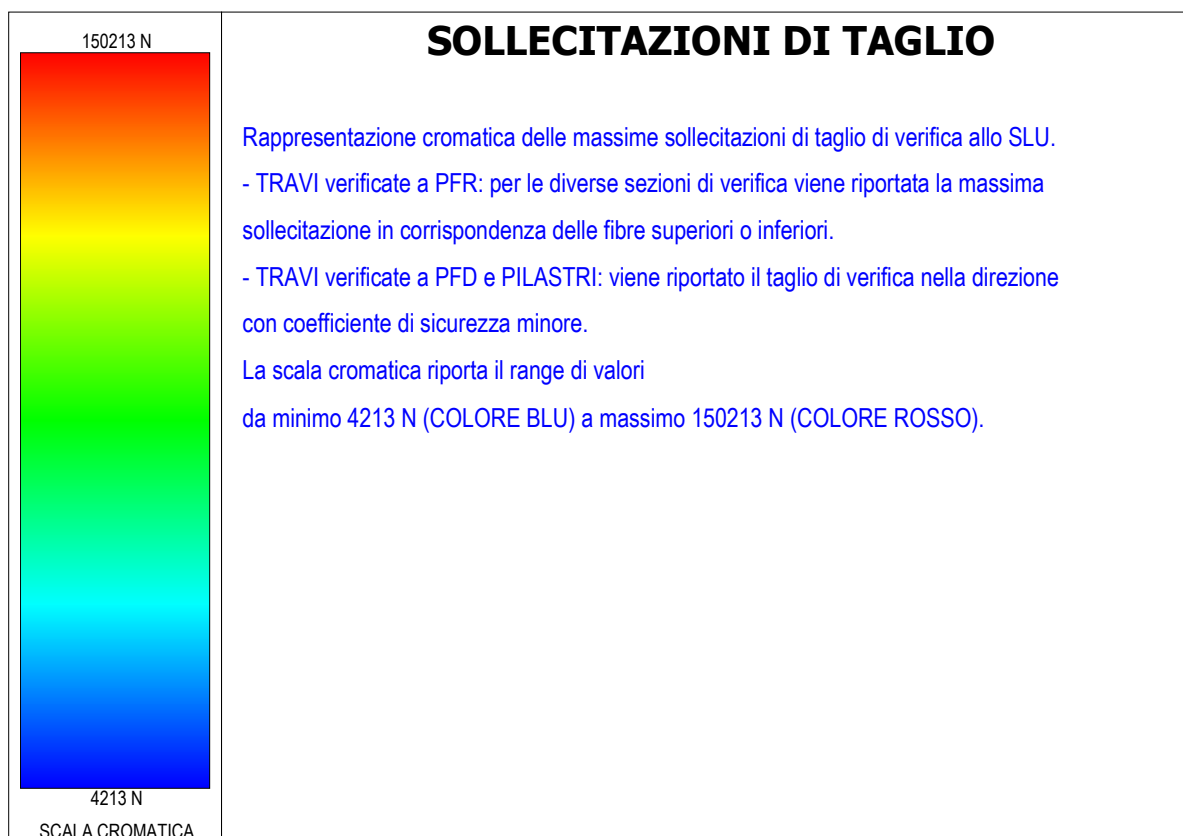


### Telaio P2-P5

SOLLECITAZIONI FLESSIONALI

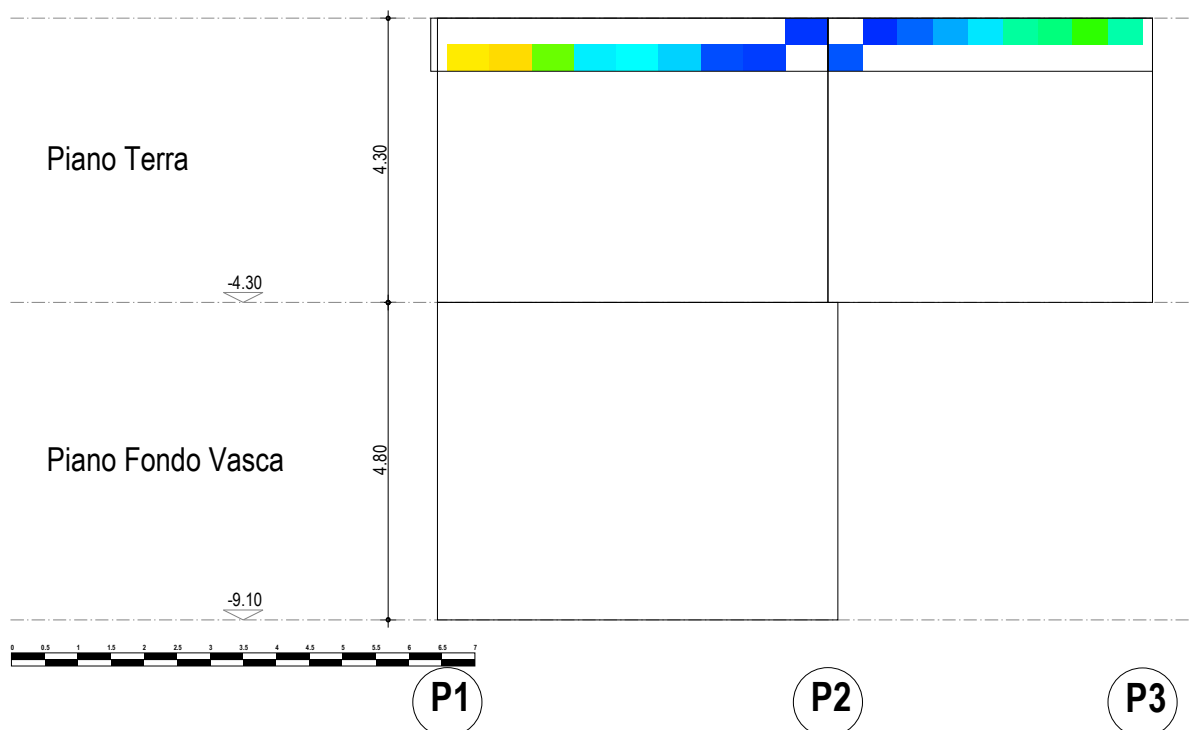






### Telaio P1-P2-P3

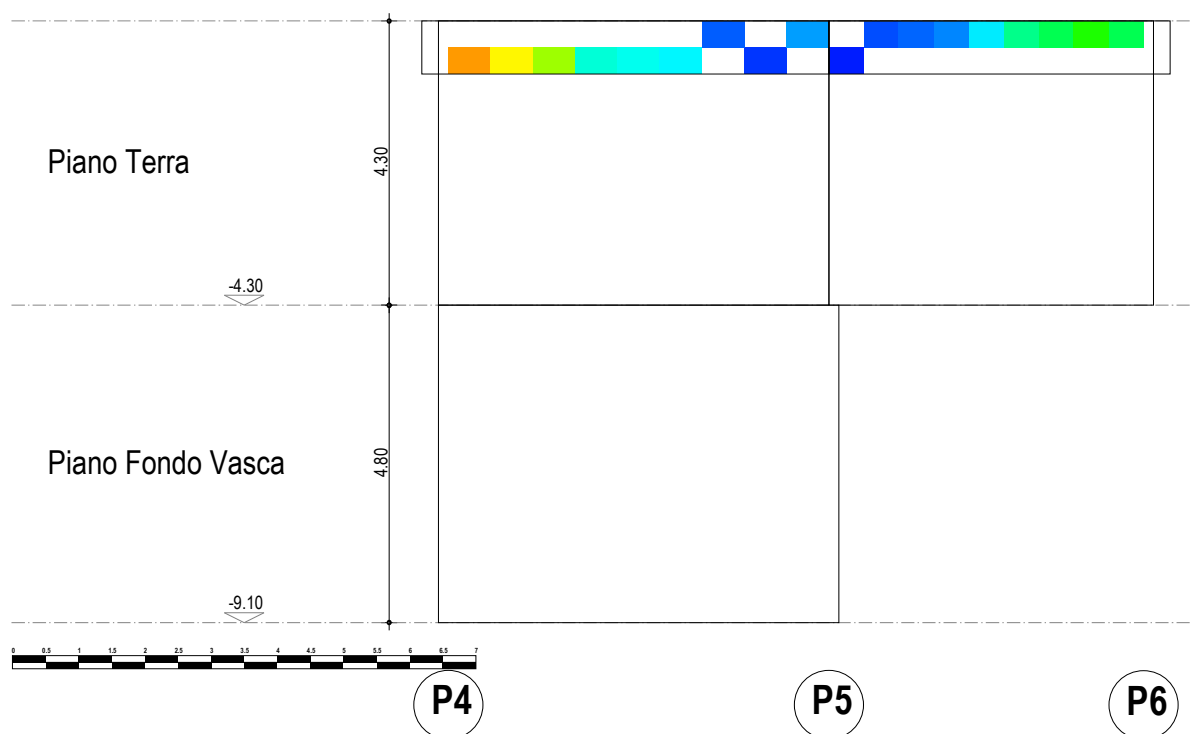
SOLLECITAZIONI DI TAGLIO





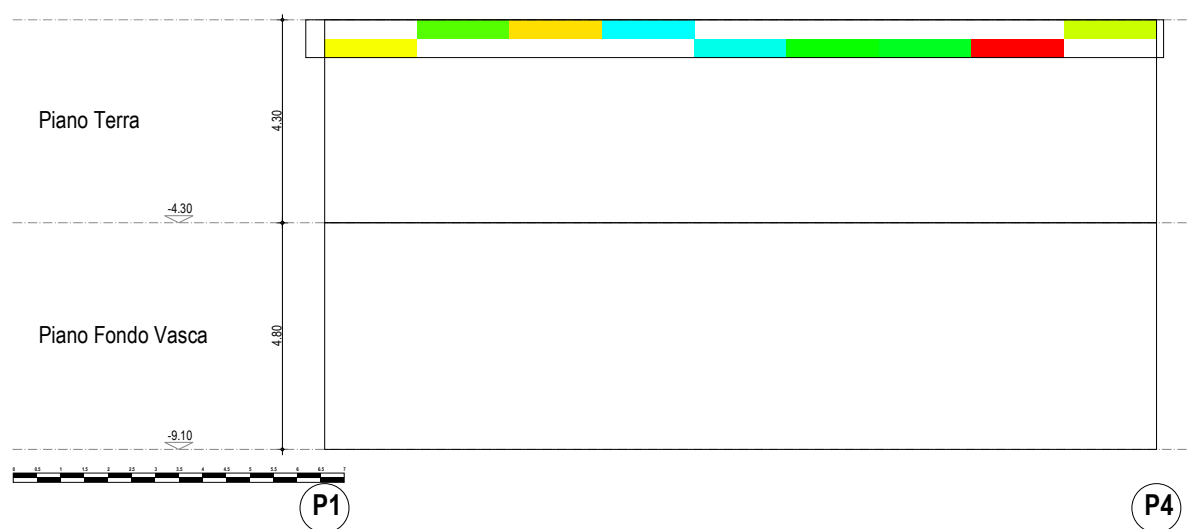
## Telaio P4-P5-P6

SOLLECITAZIONI DI TAGLIO



## Telaio P1-P4

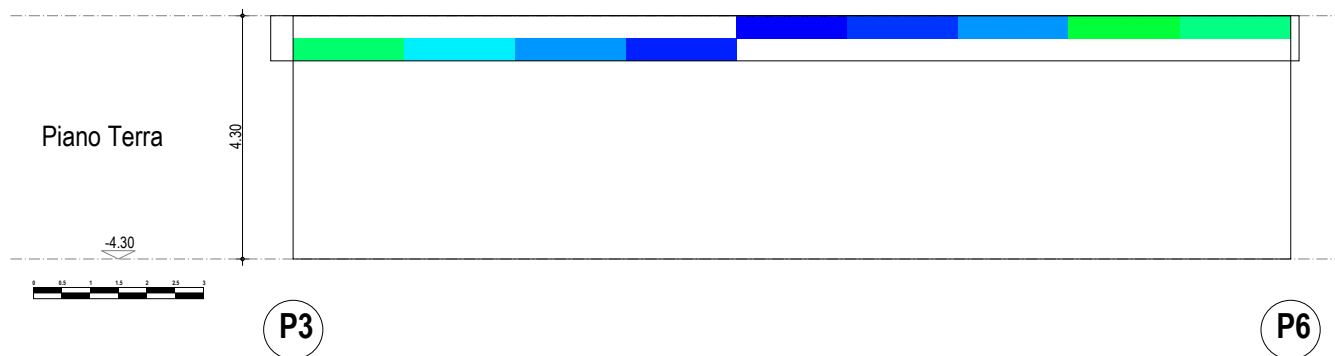
SOLLECITAZIONI DI TAGLIO





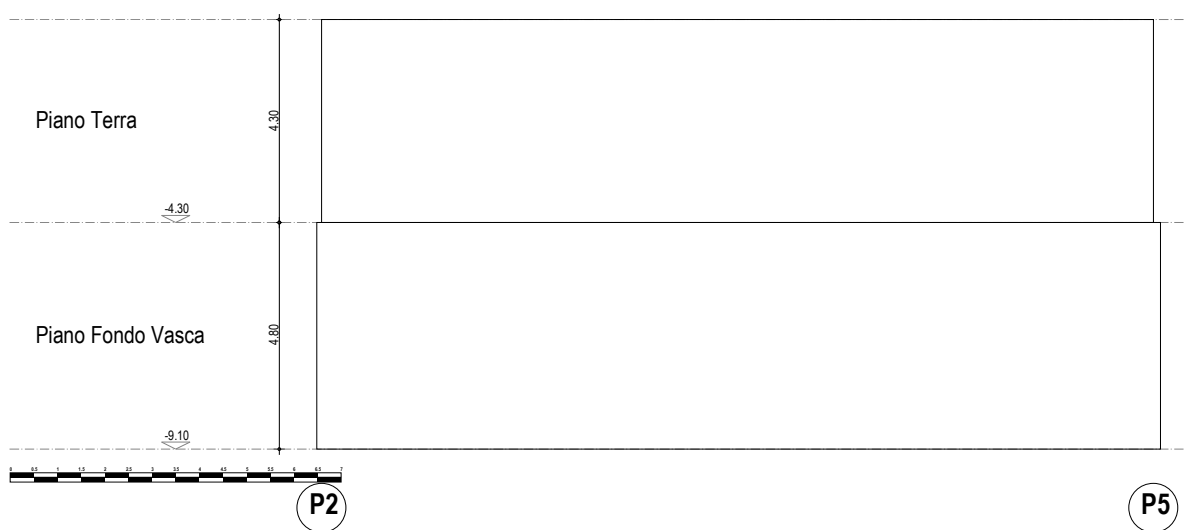
### Telaio P3-P6

SOLLECITAZIONI DI TAGLIO



### Telaio P2-P5

SOLLECITAZIONI DI TAGLIO

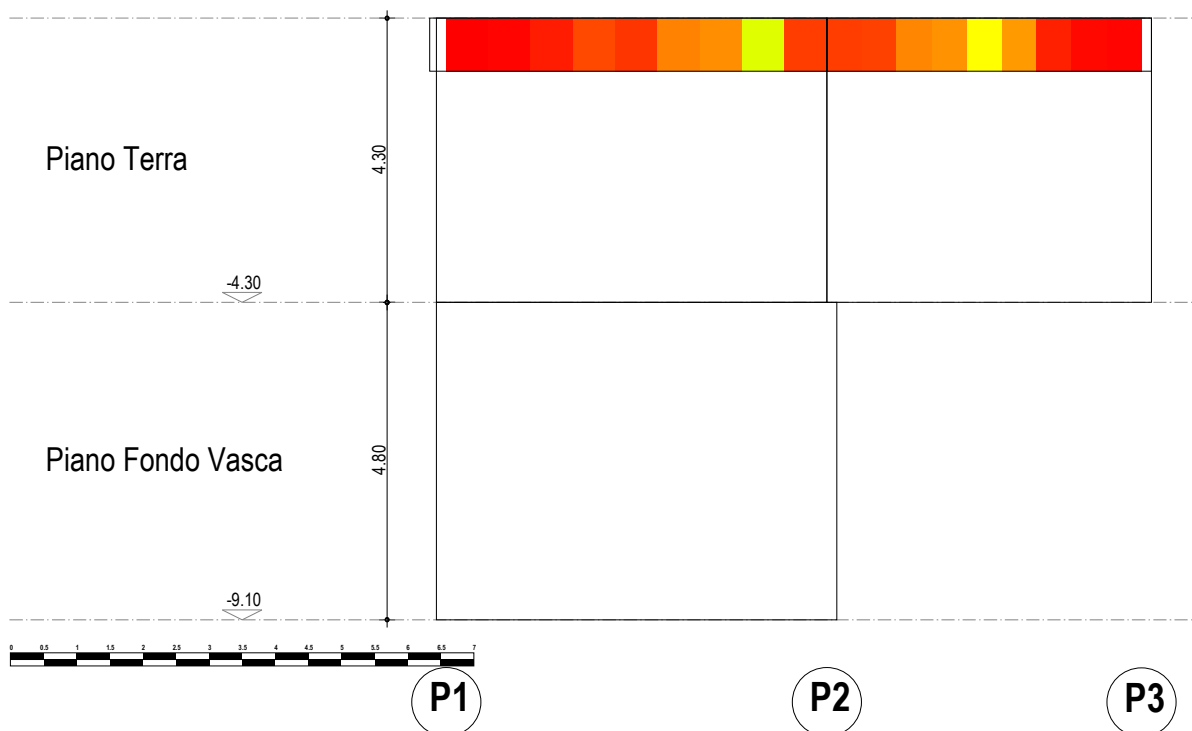






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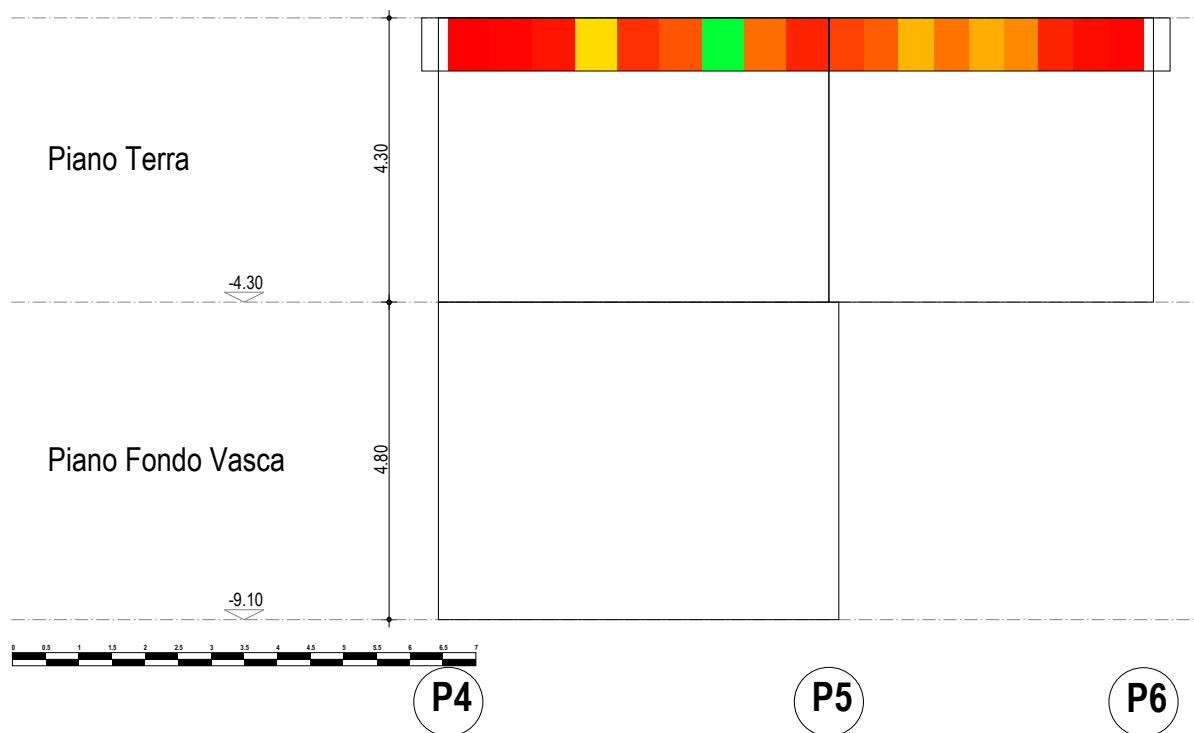
COEFFICIENTE DI SICUREZZA A FLESSIONE





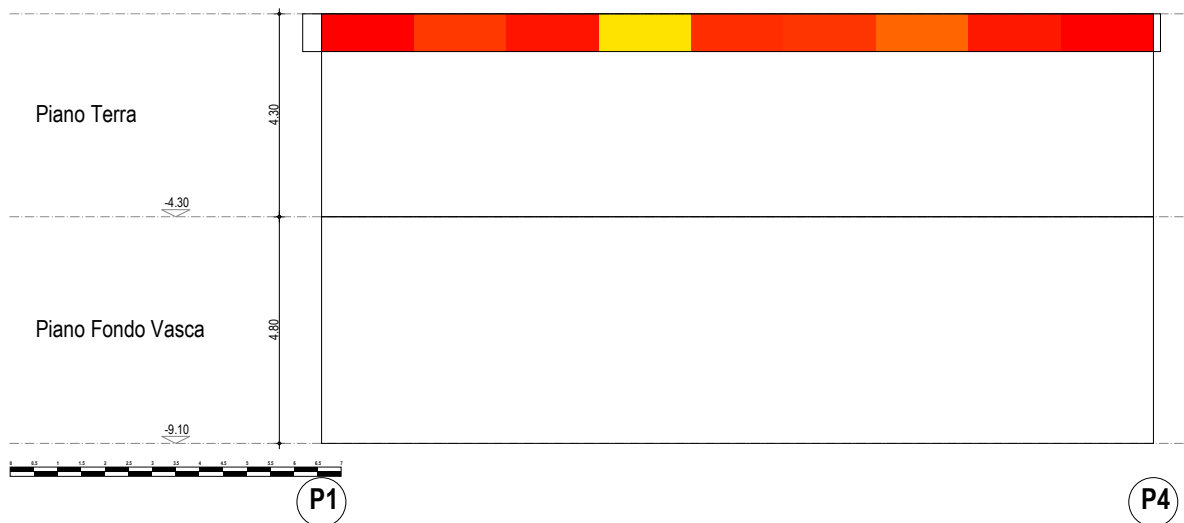
## Telaio P4-P5-P6

COEFFICIENTE DI SICUREZZA A FLESSIONE



## Telaio P1-P4

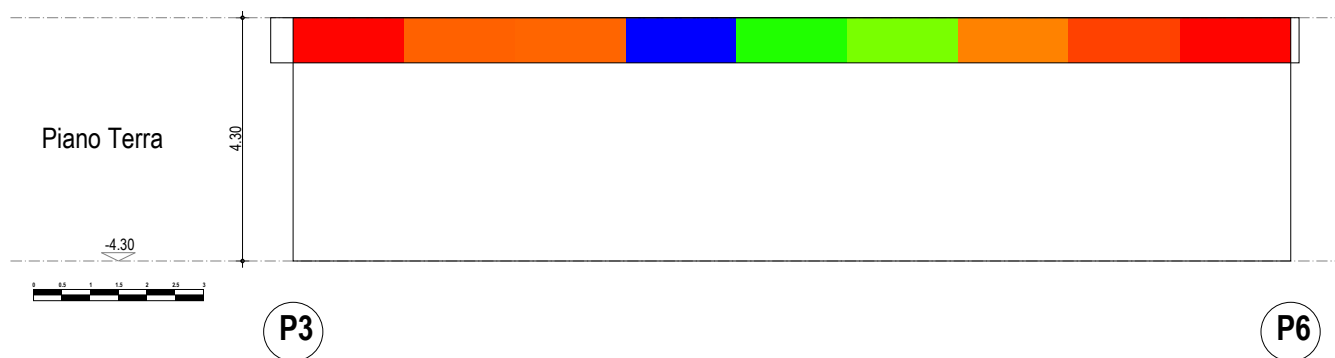
COEFFICIENTE DI SICUREZZA A FLESSIONE





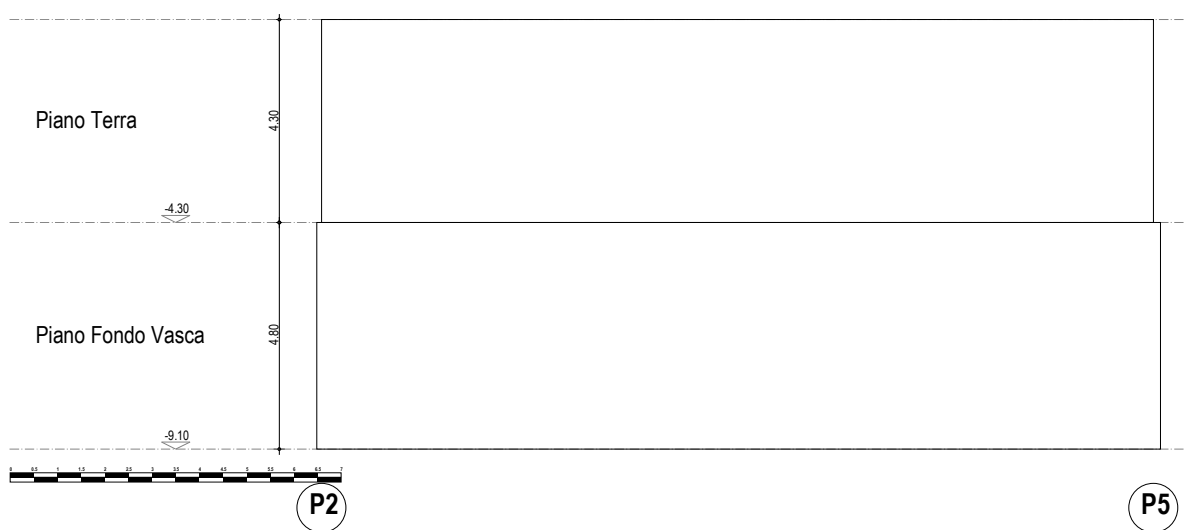
### Telaio P3-P6

COEFFICIENTE DI SICUREZZA A FLESSIONE



### Telaio P2-P5

COEFFICIENTE DI SICUREZZA A FLESSIONE

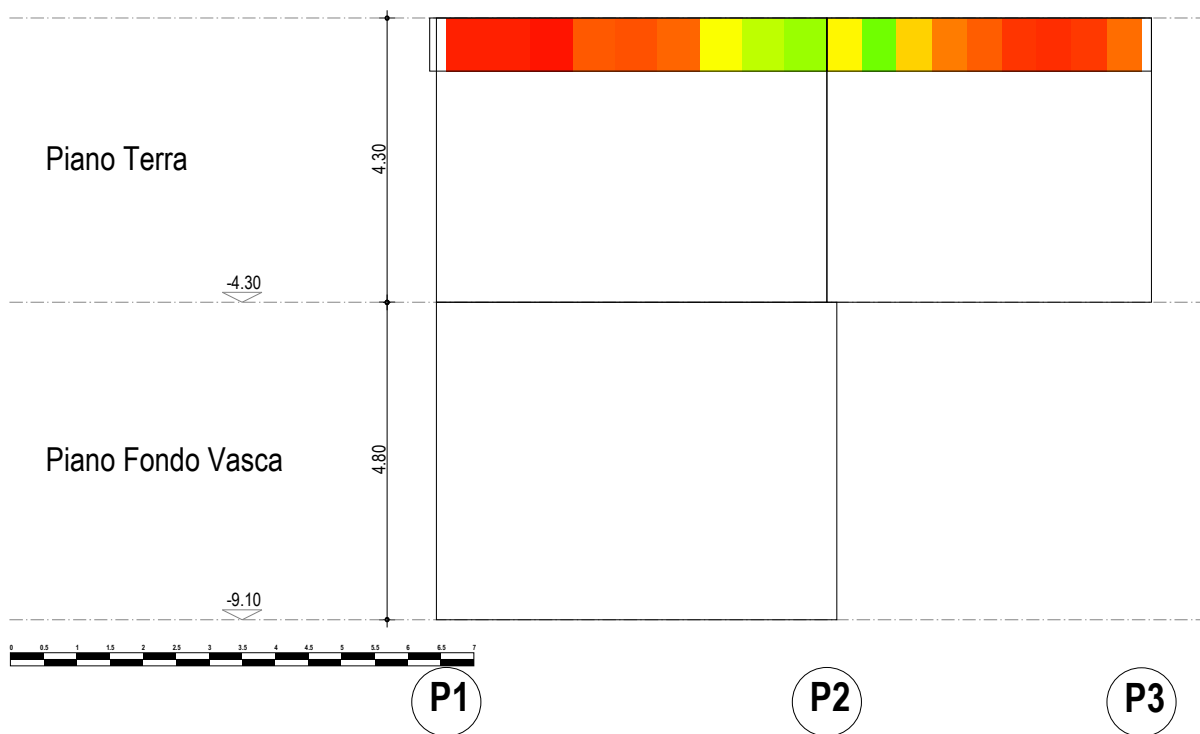






### Telaio P1-P2-P3

COEFFICIENTE DI SICUREZZA A TAGLIO





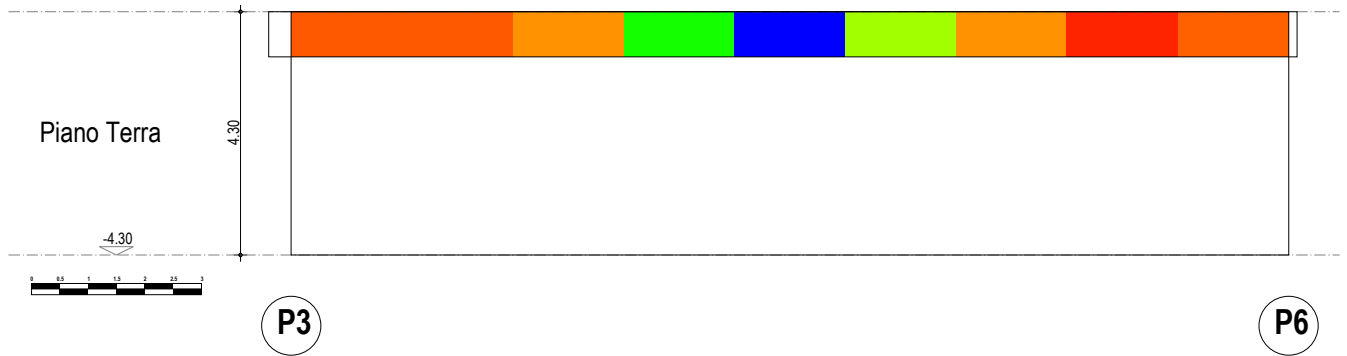
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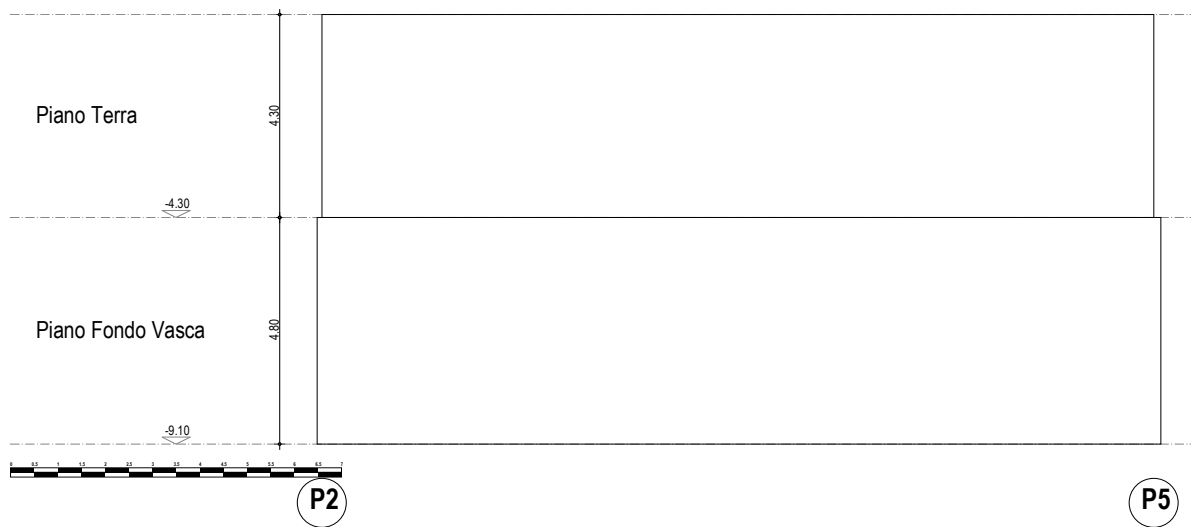
### Telaio P3-P6

COEFFICIENTE DI SICUREZZA A TAGLIO



### Telaio P2-P5

COEFFICIENTE DI SICUREZZA A TAGLIO





## **5 - CONCLUSIONI**

Le verifiche eseguite in merito alla stabilità globale e locale della struttura hanno dato esito positivo per l'opera di progetto, pertanto la struttura risulta verificata rispetto alla crisi locale e globale in ogni sua parte sia per forze statiche che per sollecitazione sismica nel rispetto dei D.M. Min. LL. PP. 14 Gennaio 2008.

Si rilascia per gli usi consentiti dalla legge.

Il Tecnico  
**Ing. Fabio Mastellone di Castelvete**